



THE ADSORBENTS NANOPOROUS STRUCTURES REGENERATION FOR INDUSTRIAL DRYERS BY MICROWAVE ENERGY

KHARKOV 2021

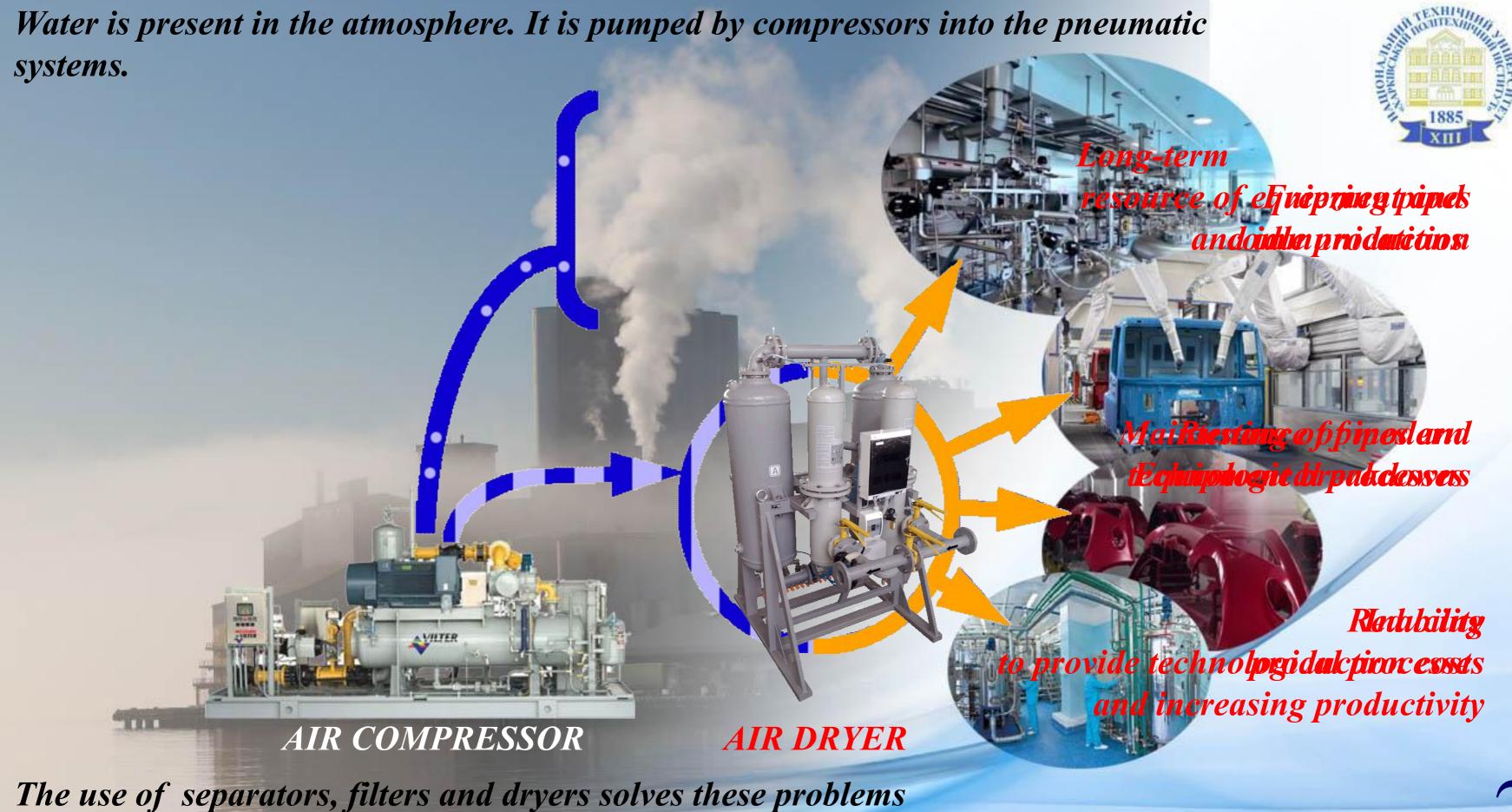
The main researches must be dedicated to a wider exploration of the means for reducing the atmospheric impact of other non-CO₂, gaseous emissions such as <u>water vapor</u>.



Aircraft running on hydrogen still emit water vapour and, in the case of hydrogen combustion, also NOx. On the other hand, particles may strongly be reduced.

The technology we propose can be used in the design of equipment that solves this problem.

As a consequence, high altitude phenomena have a substantial impact on the global impact of aviation on global warming through radiative forcing, may strongly be modified. Decreasing the level of this impact is crucial in order to increase the environmental potential of H_2 aircraft.



The reason for the significant consumption of electricity by compressors is due to the laws of thermodynamics.

