**Unit 6: Bending** 

## **Shear and Moment Diagrams**

- Members with support loadings applied perpendicular to their longitudinal axis are called beams.
- Beams classified according to the way they are supported.



### **Shear and Moment Diagrams**

- Shear and moment functions can be plotted in graphs called shear and moment diagrams.
- In order to properly design a beam, it is important to know the variation of the shear force and moment along its axis to find the points where these values are a maximum.

Draw the shear and moment diagrams for the beam shown.

### Solution:

From the free-body diagram of the left segment, we apply the equilibrium equations,

$$+ \uparrow \sum F_{y} = 0; \quad V = \frac{P}{2} \qquad (1)$$
$$(+\sum M = 0; \quad M = \frac{P}{2}x \qquad (2)$$

Left segment of the beam extending a distance *x* within region *BC* is as follow,

$$\uparrow \sum F_{y} = 0; \qquad \frac{P}{2} - P - V = 0 \Longrightarrow V = -\frac{P}{2} \quad (3)$$

$$(+\sum M = 0 \qquad M + P\left(x - \frac{L}{2}\right) - \frac{P}{2}x \Longrightarrow M = \frac{P}{2}(L - x) \quad (4)$$







The shear diagram represents a plot of Eqs. 1 and 3  $\square$ 

The moment diagram represents a plot of Eqs. 2 and 4  $\hfill\square$ 



#### **EXAMPLE 2**

Draw the shear and moment diagrams for the beam shown in Fig. 6–12*a*.

#### EXAMPLE 2 (cont.)

#### **Solutions**

• The reactions are shown on the free-body diagram in Fig. 6–12*b.* 

 The shear at each end is plotted first, Fig. 6–12c. Since there is no distributed load on the beam, the shear diagram has zero slope and is therefore a horizontal line.



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#### EXAMPLE 2 (cont.)

#### **Solutions**

 The moment is zero at each end, Fig. 6–12*d*. The moment diagram has a constant negative slope of -M<sub>0</sub>/2L since this is the shear in the beam at each point. Note that the couple moment causes a jump in the moment diagram at the beam's center, but it does not affect the shear diagram at this point.



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Draw the shear and moment diagrams for the beam shown.

### Solution:

The distributed load is replaced by its resultant force and the reactions.

Intensity of the triangular load at the section is found by proportion,

$$w/x = \frac{w_0}{L}$$
 or  $w = \frac{w_0}{L}$ 

Resultant of the distributed loading is determined from the area under the diagram,

$$+ \uparrow \sum F_{y} = 0; \quad \frac{w_{0}L}{2} - \frac{1}{2} \left(\frac{w_{0}x}{L}\right) x - V = 0 \Longrightarrow V = \frac{w_{0}}{2L} \left(L^{2} - x^{2}\right) \quad (1)$$
$$+ \sum M = 0; \quad \frac{w_{0}L^{2}}{3} - \frac{w_{0}L}{2} \left(x\right) + \frac{1}{2} \left(\frac{w_{0}x}{L}\right) x \left(\frac{1}{3}x\right) + M = 0 \quad (2)$$







The shear diagram represents a plot of Eqs. 1  $\hfill\square$ 

The moment diagram represents a plot of Eqs. 2  $\hfill\square$ 



Draw the shear and moment diagrams for the beam shown.

### Solution:

2 regions of *x* must be considered in order to describe the shear and moment functions for the entire beam.

$$0 \le x_{1} < 5 \text{ m},$$
  
+  $\uparrow \sum F_{y} = 0;$   $5.75 - V = 0 \Rightarrow V = 5.75 \text{ kN}$  (1)  
+  $\sum M = 0;$   $-80 - 5.75x_{1} + M = 0 \Rightarrow M = (5.75x_{1} + 80) \text{ kNm}$  (2)  
 $5 \text{ m} \le x \le 10 \text{ m}$ 

$$+ \uparrow \sum F_{y} = 0; \quad 5.75 - 15 - 5(x_{2} - 5) - V = 0 \Rightarrow V = (15.75 - 5x_{2}) \text{ kN } (3)$$

$$+ \sum M = 0; \quad -80 - 5.75x_{1} + +15 + 5(x_{2} - 5)\left(\frac{x_{2} - 5}{2}\right) + M = 0$$

$$M = (-2.5x_{2}^{2} + 15.75x_{2} + 92.5) \text{ kNm} \quad (4)$$



 $15 \text{ kN} 5(x_2 - 5)$ 



5.75 kN

80 kN·m



15 kN

Graphical Method for Constructing Shear and **Moment Diagrams** 

#### **Regions of Distributed Load**

The following 2 equations provide a convenient means for quickly obtaining the shear and moment diagrams for a beam. w(x)



area of segment

Draw the shear and moment diagrams for the beam shown.

### Solution:

The reactions are shown on a free-body diagram.

For shear diagram according to the sign convention,

at x = 0, V = +P and at x = L, V = +P

Since w = 0, the *slope* of the shear diagram will be zero, thus

dV/dx = -w = 0 at all points

For moment diagram according to the sign convention,

at x = 0, M = -PL and at x = L, M = 0

The shear diagram indicates that the shear is constant Positive, thus

dM/dx = V = +P at all points





Draw the shear and moment diagrams for the beam shown.

