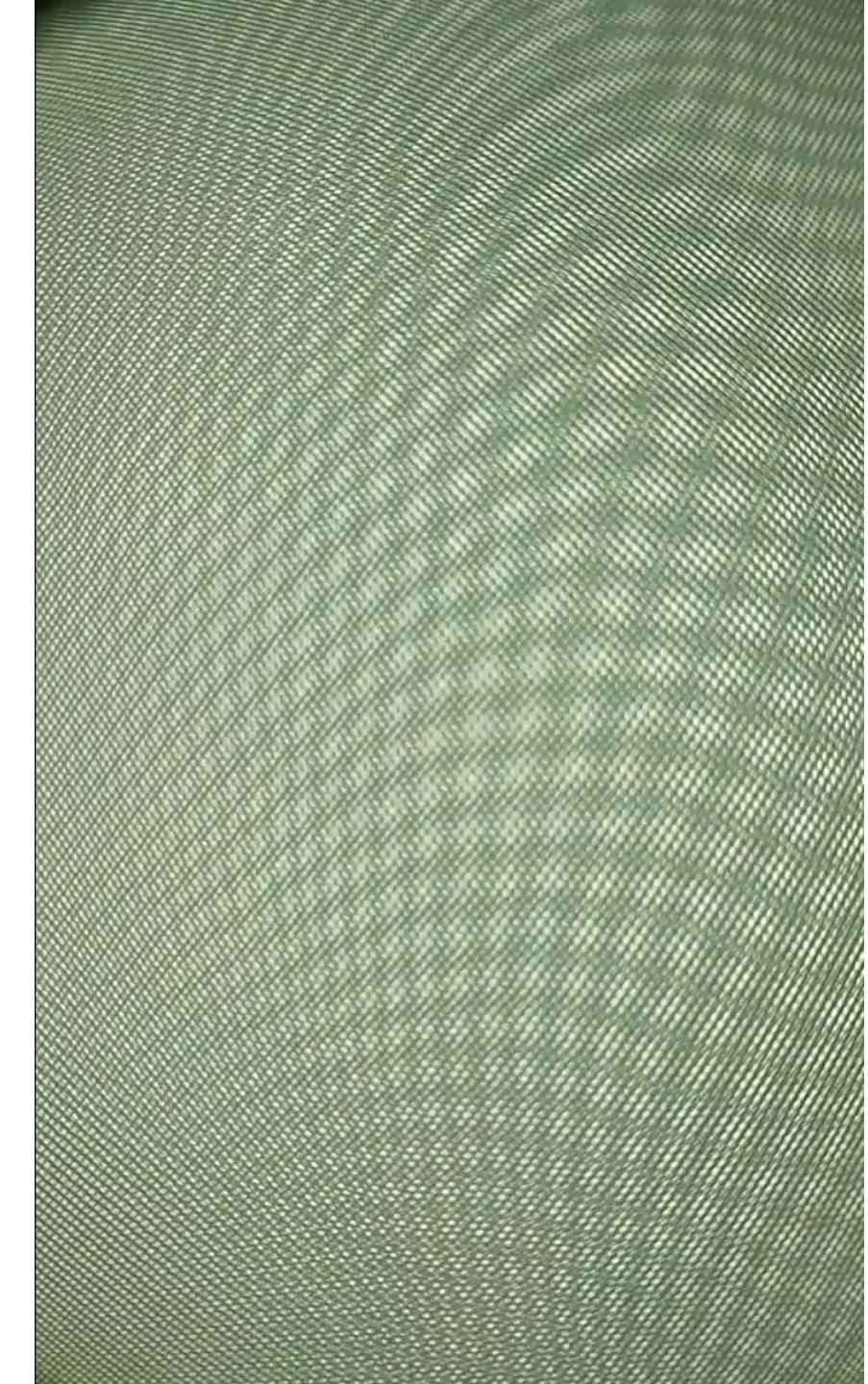


Problem № 13

“Moiré Thread Counter”

When a pattern of closely spaced **non-intersecting** lines (with transparent gaps in between) is overlaid on a piece of woven fabric, characteristic **moiré fringes** may be observed. Design an **overlay** that allows you to measure the **thread count** of the fabric. Determine the **accuracy** for simple fabrics (e.g. linen) and investigate if the method is **reliable for more complex fabrics** (e.g. denim or Oxford cloth).

