

Diffusion Welding

Diffusion Welding

Lesson Objectives

When you finish this lesson you will understand:

- Diffusion Welding Definition, Characteristics, Process & Applications
- Diffusion Coefficients & Kirkendall Effect
- Interface Interactions & Dissimilar Metals

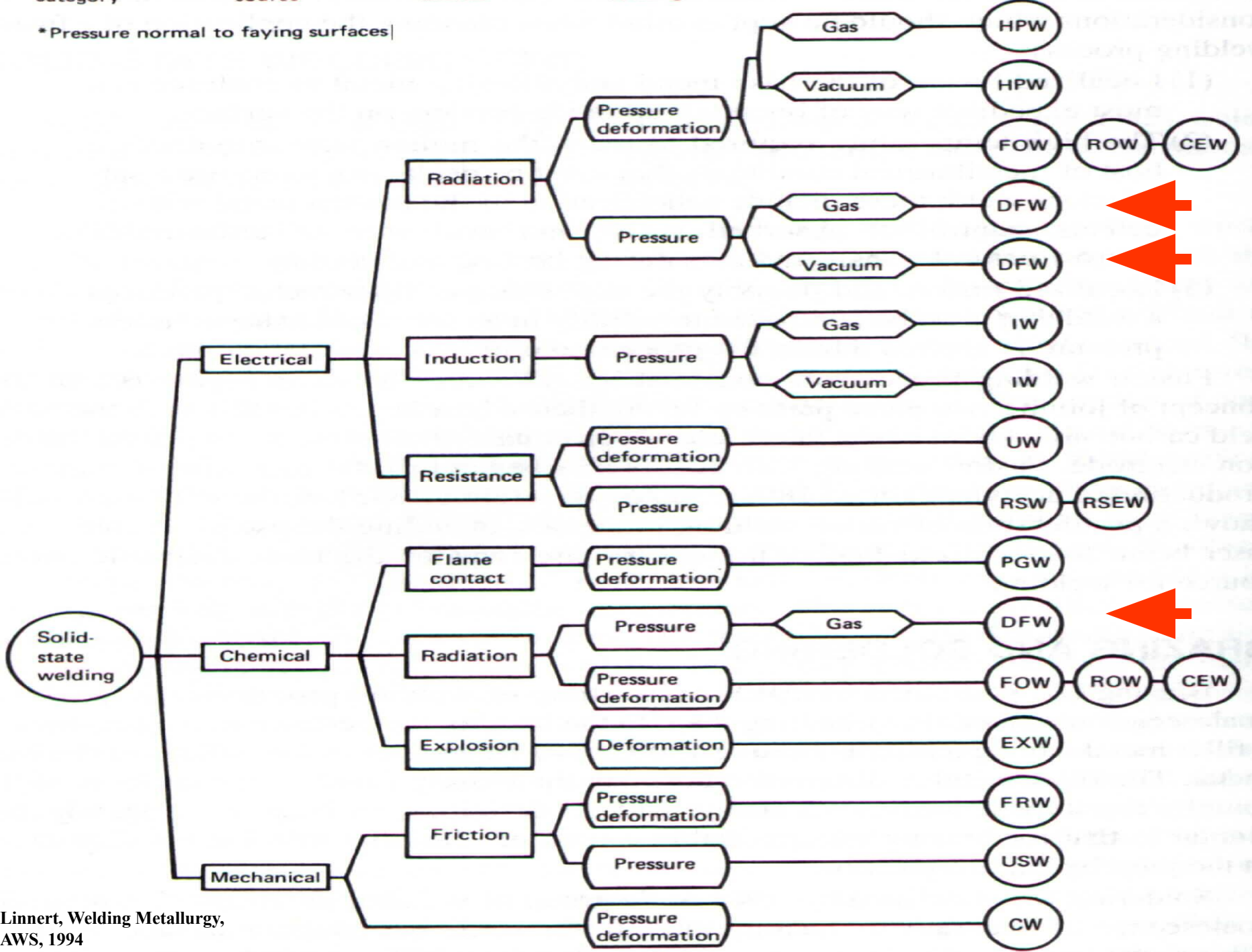
Learning Activities

1. View Slides;
2. Read Notes,
3. Listen to lecture
4. Do on-line workbook

Keywords: Diffusion Welding, Diffusion Brazing, Transient Liquid Phase Bonding, Diffusion Coefficient, Kirkendall Porosity

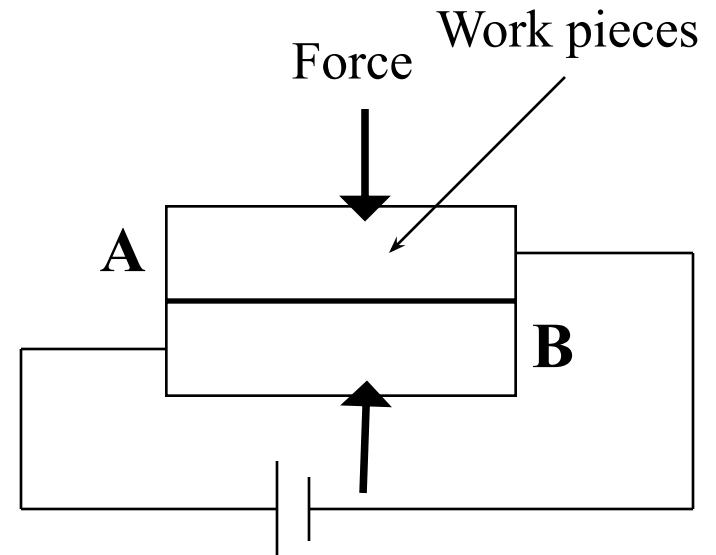
category source loading

*Pressure normal to faying surfaces|



Definition of Diffusion Welding

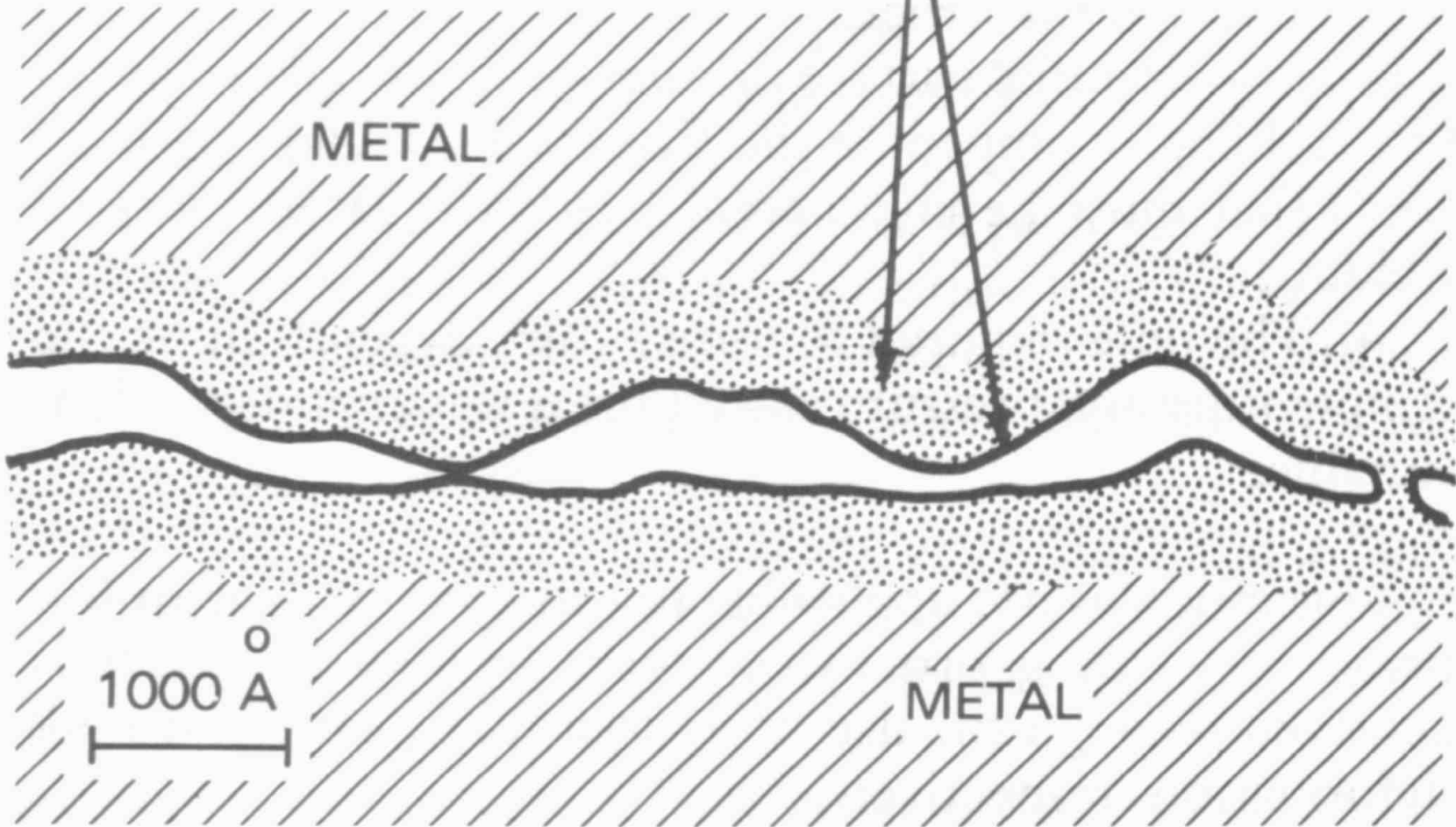
- A solid-state welding process that produces coalescence of the faying surfaces by the application of pressure at elevated temperature.
- The process does not involve macroscopic deformation, or relative motion of the workpieces.
- A solid filler metal may or may not be inserted between the faying surfaces.



Schematic representation of diffusion welding using electrical resistance for heating

OXIDE AND
CONTAMINANT LAYERS

METAL



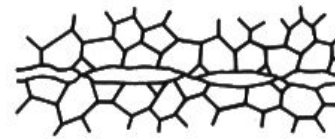
1000 Å

METAL

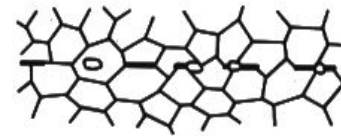
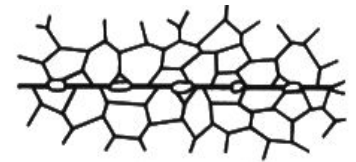
Diffusion Welding Working Principles

- 1st stage
 - deformation forming interfacial boundary.
- 2nd stage
 - Grain boundary migration and pore elimination.
- 3rd stage
 - Volume diffusion and pore elimination.

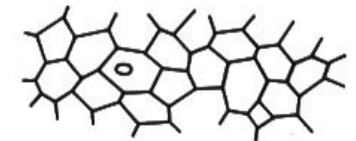
asperities come into contact.