WET AIR





Blowing purge air losses

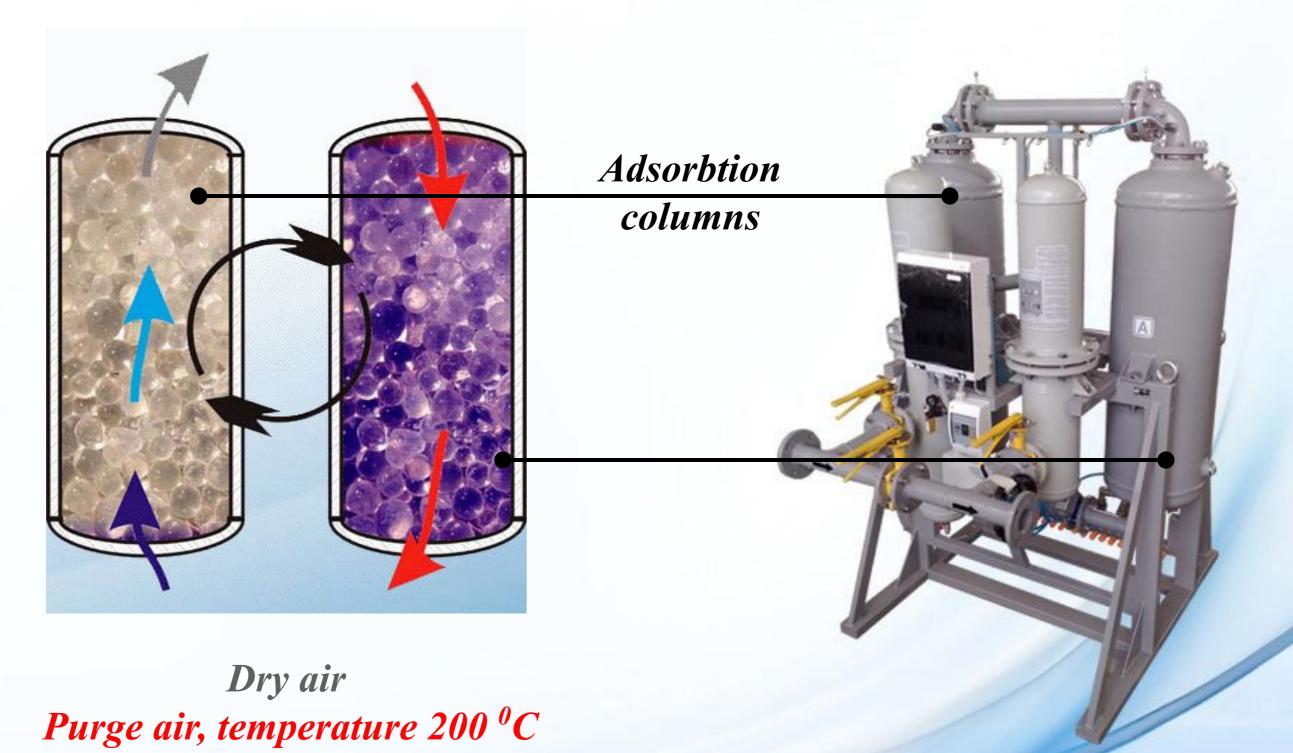
UP TO 20 % AIR LOST

Water removal losses

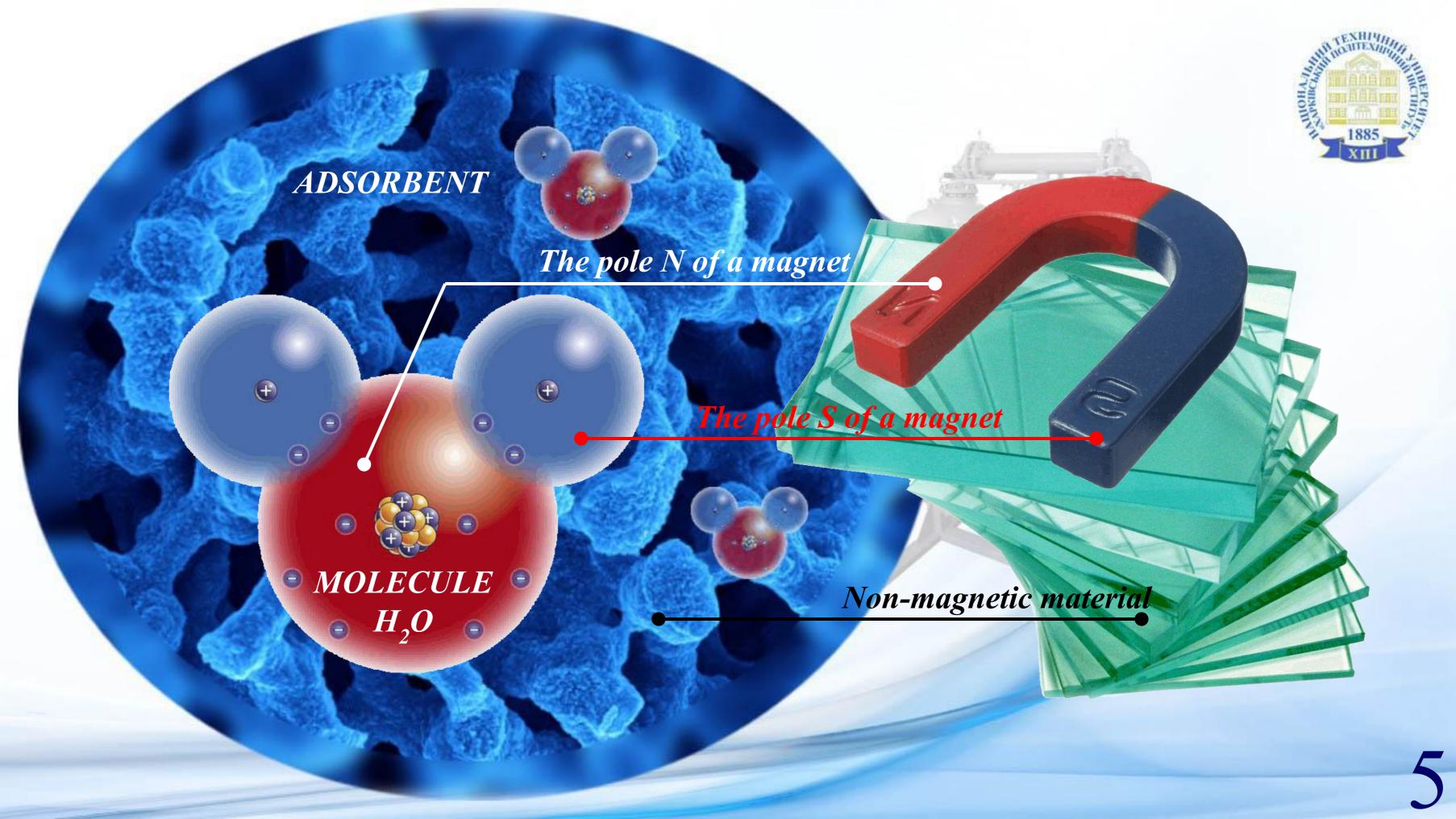
Reducing the amount of compressed air used to adsorbent regeneration is a challenge that must be addressed to reduce the cost of air production.

Adsorption columns of the dryer and their cyclic functioning.