### Solution:

The reaction at the fixed support is shown on the free-body diagram.

Since no distributed load exists on the beam the shear diagram will have zero *slope*, at all points.

From the shear diagram the *slope* of the moment diagram will be zero since V = 0.







Draw the shear and moment diagrams for the beam shown.

### Solution:

The reaction at the support is calculated and shown on the free-body diagram.

The distributed loading on the beam is positive yet Decreasing, thus negative slope.

The curve of the moment diagram having this slope behaviour is a *cubic* function of *x*.





Draw the SFD and BMD for overhanging beam

#### Solution:

Calculate the reactions by using equations of static equilibrium

 $A_y = 25 \text{ kN}, C_y = 35 \text{ kN}$ 

[Max B.M occurs at the point of zero S.F. in Simple beam] From SFD

25/x = 15/(4-x);

Which gives x = 2.5 m;

Therefore maximum +ve bending moment will occur at x = 2.5 m;

 $M_{max}$  (+ve) = 25x2.5 - 10x(2.5)x(2.5/2) = 31.25 kNm

and  $M_{max}$  (-ve) = - 40 kNm; at point C.

Point of contra-flexure can be determined by writing the equation of BM for part BC and put it equal to zero;  $Mx= 25x - 10^{*}4(x-2) = 0;$  x= 5.33 from A.

https://civilengineer.webinfolist.com/mech/prob54.htm



#### Bending Deformation of a Straight Member

- Cross section of a straight beam remains plane when the beam deforms due to bending.
- There will be tensile stress on one side and compressive stress on the other side.



#### Bending Deformation of a Straight Member

- Longitudinal strain varies linearly from zero at the neutral axis.
- Hooke's law applies when material is homogeneous.
- Neutral axis passes through the *centroid* of the cross-sectional area for linear-elastic material.



### The Flexure Formula

 Resultant moment on the cross section is equal to the moment produced by the linear normal stress distribution about the neutral axis.

$$\sigma = -\frac{My}{I}$$

σ = normal stress in the member
 M = resultant internal moment
 I = moment of inertia

y = perpendicular distance from the neutral axis



Bending stress variation

By the right-hand rule, negative sign is compressive since it acts in the negative x direction.

The simply supported beam has the cross-sectional area as shown. Determine the absolute maximum bending stress in the beam and draw the stress distribution over the cross section at this location.





#### Solution:

The maximum internal moment in the beam is M = 22.5 kNm



By symmetry, the centroid *C* and thus the neutral axis pass through the mid-height of the beam, and the moment of inertia is 20 mm

$$I = \sum (\bar{I} + Ad^{2})$$
  
=  $2 \left[ \frac{1}{12} (0.25)(0.02)^{3} + (0.25)(0.002)(0.16)^{2} \right] + \left[ \frac{1}{12} (0.02)(0.3)^{3} \right]$   
=  $301.3(10^{-6}) m^{4}$ 

Applying the flexure formula where c = 170 mm,

$$\sigma_{\text{max}} = \frac{Mc}{I}; \quad \sigma_{\text{max}} = \frac{22.5(0.17)}{301.3(10^{-6})} = 12.7 \text{ MPa} \text{ (Ans)}$$



# **Unsymmetric Bending**

#### **Moment Arbitrarily Applied**

 We can express the resultant normal stress at any point on the cross section in general terms as



 $\sigma$  = normal stress at the point



- y, z = coordinates of the point measured from x, y, z axes  $M_y$ ,  $M_z$  = resultant internal moment components directed along y and z axes
  - $I_y, I_z = principal moments of inertia computed about the y$ and z axes

A T-beam is subjected to the bending moment of 15 kNm. Determine the maximum normal stress in the beam .



### Solution:

Both moment components are positive,

$$M_y = (15)\cos 30^\circ = 12.99 \text{ kNm}$$
  
 $M_z = (15)\sin 30^\circ = 7.50 \text{ kNm}$ 

For section properties, we have

$$\overline{z} = \frac{\sum \overline{z}A}{\sum A} = \frac{(0.05)(0.1)(0.04) + (0.115)(0.03)(0.2)}{(0.1)(0.04) + (0.03)(0.2)} = 0.0890 \text{ m}$$



Using the parallel-axis theorem,  $I = \overline{I} + Ad^2$  the principal moments of inertia are thus

0.080 m

0.080 m

 $\overline{z}$ 

$$I_{z} = \frac{1}{12} (0.1)(0.04)^{3} + \frac{1}{12} (0.03)(0.2)^{3} = 20.53(10^{-6}) \text{m}^{4}$$

$$I_{y} = \left[\frac{1}{12} (0.04)(0.1)^{3} + (0.1)(0.04)(0.089 - 0.05)^{2}\right] + \left[\frac{1}{12} (0.2)(0.03)^{3} + (0.2)(0.03)(0.115 - 0.089)^{2}\right] = 13.92(10^{-6}) \text{m}^{4}$$

The largest tensile stress at B and greatest compressive stress at C.