1st stage deformation and interfacial boundary formation

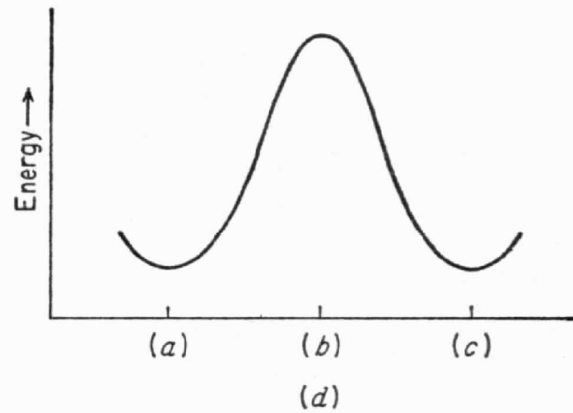
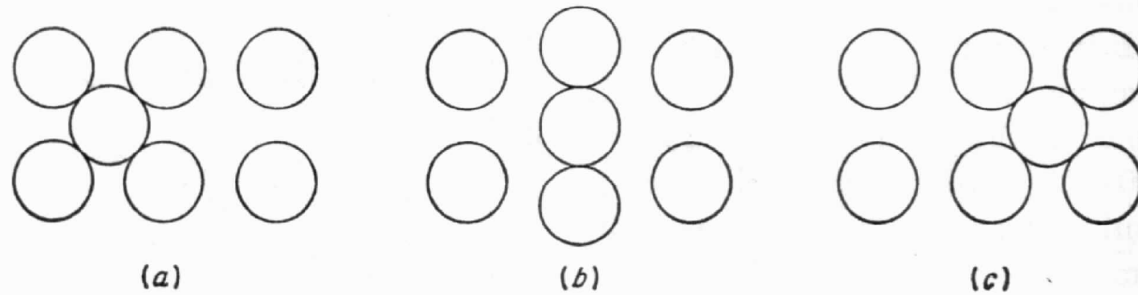


2nd stage grain boundary migration and pore elimination



3rd stage volume diffusion pore elimination

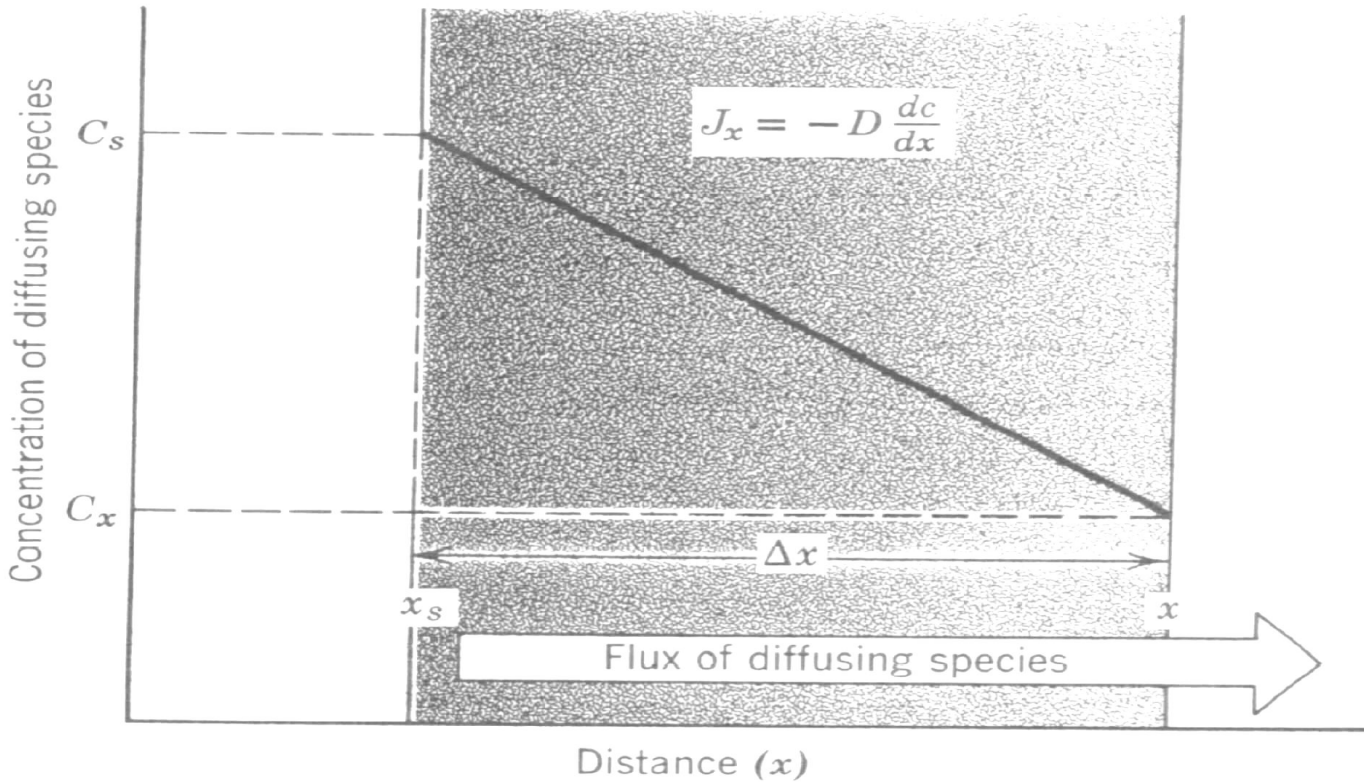
Free Energy as Atom Reversibly Moves



Factors Influencing Diffusion Welding

(Relation between Temperature and Diffusion Coefficient)

- Temperature
- $D = D_0 e^{-Q/KT}$
 - D = Diffusion coefficient
 - D_0 = Diffusion constant
 - Q = Activation energy
 - T = Absolute temperature
 - K = Boltzman's constant



$$J_1 = -D_1 \left(\frac{dc}{dx} \right)$$

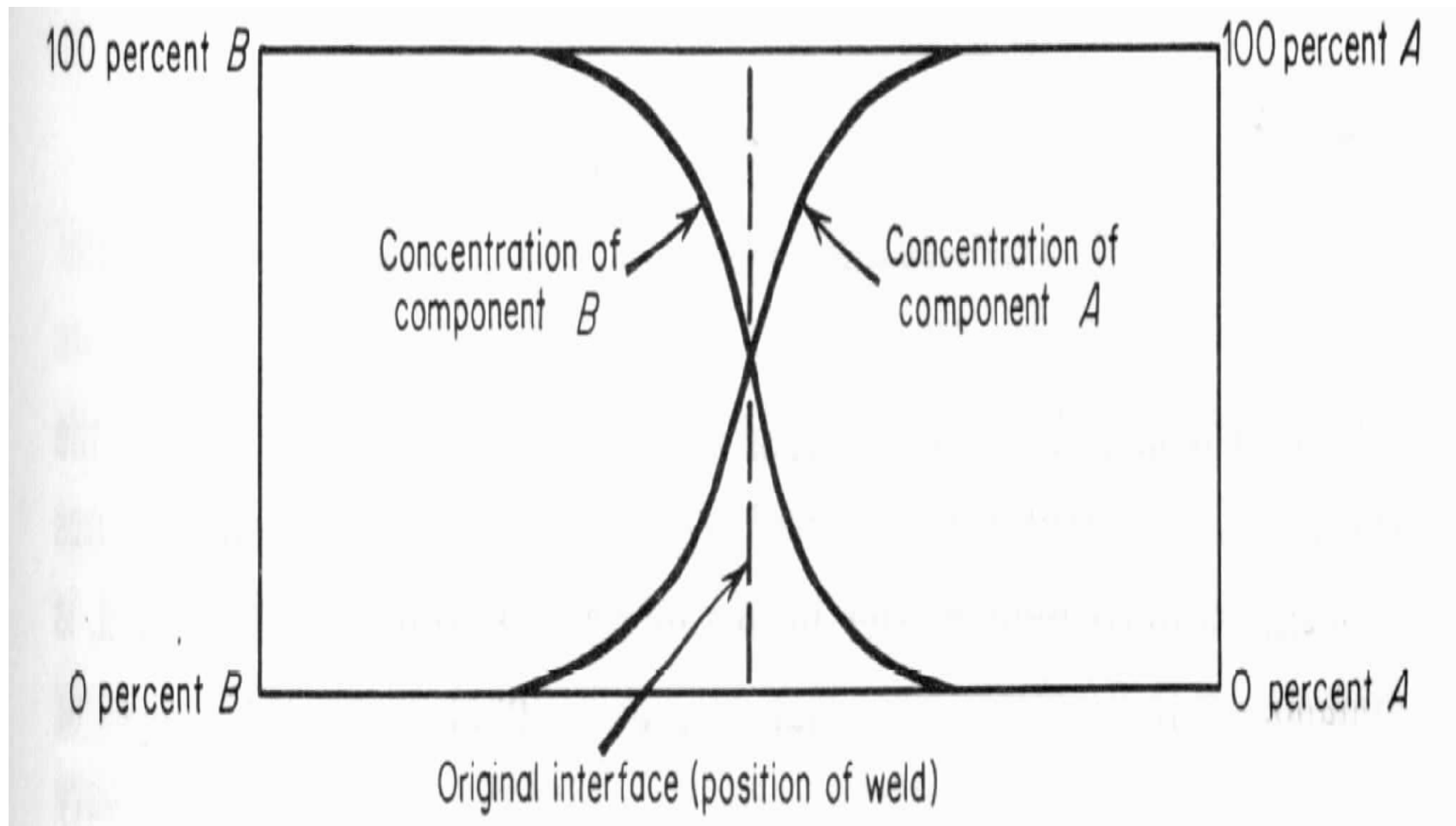
$$\frac{\text{Mass}}{\text{L}^2 \text{t}}$$

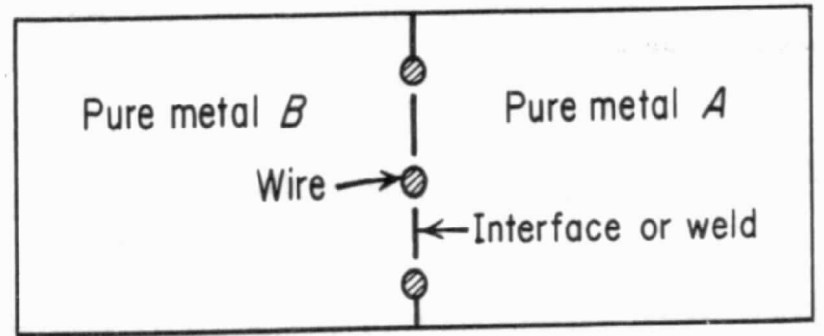
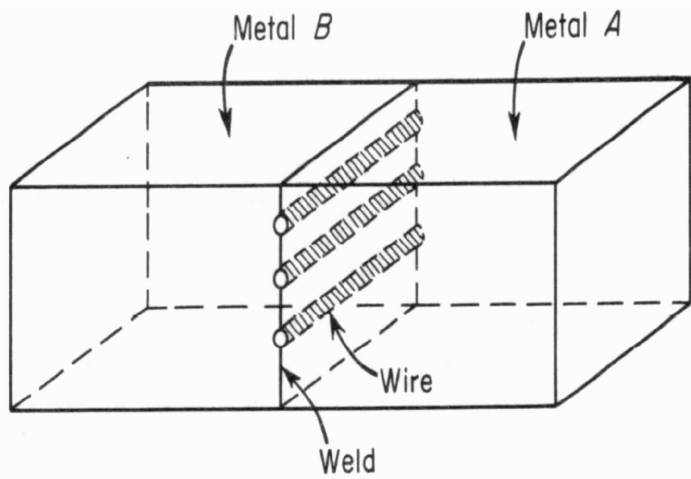
$$\frac{\text{L}^2}{\text{t}}$$

$$\frac{\text{Mass/L}^3}{\text{L}}$$

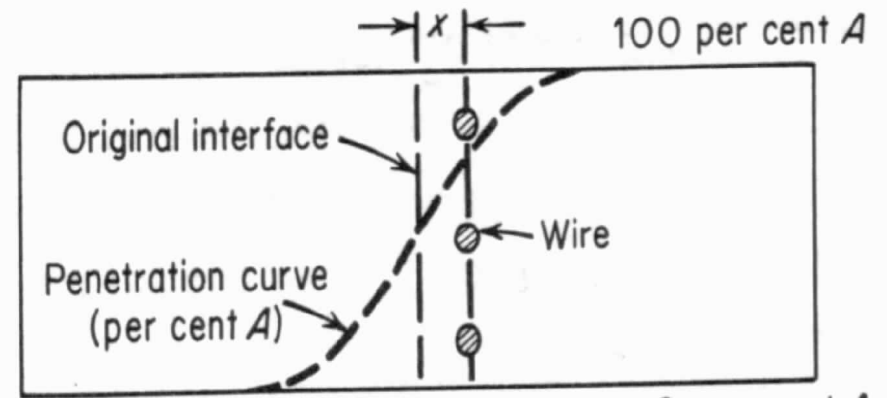
Factors Influencing Diffusion Welding

- Temperature (effects diffusion coefficient)
- Time
- $X = C (Dt)^{1/2} = \text{Diffusion Length}$
 - $X = \text{Diffusion length}$
 - $C = \text{A constant}$
 - $D = \text{Diffusion coefficient (see previous slide)}$
 - $t = \text{Time}$
- Pressure