Being dryed air



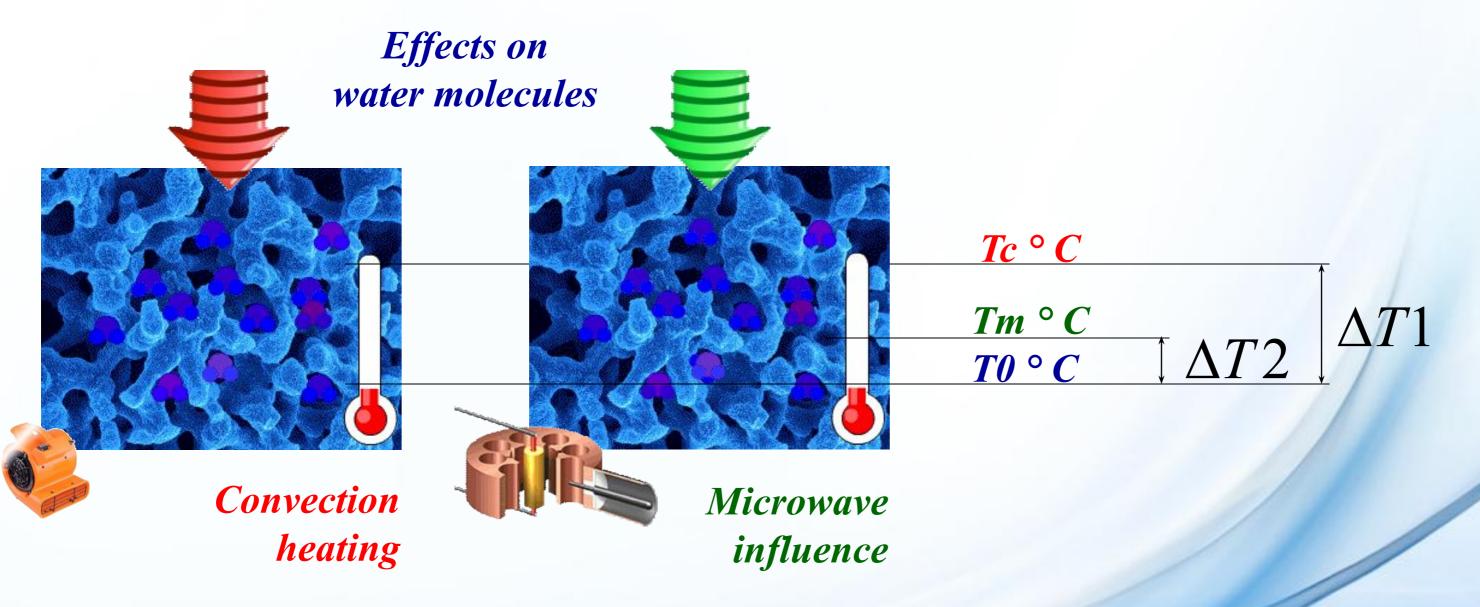
AIR DRYER



A <u>lower</u> heating temperature of the adsorbent requires a <u>smaller</u> volume of dried air to cool the adsorbent to the adsorption temperature



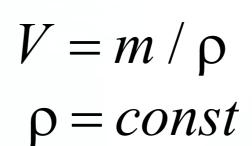
If the
$$H_{u_convection} = H_{u_microwave}$$

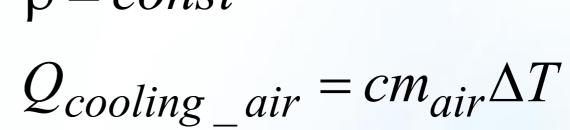


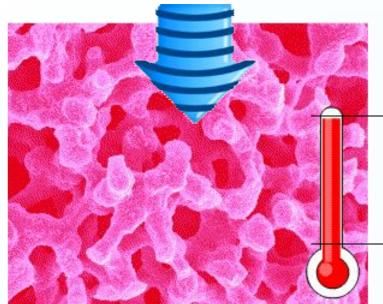
Then
$$\Delta T_{convection} > \Delta T_{microwave}$$

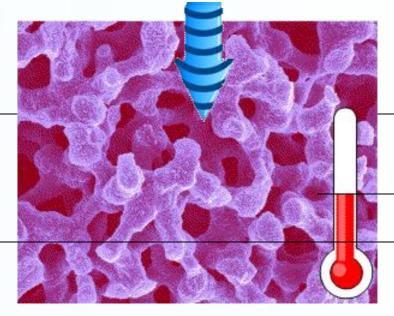
COOLING ADSORBENT STAGE











Tc ° *C*

$$Tm \circ C$$
 $T0 \circ C \qquad \uparrow \Delta T2$
 $\Delta T1$

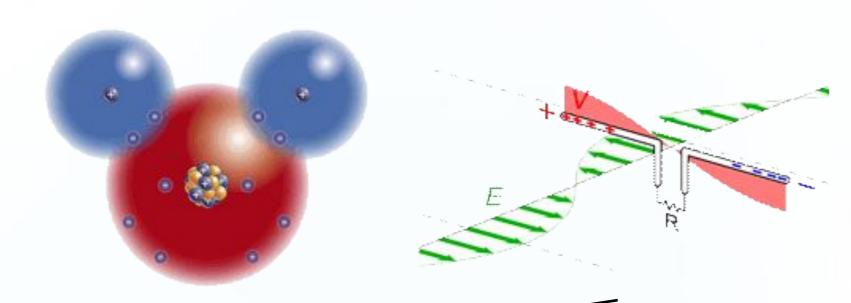
Convection heating

 $m_{air(convection)} > m_{air(microwave)}$



The action of high frequency radiation makes it possible to effect on water molecules directly.