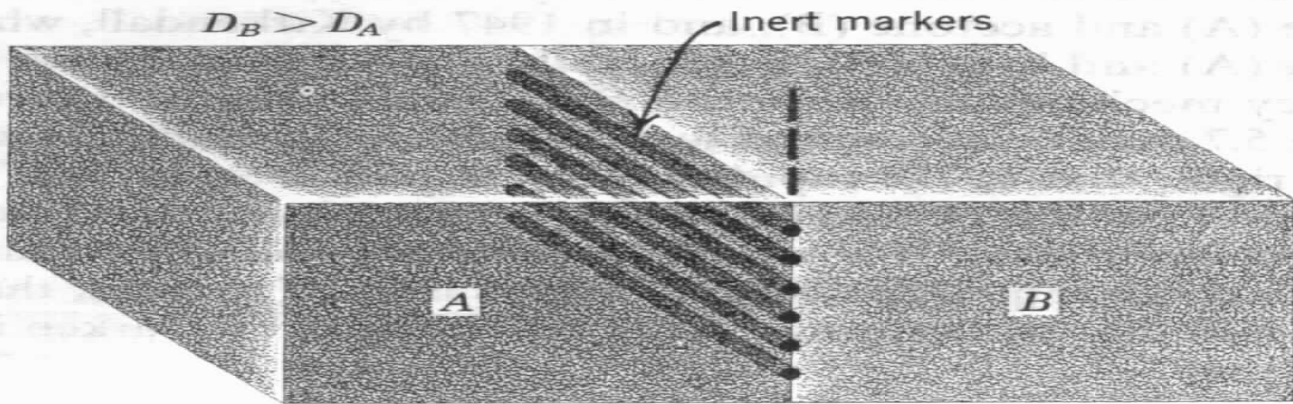




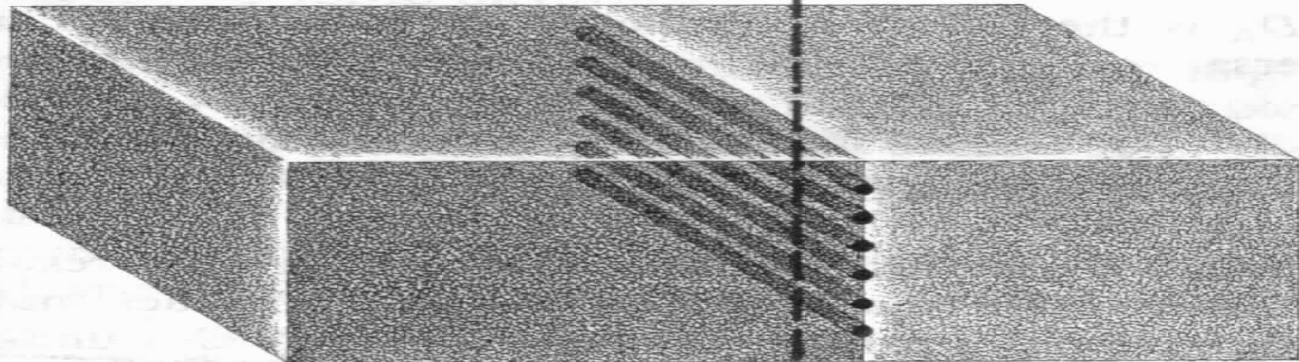
(A)



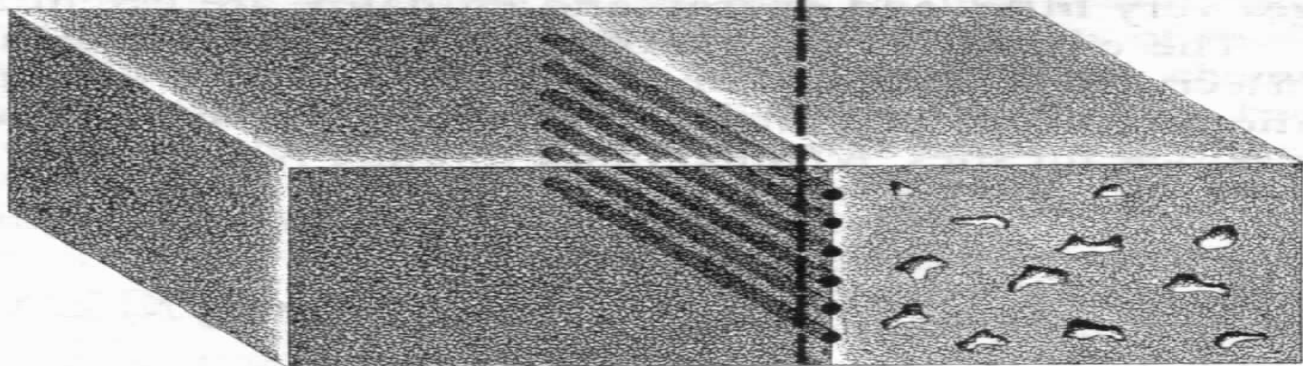
(B)



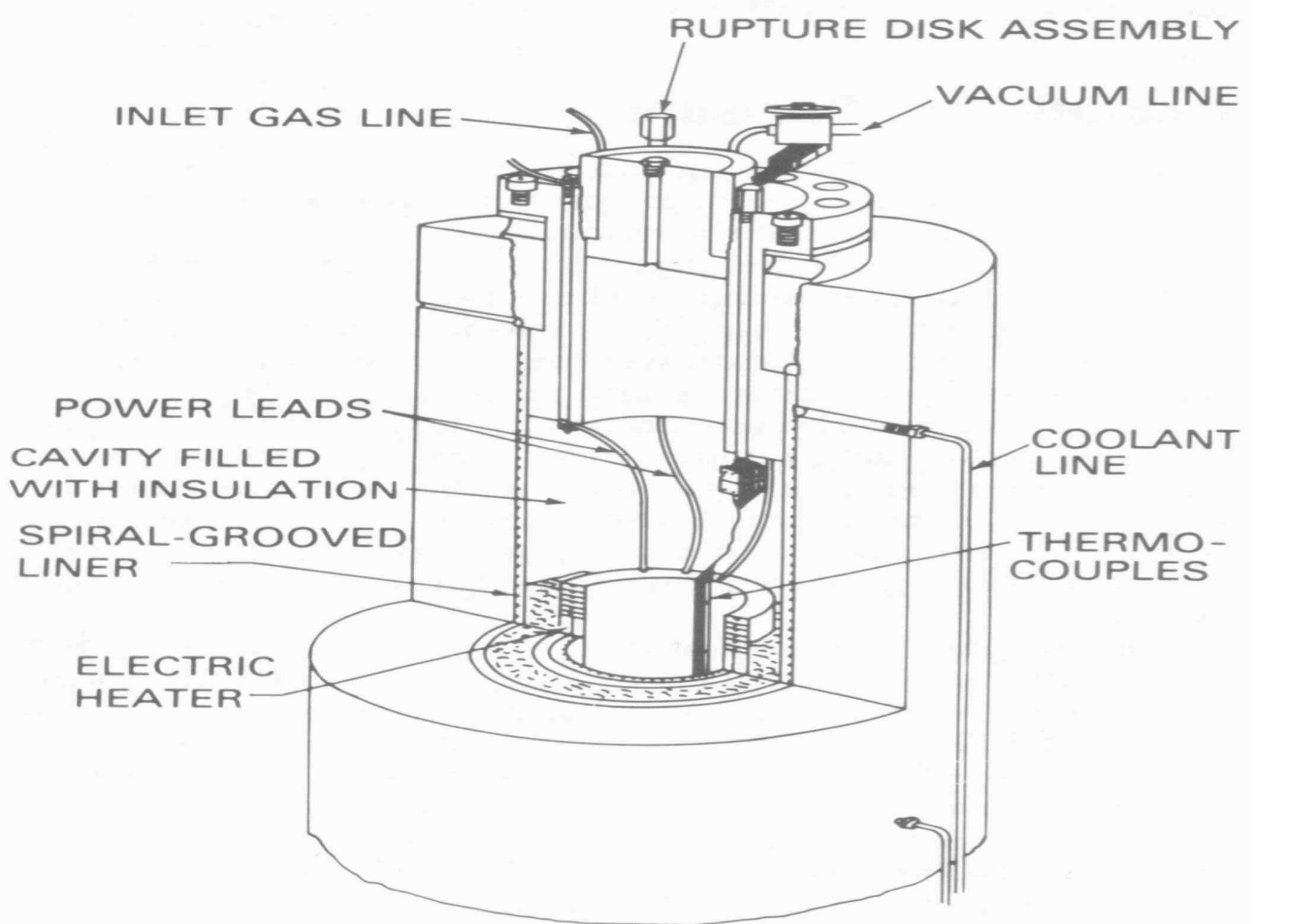
(a) Initial conditions

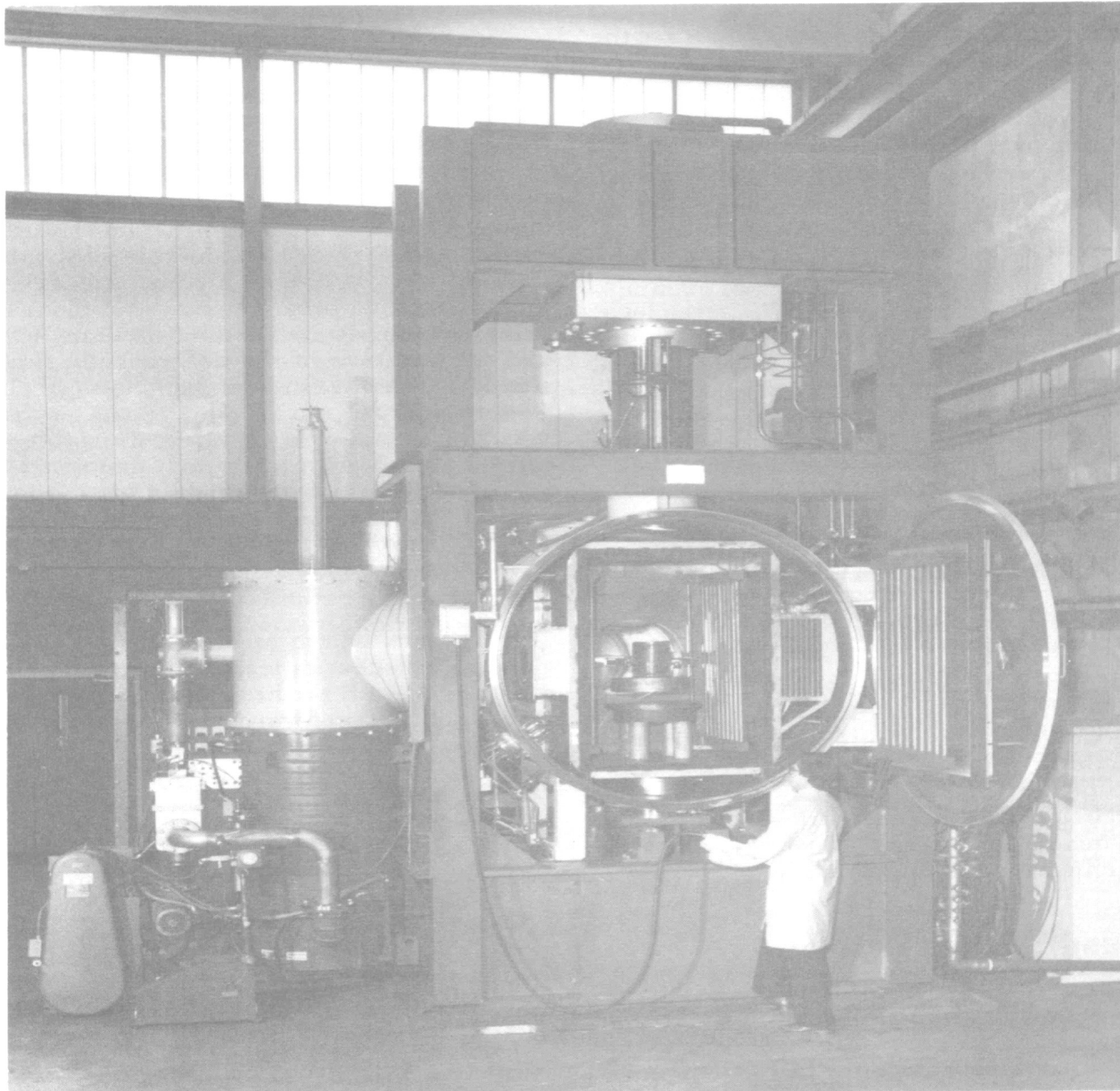


(b) Marker migration



(c) Marker migration and porosity





Applications of Diffusion Welding

- Application in titanium welding for aero-space vehicles.
- Diffusion welding of nickel alloys include Inconel 600, wrought Udimet 700, and Rene 41.
- Dissimilar metal diffusion welding applications include Cu to Ti, Cu to Al, and Cu to Nb-1%Zr. Brittle intermetallic compound formation must be controlled in these applications.

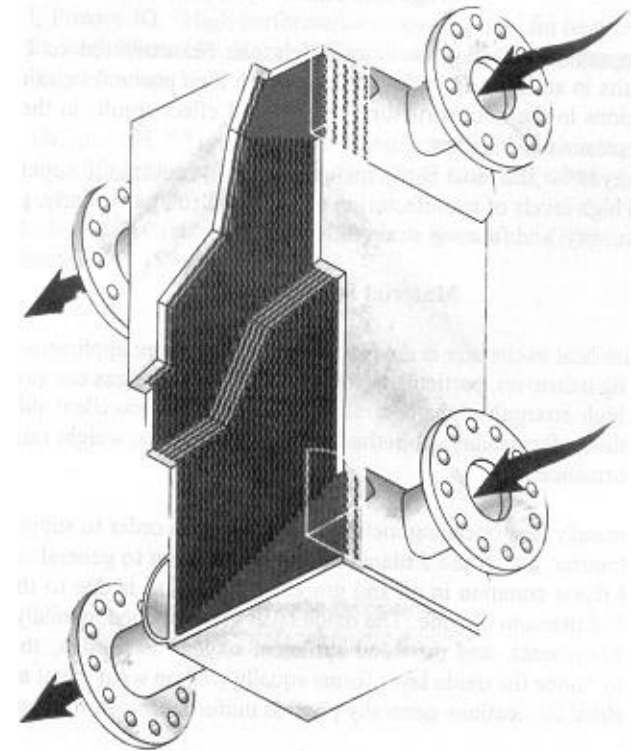
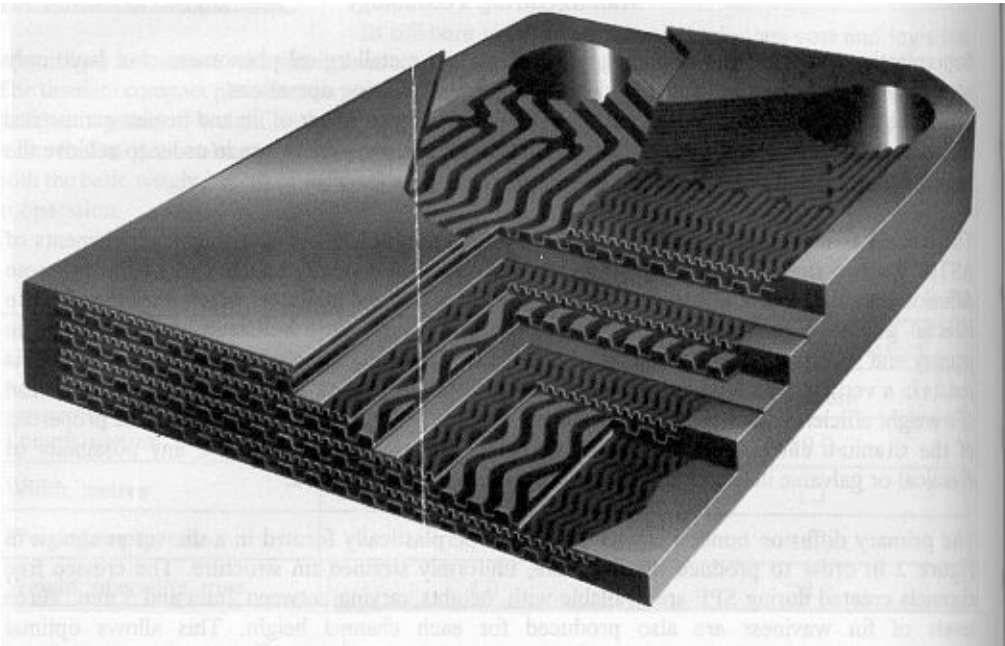
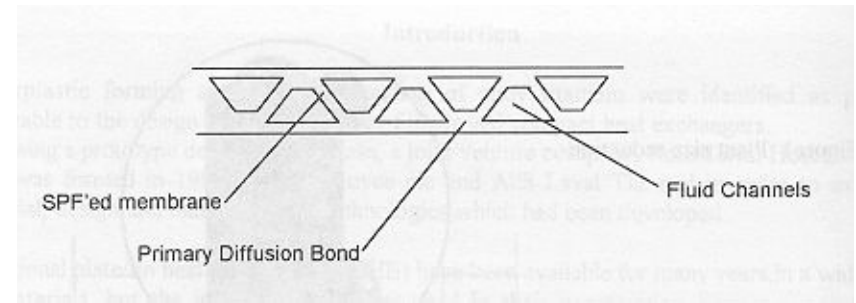
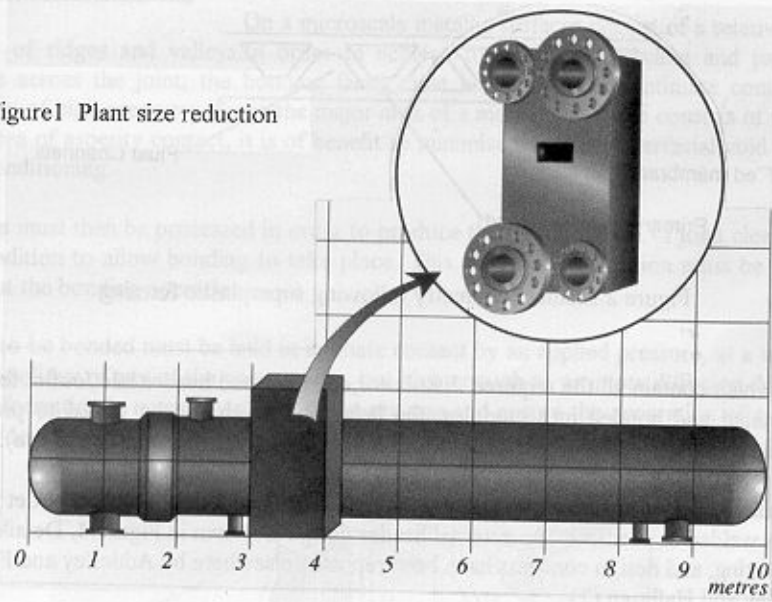
Titanium Diffusion Welding

- **Temp As High As Possible Without Damage to Base Metal**
75 to 100 F below Alpha-Beta Transus (eg 1700F)
- **Time varies with other facts below but 1 hr to 4 hour typical**
- **Pressure near yield (at temp)**
- **Smooth Faying Surface (rough surfaces = more time, pressure)**
- **Clean Surface (usually acid cleaning)**

**Space Shuttle designed to have 28 Diffusion
Welding Components**

Superplastic Formed & Diffusion Bonded Titanium Heat Exchanger

Figure 1 Plant size reduction



Nickel Diffusion Welding

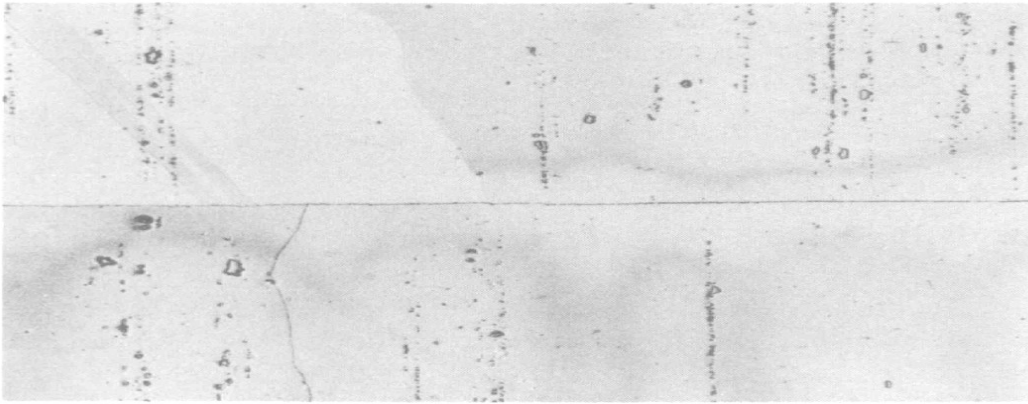
(More Difficult to Weld)