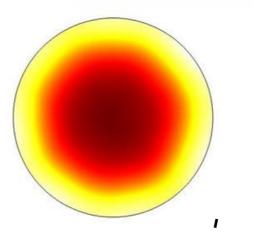


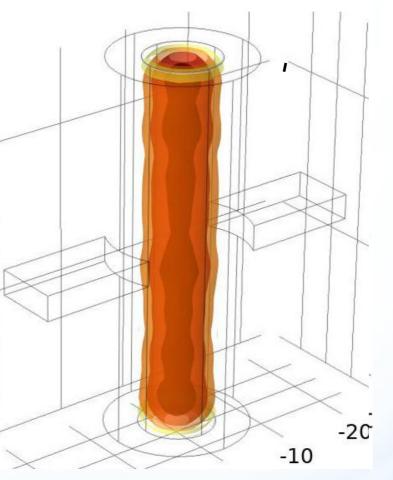


Electromagnetic field

Usually the impact is carried out using a magnetron, but this is uneven effect









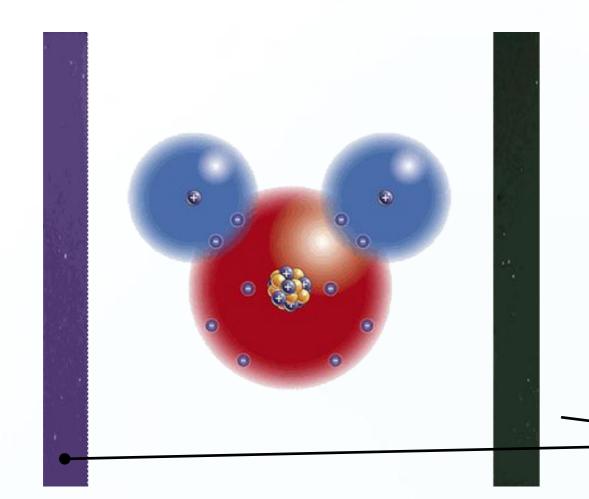
Overheating zone

We have improved the uniformity of the magnetron energy distribution in the adsorbent volume

The problem of using one or a group of magnetrons to regenerate a large volume of adsorbent is the limited depth of wave energy penetration into the bulk of the material

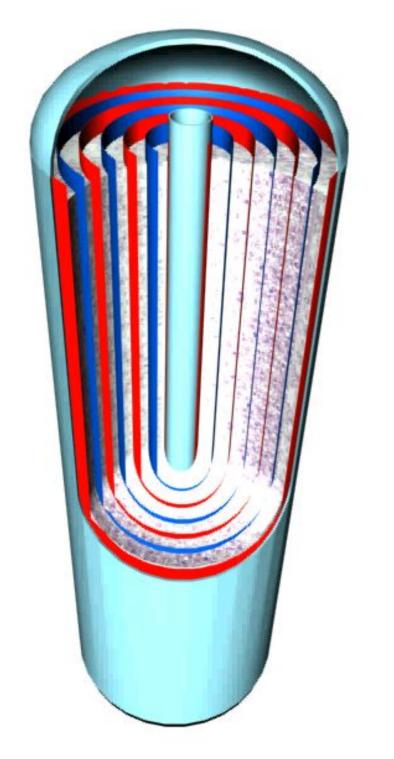
The action of high frequency radiation makes it possible to effect on water molecules directly.

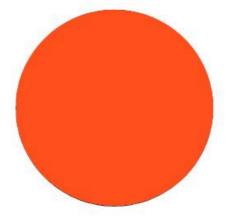


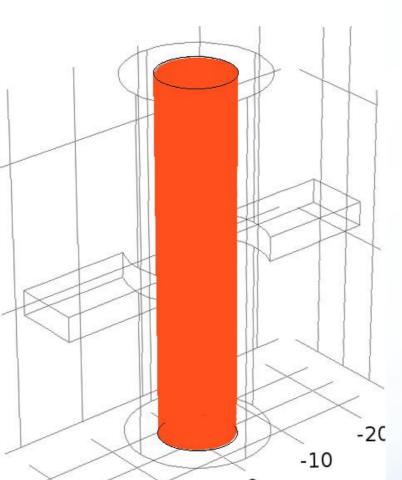


Pole plates

A similar effect can be achieved using pole plates







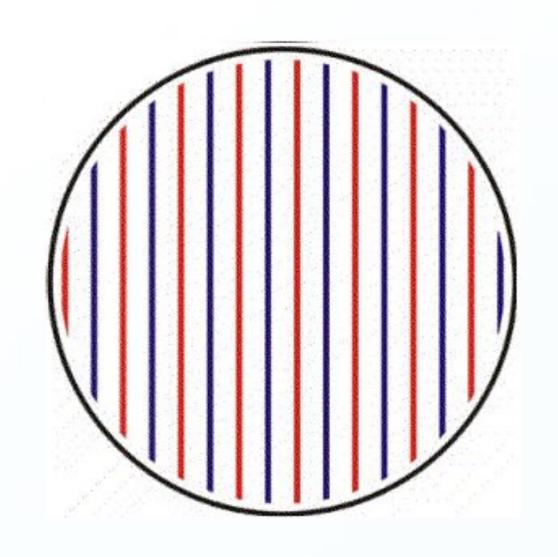


The technology we offer allows to achieve an even distribution of energy in large volumes and complex shapes

We propose to divide the entire volume of the adsorbent by parallel pole plates

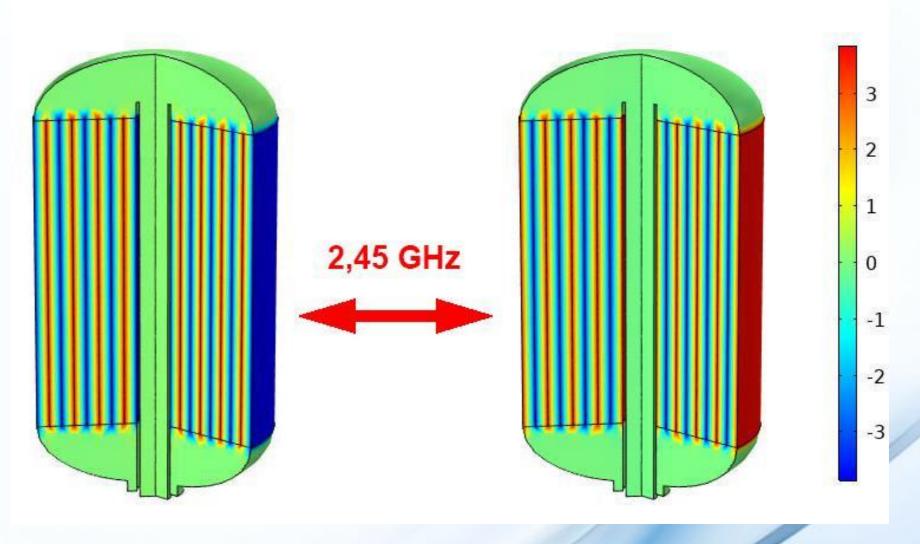
We study various Pole plate designs in terms of their placement in the volume of the adsorbent