- Temp close to MP
- High Pressure (because High hot strength)
- Clean Surfaces - Ambient Atmosphere Control
(Surface Oxides Do Not Dissolve)
- Nickel Filler often used (especially for rough surface)

**Table 201
Typical Diffusion Welding Conditions for Some Nickel-Base Alloys**

Base Metal*	Filler Metal	Welding Temp.		Pressure,		Time, h
		°F	°C	psi	kPa	
Inconel 600	Ni	2000	1090	100-500	690-3450	0.5
Hastelloy X	Ni	2050	1120	100-500	690-3450	4
Wrought Udimet 700	Ni-35%Co	2140	1170	1000	6900	4
Cast Udimet 700	Ni-35%Co	2175	1190	1200	8275	4
Rene 41	Ni-Be	2150	1180	1550	10690	2
Mar-M 200	Ni-25%Co	2200	1205	1000-2000	6900-13800	2

**Without Nickel Filler Metal
Fine Ti(C,N) and NiTiO₃
Forms Reducing Strength**



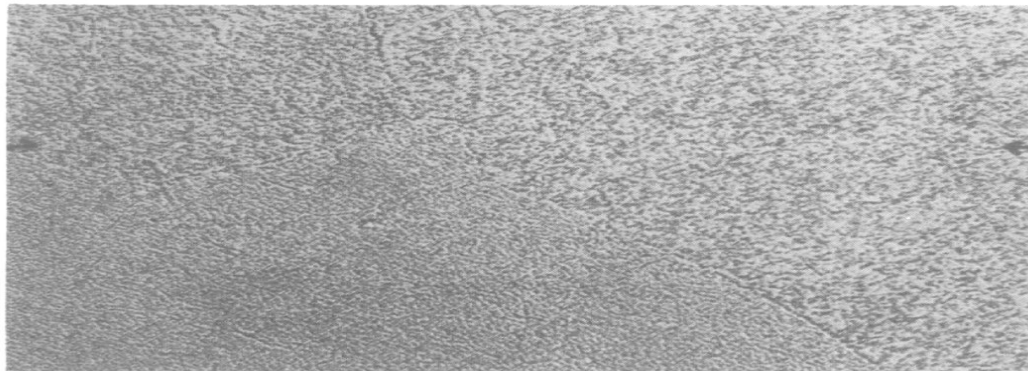
(A)

**With Ni Filler Metal
No Precipitates Formed
Grain Boundary Migration
But Excessive Ni₃Al ppt.**



(B)

**With Ni-35% Co
Good Joint Obtained**



(C)

Diffusion Welding of Dissimilar Metals

Some Potential Problems

- An intermetallic phase or a brittle intermetallic compound may form at the weld interface. Selection of an appropriate filler metal can usually prevent such problems. Joint designs can help also.
- Low melting phases may form. Sometime this effect is beneficial
- Porosity may form due to unequal rates of metal transfer by diffusion in the region adjacent to the weld (Kirkendall Porosity). Proper welding conditions or the use of and appropriate filler metal or both may prevent this problem.

**Table 20.2
Diffusion Welding Conditions for Some Dissimilar Metal Combinations**

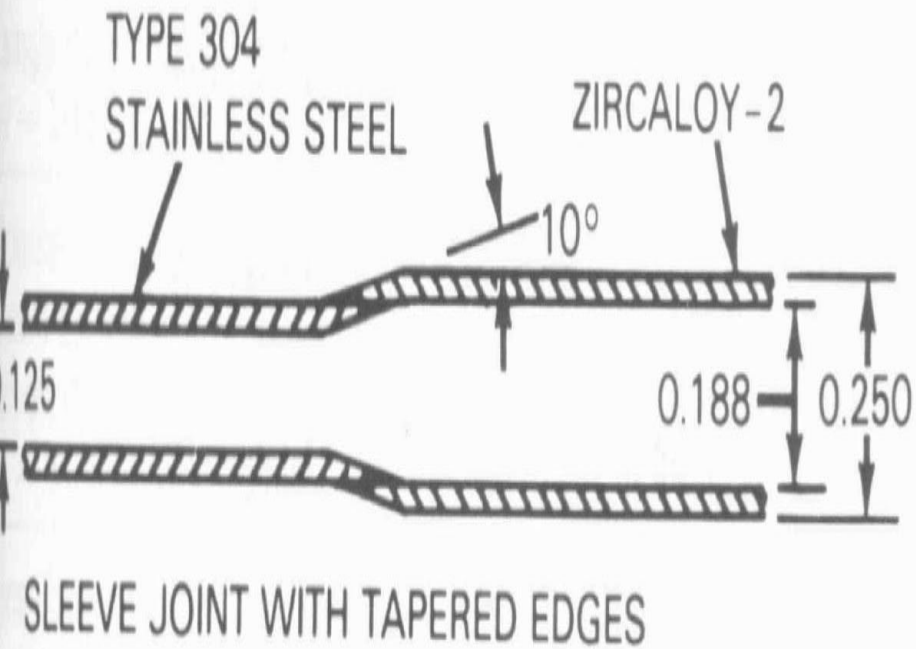
Base Metal Combinations	Filler Metal	Temperature,		Time,h	Pressure ^a ,		Atmosphere
		°F	°C		ksi	MPa	
Cu to Al	—	950	510	0.25	1	7	Vacuum
Cu to 316 Stainless Steel	Cu	1800	982	2		a	Vacuum
Cu to Ti	—	1560	849	0.25	0.7	5	Vacuum
Cu to Cb-1%Zr	Cb-1%Zr	1800	982	4		a	Vacuum
Cu-10%Zn to Ti-6%Al-6%V-2%Sn	—	900	482	8		a	Vacuum
4340 Steel ^c to Inconel 718 ^b	—	1730	943	4	29	200	Vacuum
Nickel 200 to Inconel 600 ^b	—	1700	927	3	1	7	Not Reported
Pyromet X-15 ^b to T-111 Ta alloy	Au-Cu	1100	593	4	30	207	Not Reported
Cb-1%Zr to 316 Stainless Steel	Cb-1%Zr	1800	982	4		a	Vacuum
Zircaloy-2 to 304 Stainless Steel	—	1870-1900	1021-1038	0.5		a	Vacuum

Questions

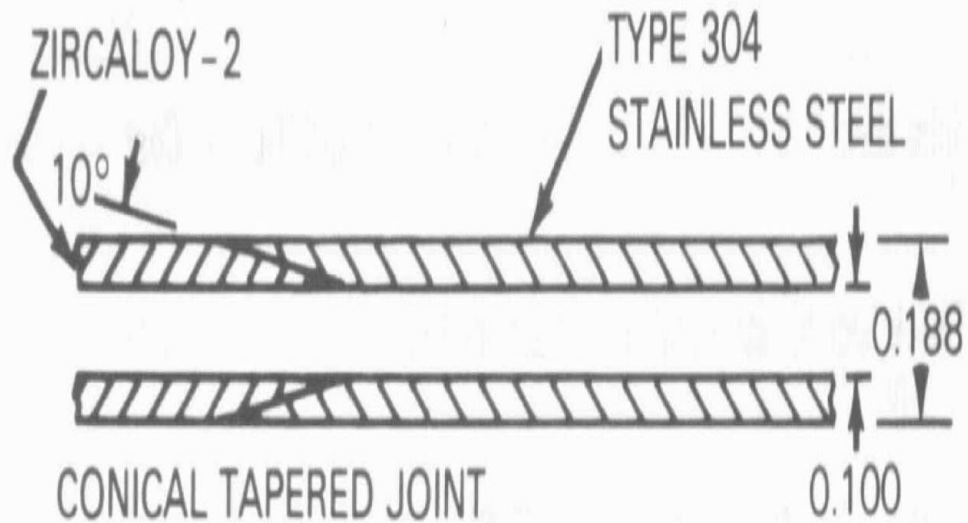
**Some
Specific
Applications
Of
Diffusion
Welding**

**Table 2.10
Recent Applications of Diffusion Joining in Japanese Industries**

Products	Materials	Reason for Adoption	Previous Method	Product Records
F-15 Fighter Fitting	Ti-6Al-4V	Cost reduction	Machining from forging or plate	more than 1000 parts
Impeller for Liquid Fuel Rocket	Ti-5Al-2.5Sn	Higher quality	—	100 parts
Jewelry	18K gold alloy	Higher quality	Brazing	400 million yen per year
Electrode	Cu-316L stainless steel	New type only possible by DJ	—	2200 parts
Tube sheet	Cupro Ni-mild steel-316L ss	Cost reduction	Rolling or explosive bonding	1000 parts
Chock liner for steel rolling mill	Brass-mild steel	Cost reduction	Solid Cu alloy	100 parts
Cooling plate for cyclotron accelerator	Cu-316Lss	New type only possible by DJ	—	50 parts
Continuous casting mold	wear resistant material - Cu alloy - 304 ss	New type only possible by DJ	—	20 parts

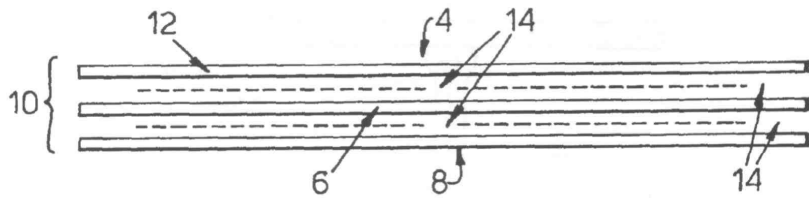


(A) BONDING PRESSURE IS APPLIED BY EXPANSION OF THE STAINLESS STEEL AGAINST THE ZIRCALOY.

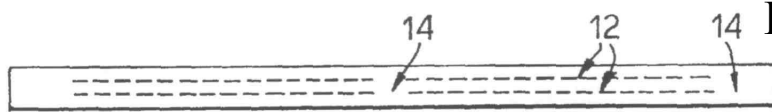


(B) BONDING PRESSURE IS APPLIED BY AN AXIAL COMPRESSIVE FORCE FROM AN INTERNAL BAR.