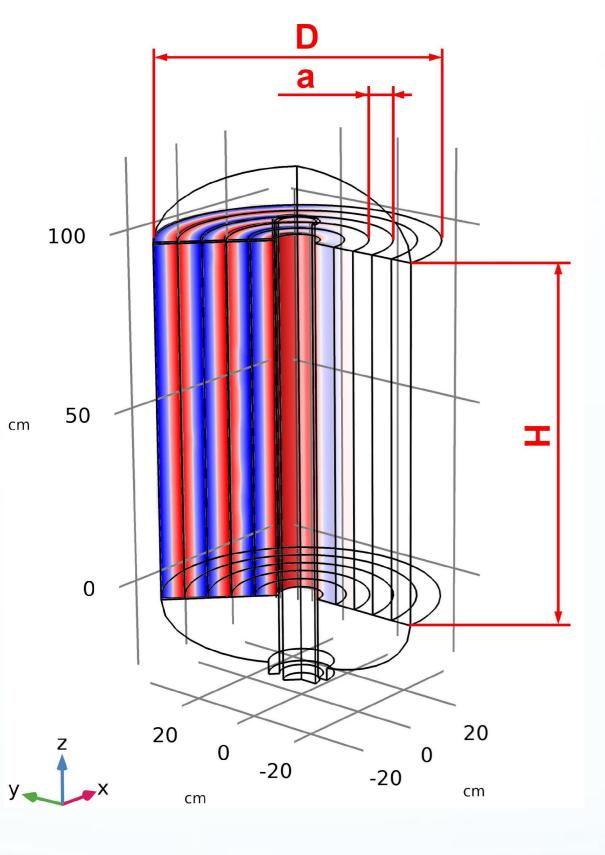


radial





Surface: Electric potential (V)

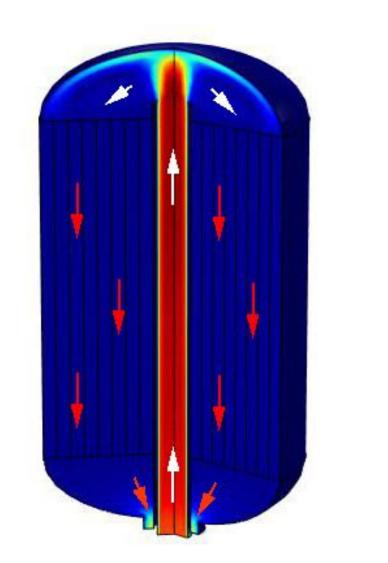


Our research was carried out on a computer model built by us with the following characteristics:



Dimension, mm:

Distance between the pole plates (a) 32/40/64 Column height (H) 1000 Column diameter (D) 760 Surface: Velocity magnitude (m/s)



Air velocity

The movement of air in the volume of the adsorbent was modeled as a motion in a porous medium.

$$\rho(u\mathfrak{g}\nabla)u = \nabla\bigg[-pl + \mu\bigg(\nabla u + \big(\nabla u\big)^T\bigg) - \frac{2}{3}\mu\big(\nabla\mathfrak{g}u\big)l\bigg] + F$$

$$\nabla g(\rho u) = 0$$

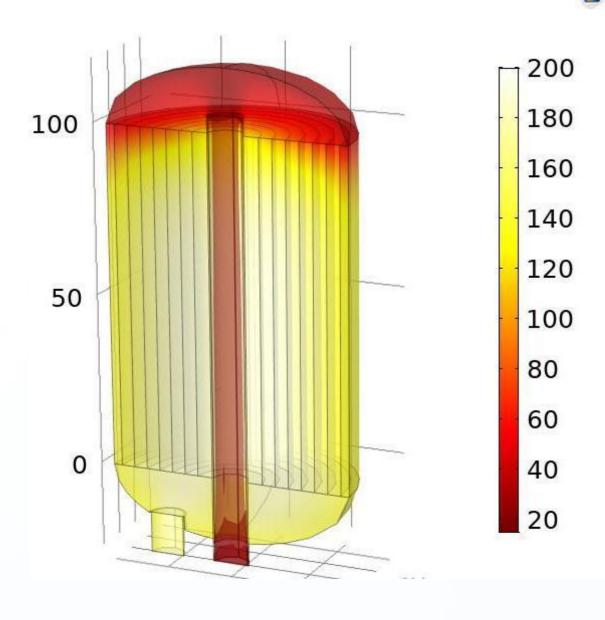
0.8

0.6

0.4

$$\frac{1}{\grave{o}_{p}}\rho\left(\mathsf{ugV}\right)\mathsf{u}\frac{1}{\grave{o}_{p}} == \nabla \left[-p\mathsf{l} + \mu \frac{1}{\grave{o}_{p}} \left(\nabla \mathsf{u} + \left(\nabla \mathsf{u}\right)^{\mathsf{T}}\right) - \frac{2}{3}\mu \frac{1}{\grave{o}_{p}} \left(\nabla \mathsf{gu}\right)\mathsf{l}\right] - \left(\mu k^{-1} + \beta_{F} \left|\mathsf{u}\right| \frac{\theta_{m}}{\grave{o}_{p}^{2}}\right)\mathsf{u} + F$$

$$\nabla \mathbf{g}(\rho u) = Q_m$$



Temperature

The influence of purge air flow on thermal processes in the column is calculated as dynamic heat transfer model

$$\begin{split} \rho C_p \, \frac{\partial T}{\partial t} + \rho C_p v_{trans} \, \mathbf{g} \! \nabla T + \nabla \mathbf{g} \! \eta &= Q + Q_{ted} \\ \rho C_p \mathbf{u} \mathbf{g} \! \nabla T + \nabla \mathbf{g} \! \eta &= Q + Q_{vd} \\ q &= -k_{e\!f\!f} \, \nabla T \end{split}$$

The heating of the adsorbent due to the effect of alternating voltage

$$\rho C_p u g \nabla T = \nabla g (k \nabla T) + Q_e$$

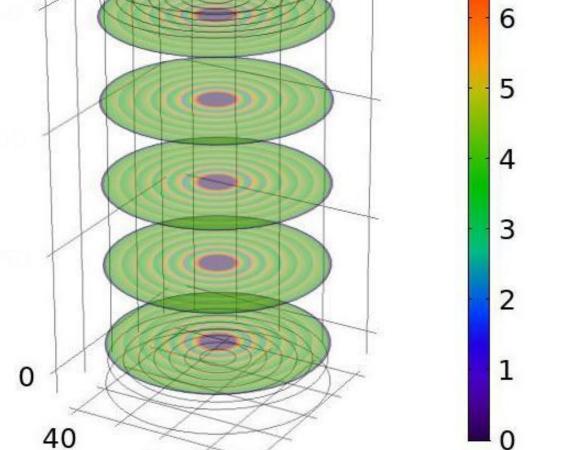
$$Q_e = JgE$$

The electric field generated in adsorbent volume

$$\nabla \times (\mu_{\gamma}^{-1} \nabla \times E) - k_0^2 \left(\varepsilon_{\gamma} - \frac{j\sigma}{\omega \varepsilon_0} \right) E = 0$$

$$\nabla g J = Q_{j,v}$$

$$J = \sigma E + j\omega D + J_{\rho} \qquad \omega = 2\pi f$$



 $\times 10^4$

cm

-40

40

Electric field

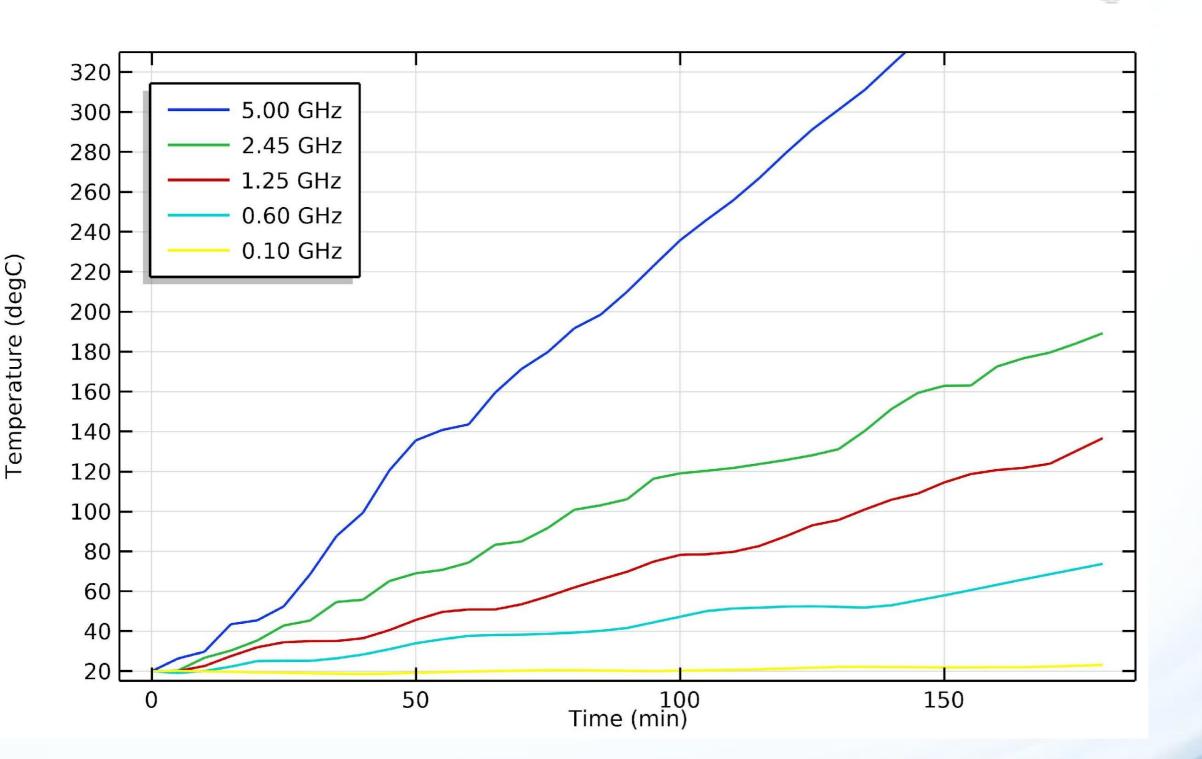
The force, which is affects on the water molecule

$$\overline{F} = \overline{\rho} \, \mathbf{g} \overline{E}$$

$$E = \frac{U}{d}$$

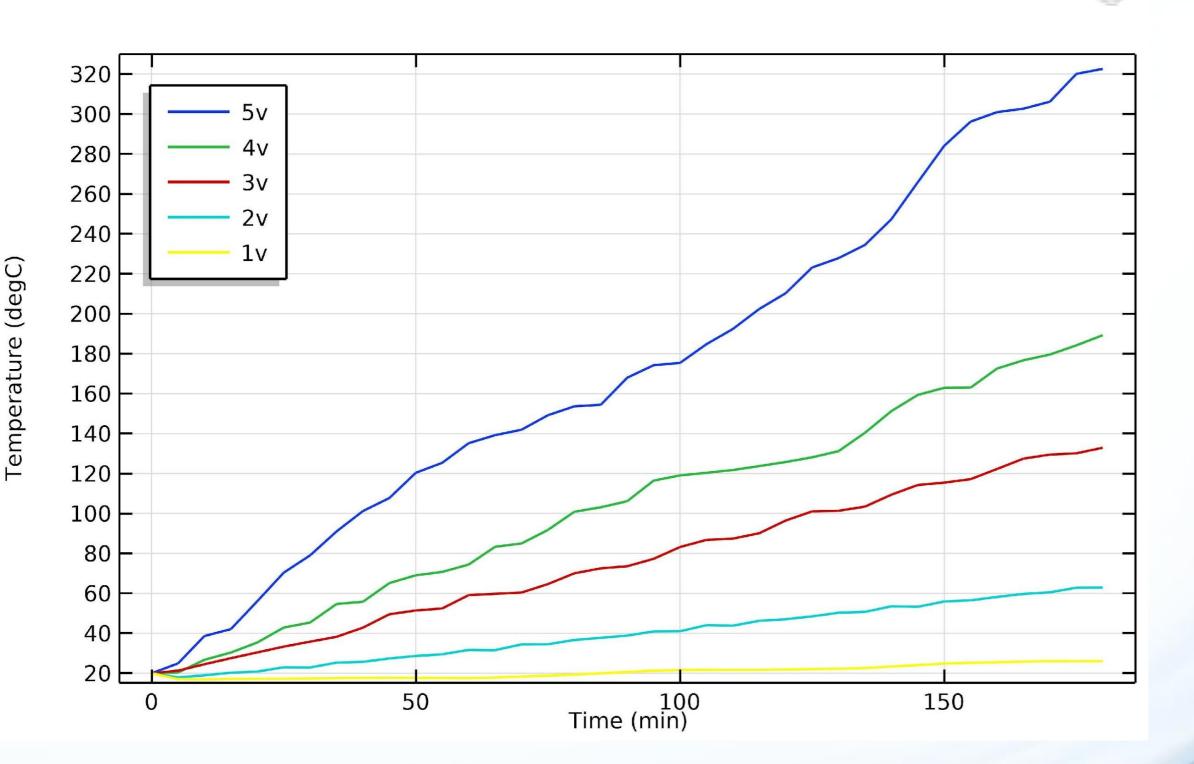
$$F = \sum_{i} \frac{\partial \overline{E}}{\partial x_{i}} \rho_{i}$$