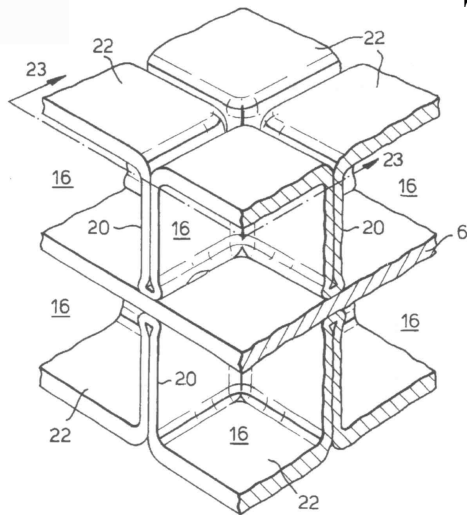
Diffusion Welding and Superplastic Forming for Aircraft Structure



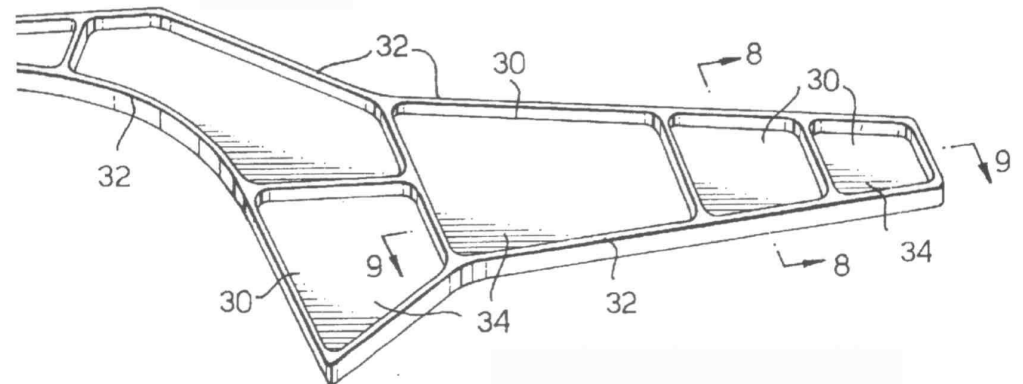
Sheets of superplastic material (ex. Al) stacked with stop-off material (silica) painted on specific areas



Diffusion bonding at 14 (stop-off areas 12)

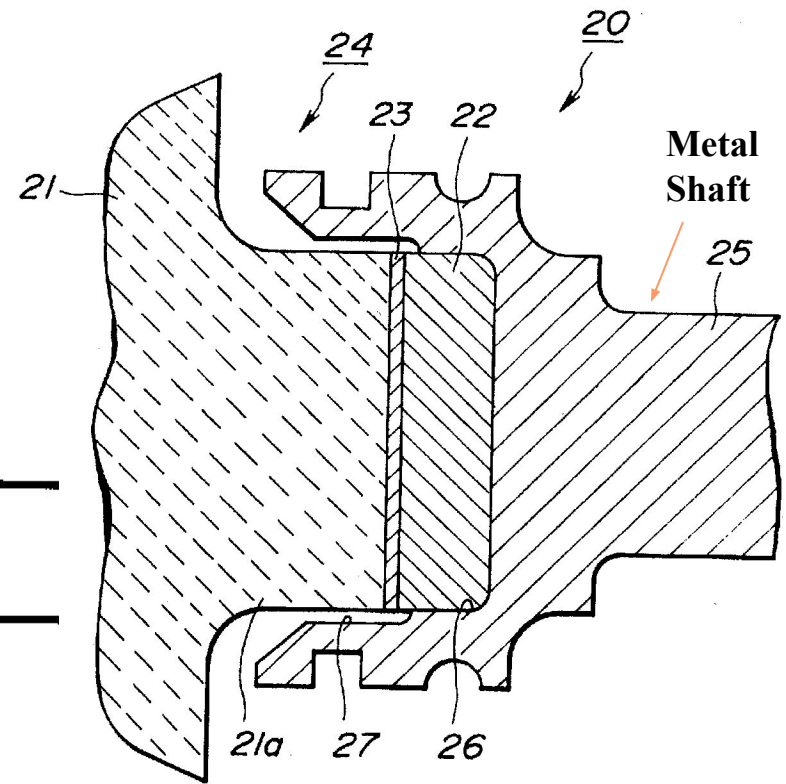
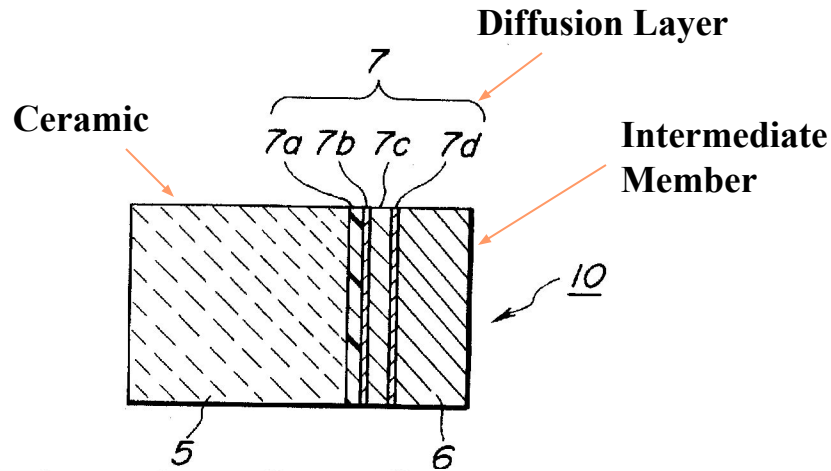


Pressure gas expands stop-off areas
Top cut off if required



Collier et al, "Method of Manufacturing Structural Parts, Particularly for use in Aircraft" US Patent 6,039,239 Mar 21, 2000

Ceramic Turbocharger Rotor (Diffusion bonded to Intermediate & Friction Welded to Shaft)



No.	Ceramic member	Intermediate member	Metallic member
A	silicon nitride	W alloy	alloy steel
B	silicon nitride	super hard hard alloy	heat resisting steel
C	silicon nitride	silicon nitride-TiN	stainless steel
D	silicon nitride	super hard alloy	Incoloy 903
E	alumina	Incoloy 903	stainless steel
D	alumina	Incoloy 903	stainless steel

Ito, M, et al, "Ceramic-Metal Composite Assembly" Patent 5,881,607 Mar 16, 1999

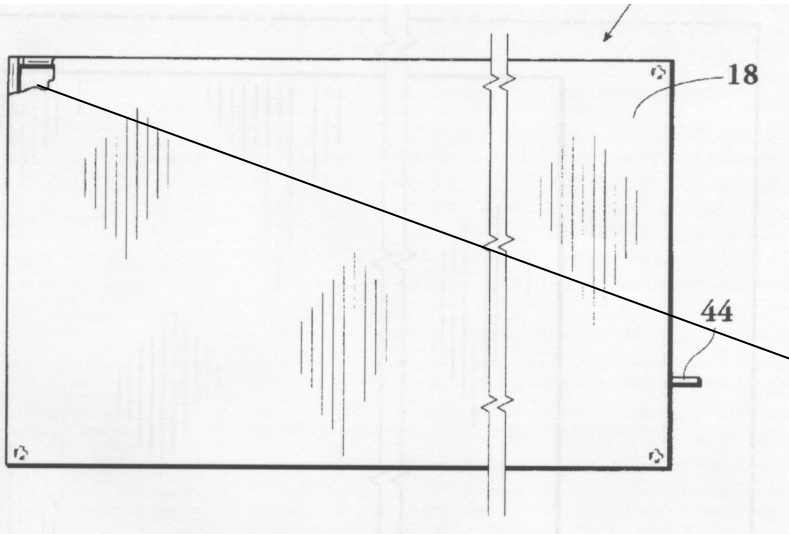
Questions

Diffusion Brazing

- **Low Melting inter-layer**
- **Melts & then diffuses into substrate**
- **Generally more rapid diffusion**

Some Applications

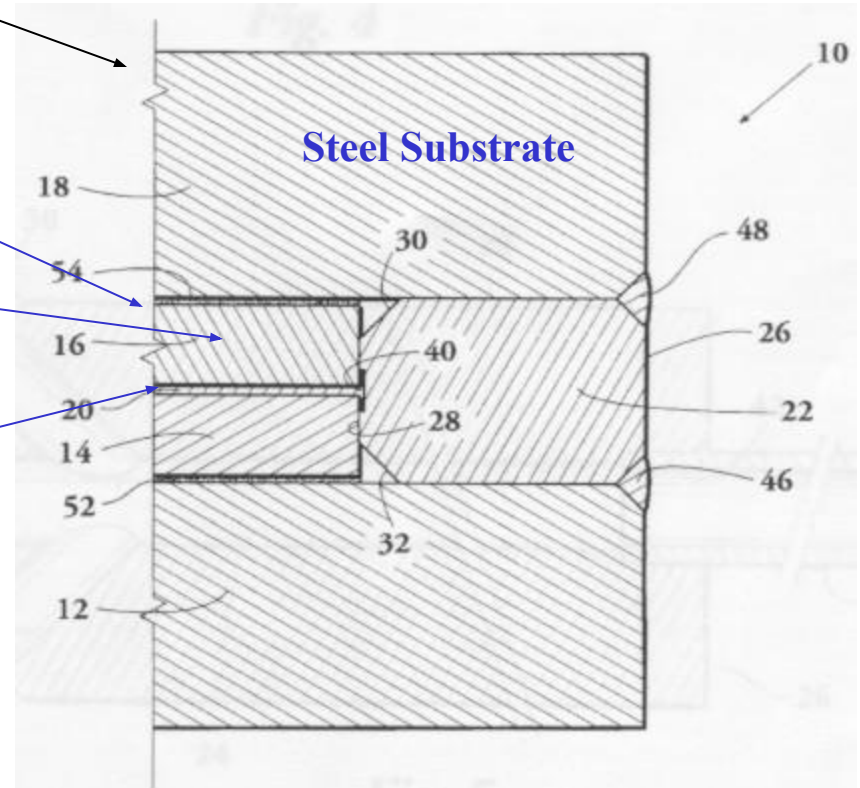
Liquid Phase Diffusion Bonding for Clad Steel Plates



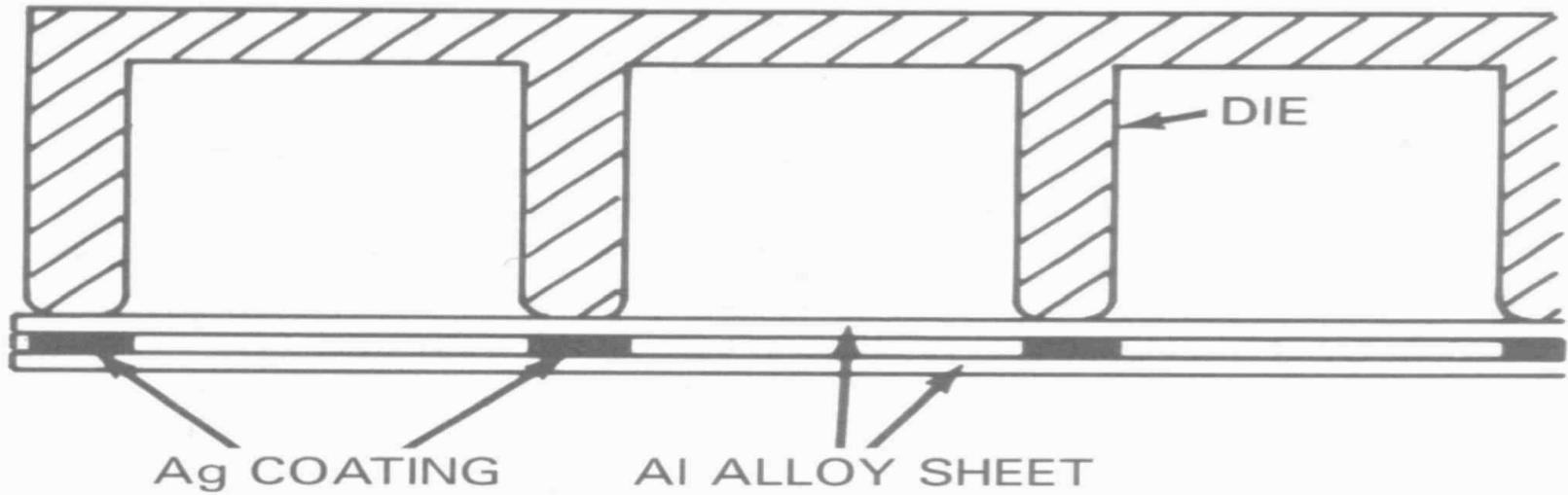
Sheets Stacked (2 sets) with bonding activator between sheets and separator between clad plates