$$E = -\nabla V$$



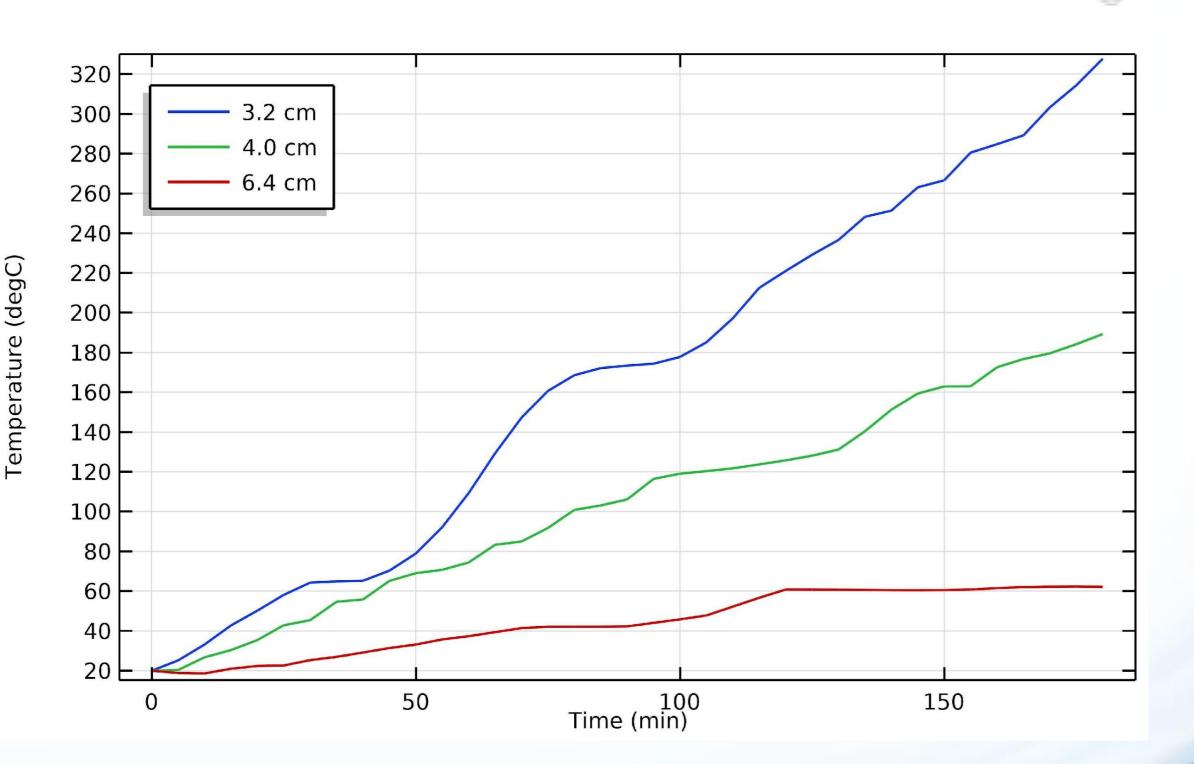
TING THE WAR T

The dependence of the heating intensity of exposure to microwave frequency [GHz]