Evacuated & Diffusion Bonded

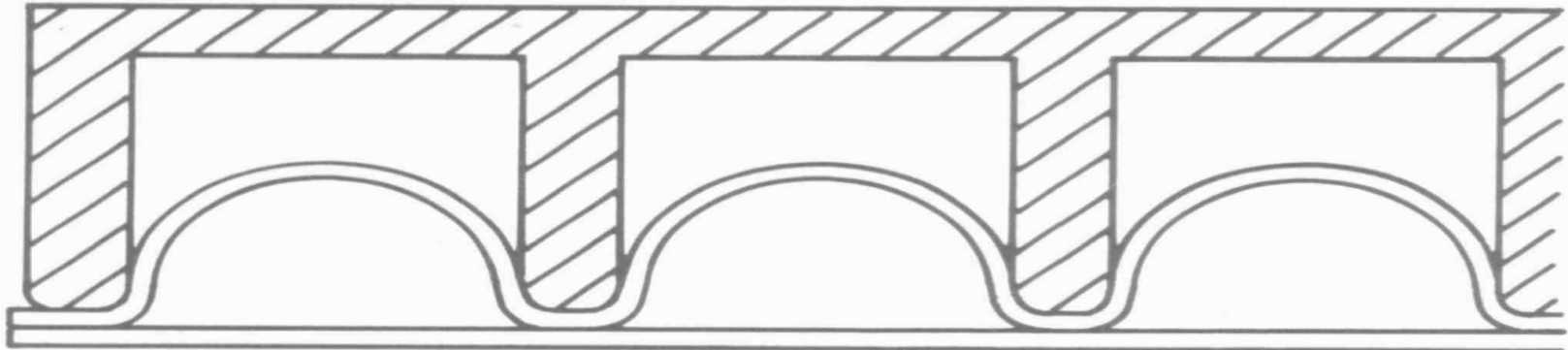
Bonding Activator (Ni4P)
Nickel Clad Material
Separator Compound (silica)