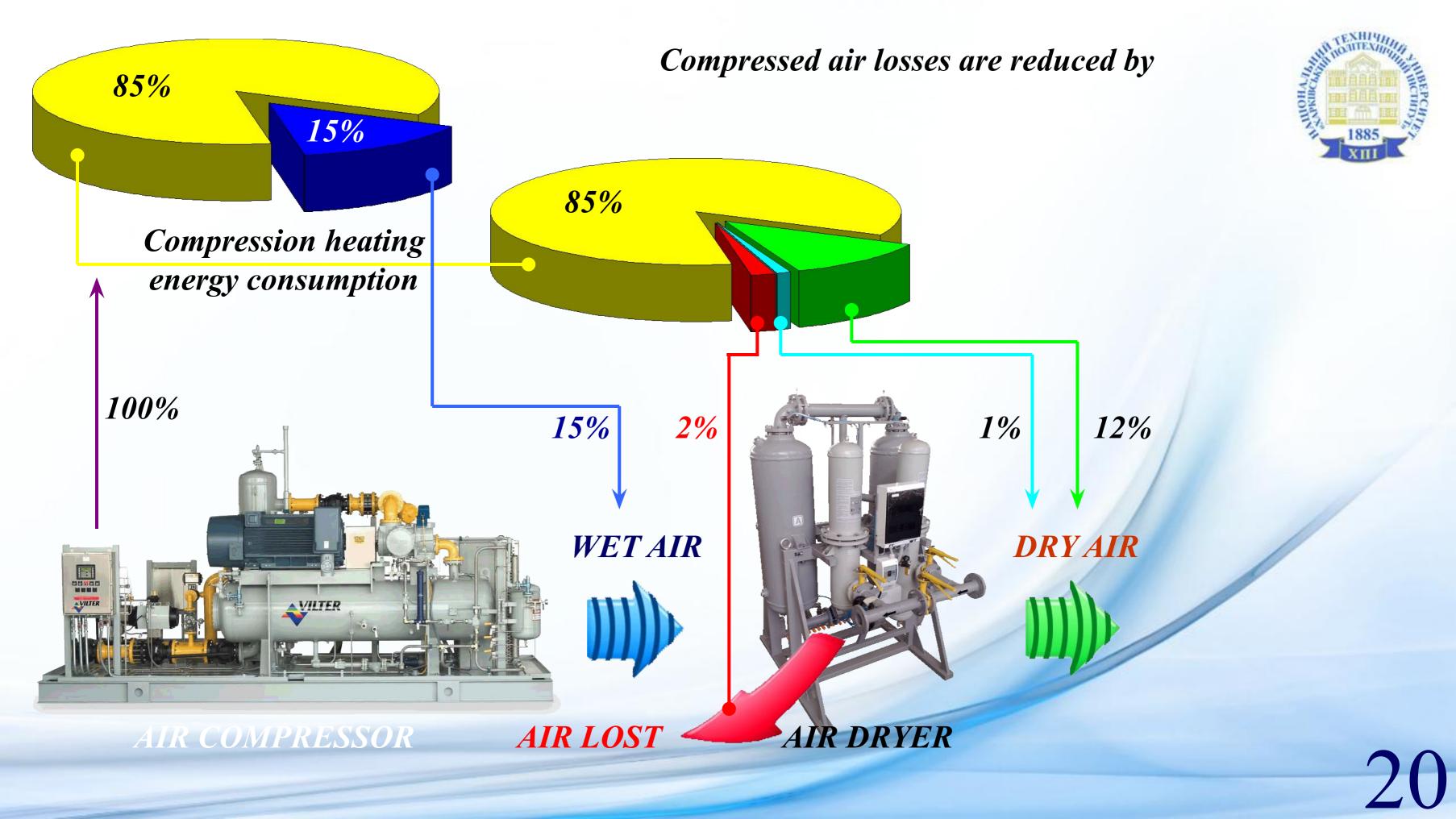


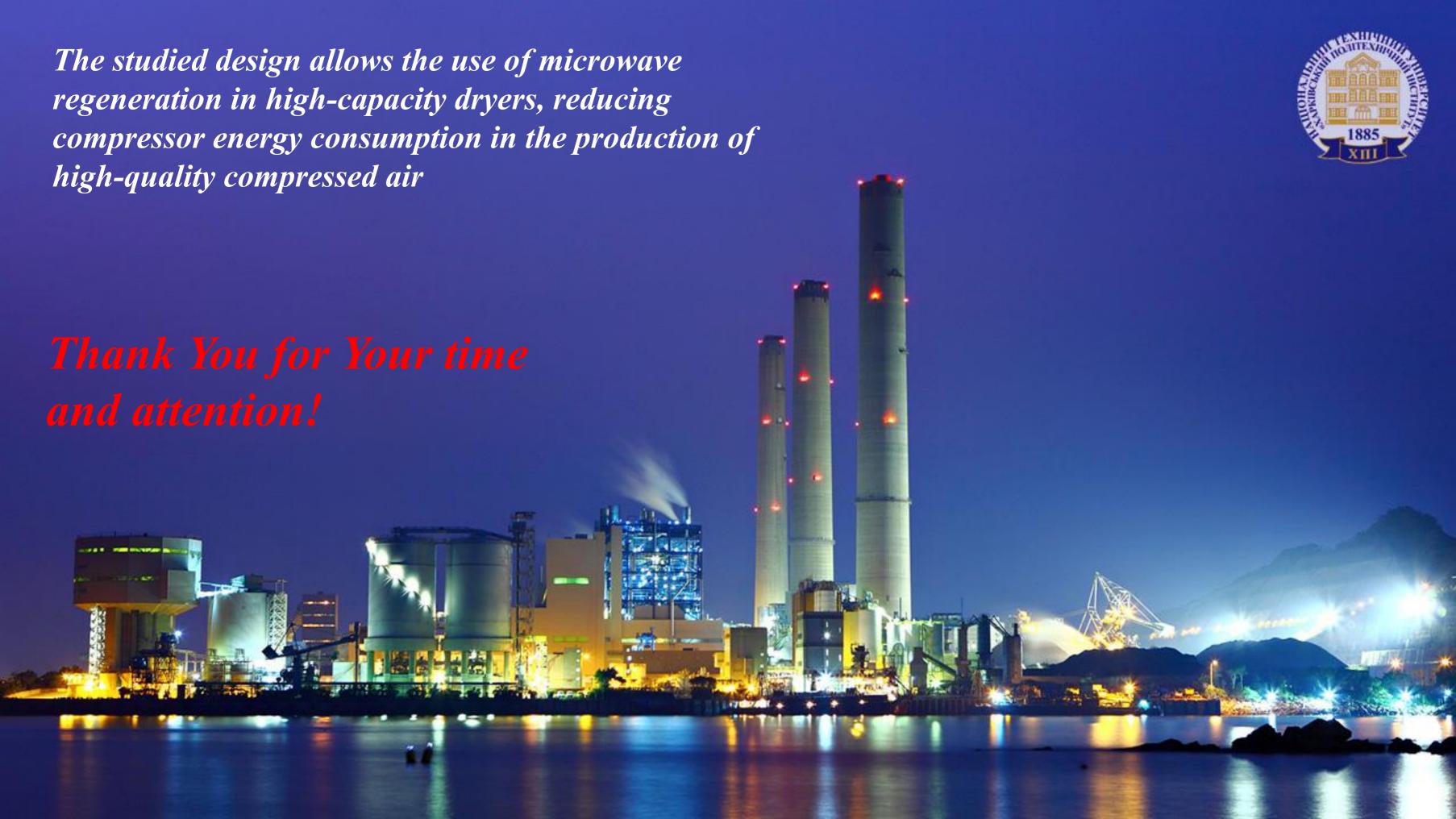
The dependence of the intensity of microwave exposure on the peak voltage on the pole plates [V]



The dependence of the intensity of microwave exposure on the distance between the pole plates [cm]











Kharkov Polytechnic Institute

Sergey Dobrotvorskiy sdobro50@gmail.com www.kpi.kharkov.ua

Aleksenko Borys A Vitalii Yepifanov Yevheniia Basova Ludmila Dobrovolska Viktor Popov