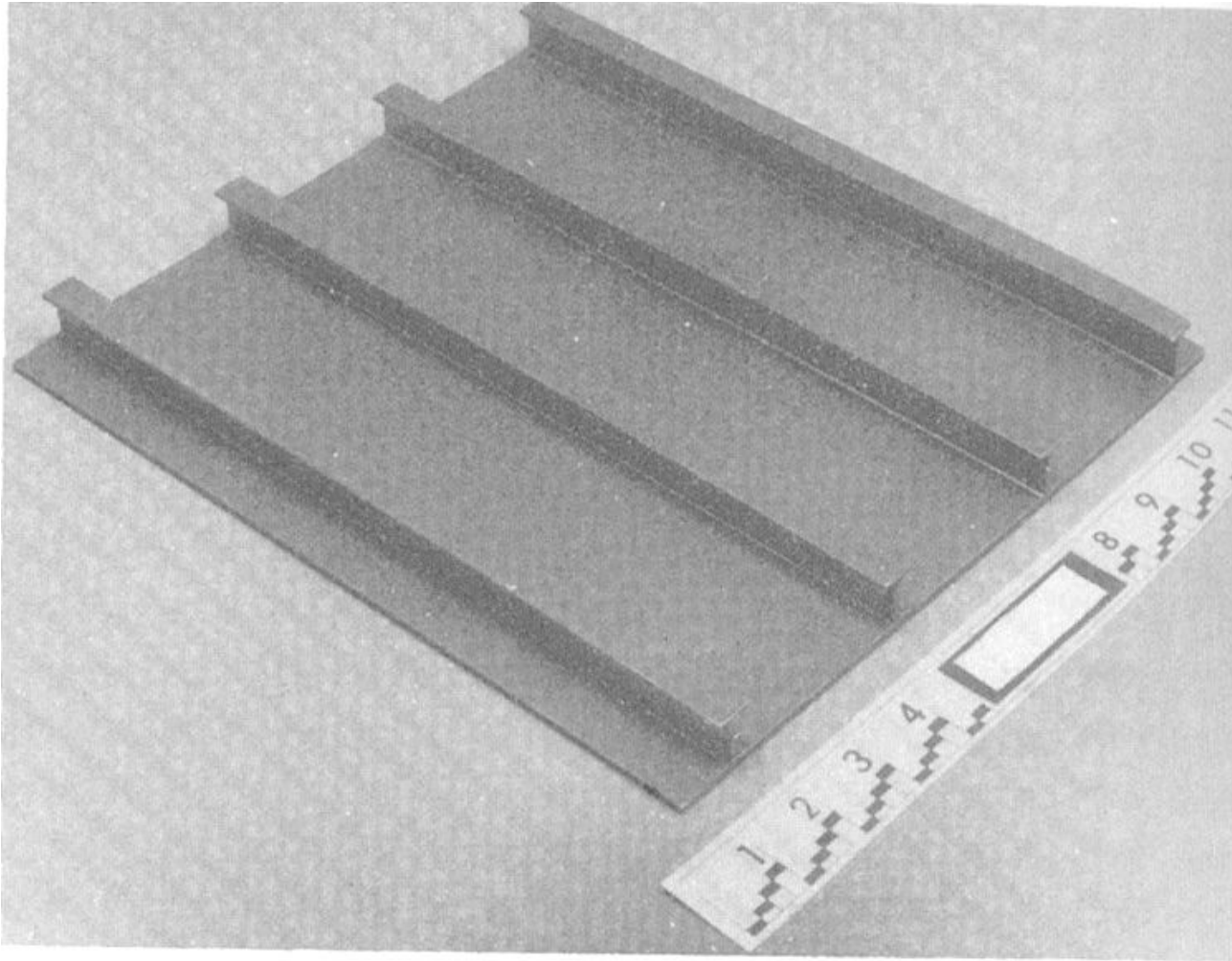
Diffusion Brazing of Aluminum



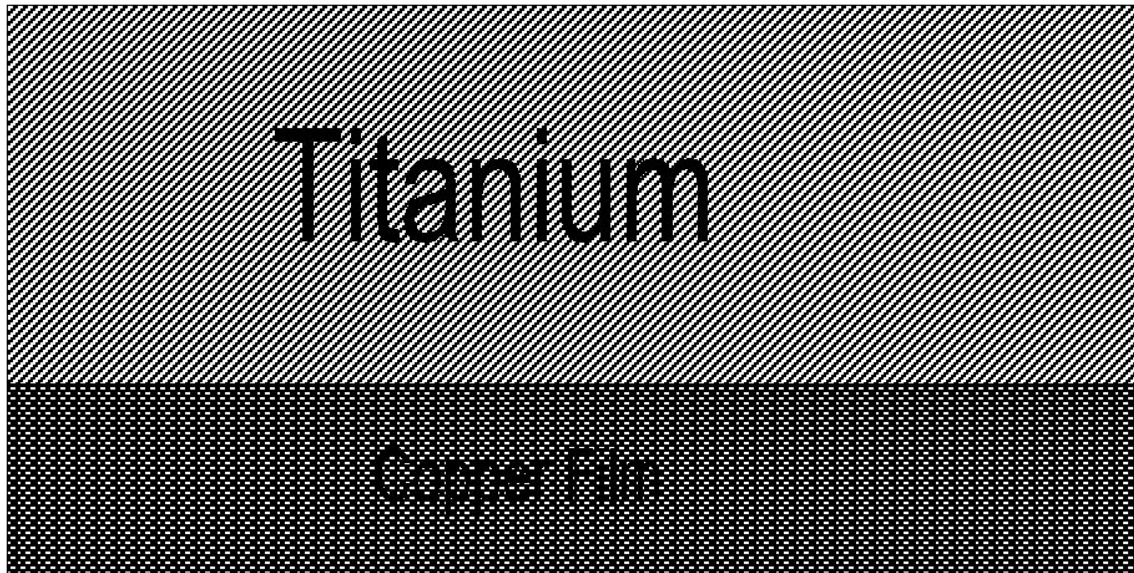
(A) SETUP PRIOR TO DIFFUSION WELDING



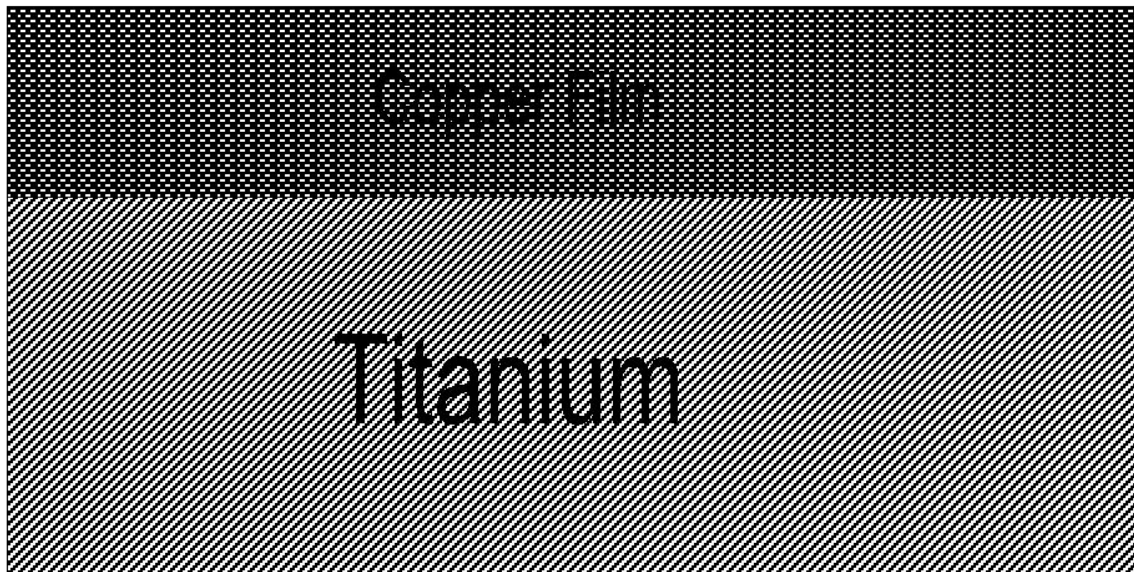
(B) ASSEMBLY AFTER WELDING AND FORMING



**A Titanium Alloy Stiffened Sheet Structure
Fabricated by Continuous Seam Diffusion Braze**

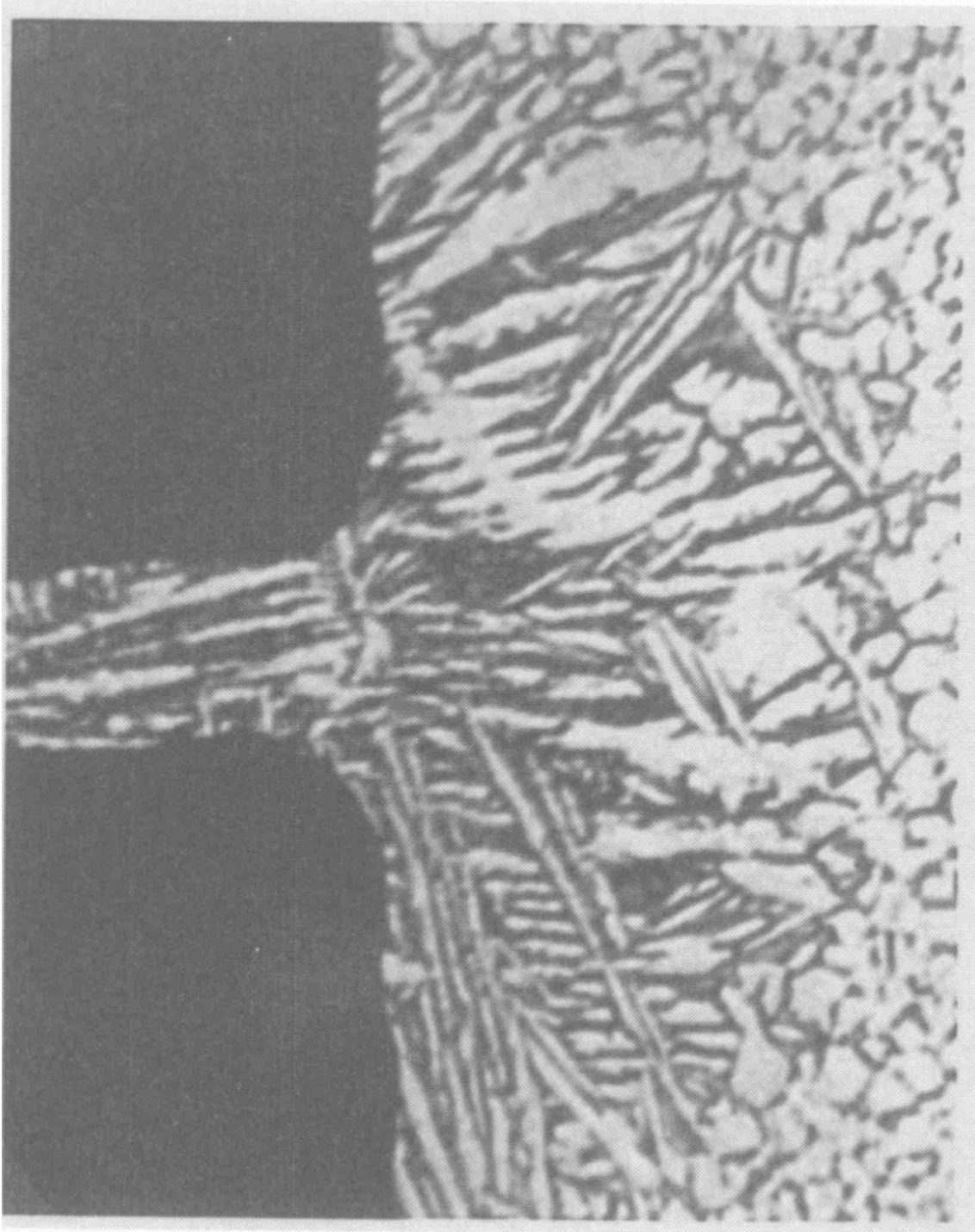


**Electrolytically
Plated
Copper
Film**



**Copper Layers
React with Ti
to form Eutectic
Brazing Alloy**

**Use Similar
Parameters as
Diffusion Weld**



Titanium Braze Plated Copper

A Widmanstaatten structure formed at the braze interface because the plated filler metal stabilized the beta phase.

Nickel Brazing

Braze Alloy

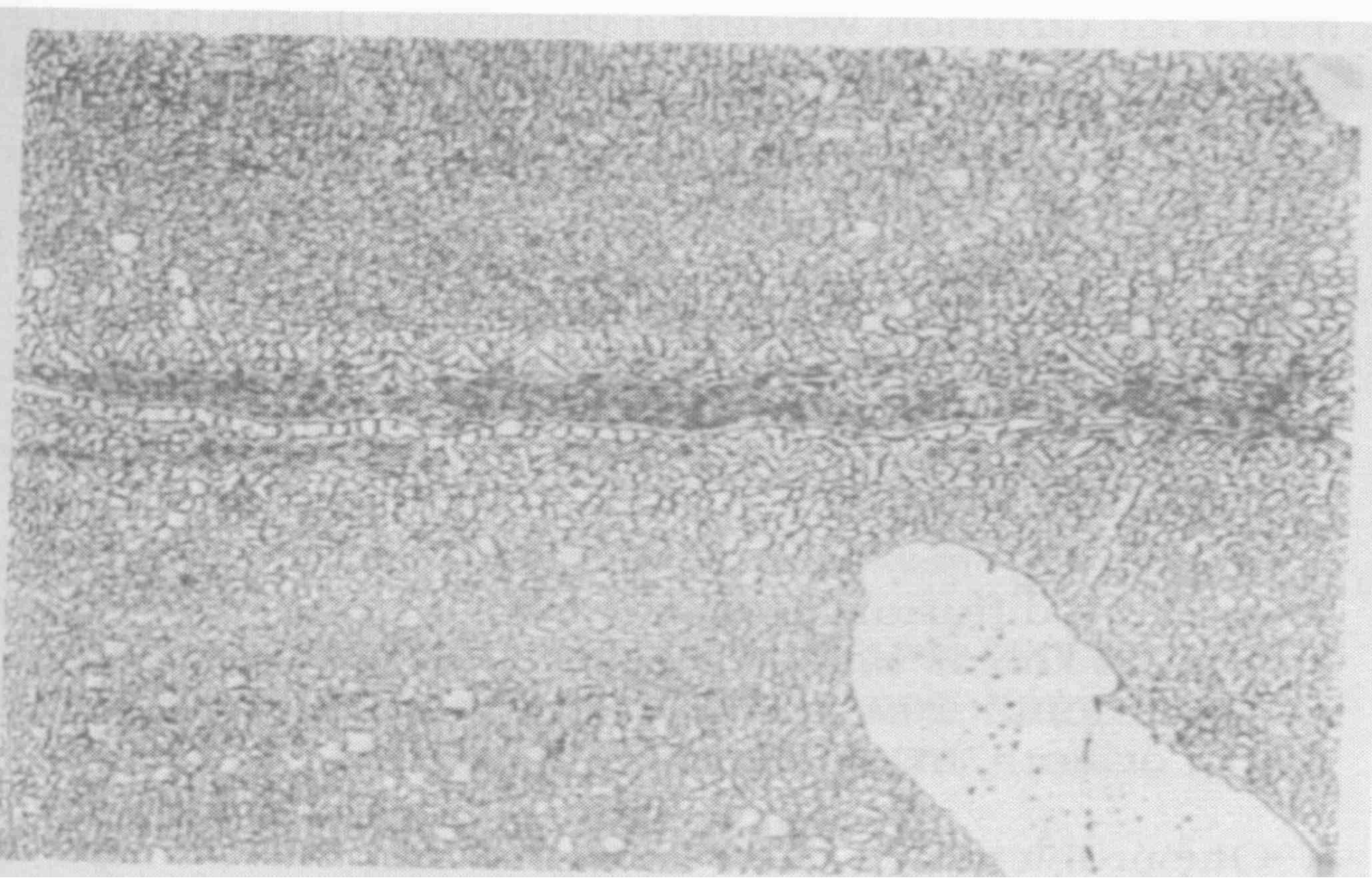
Nickel with melting Point Depressants (Silicon, Boron, Manganese, Aluminum, Titanium or Columbium)

Method 1

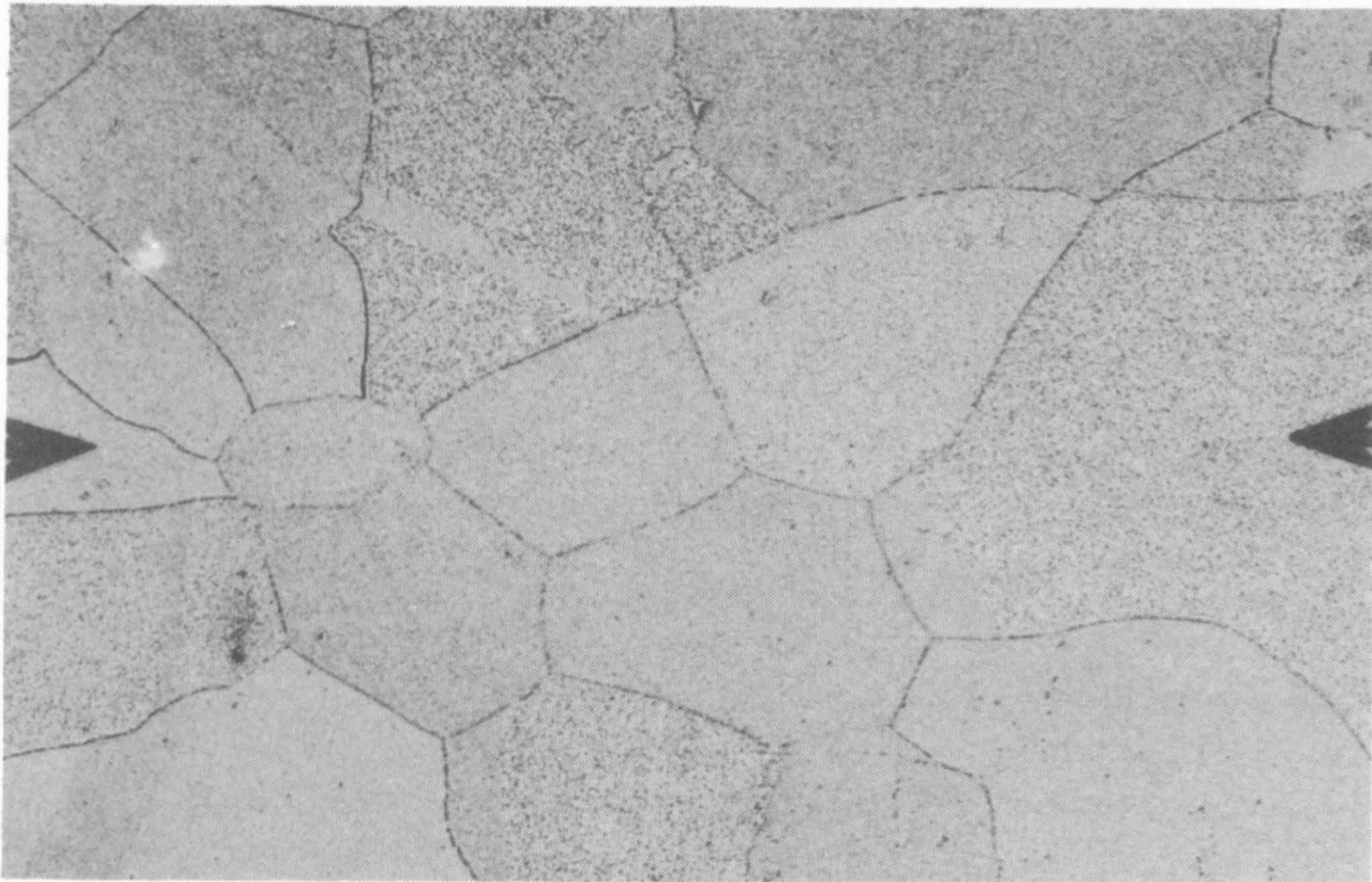


Method 2





Nickel Braze - Isothermal Solidification



Nickel Braze - Reheat for Diffusion

**Check Web Page For
Homework Assignment**