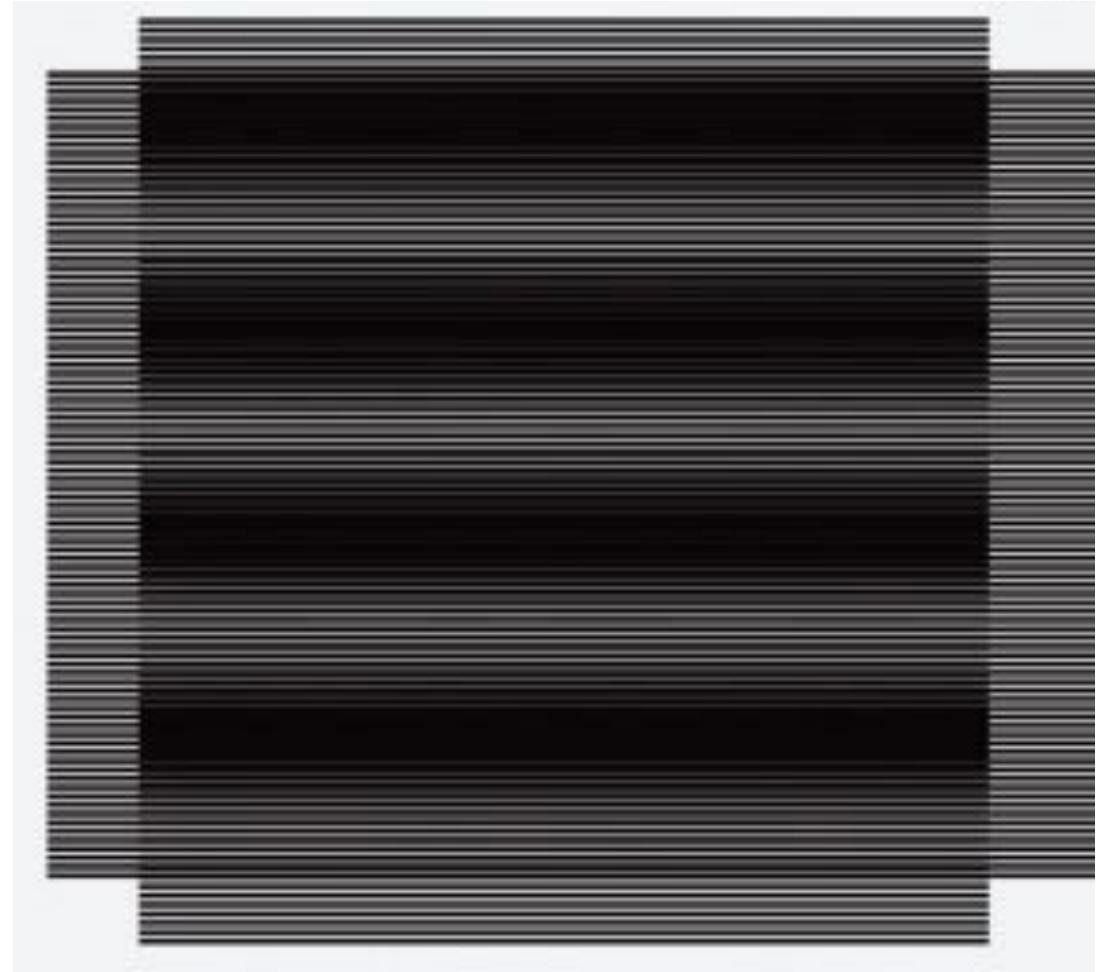
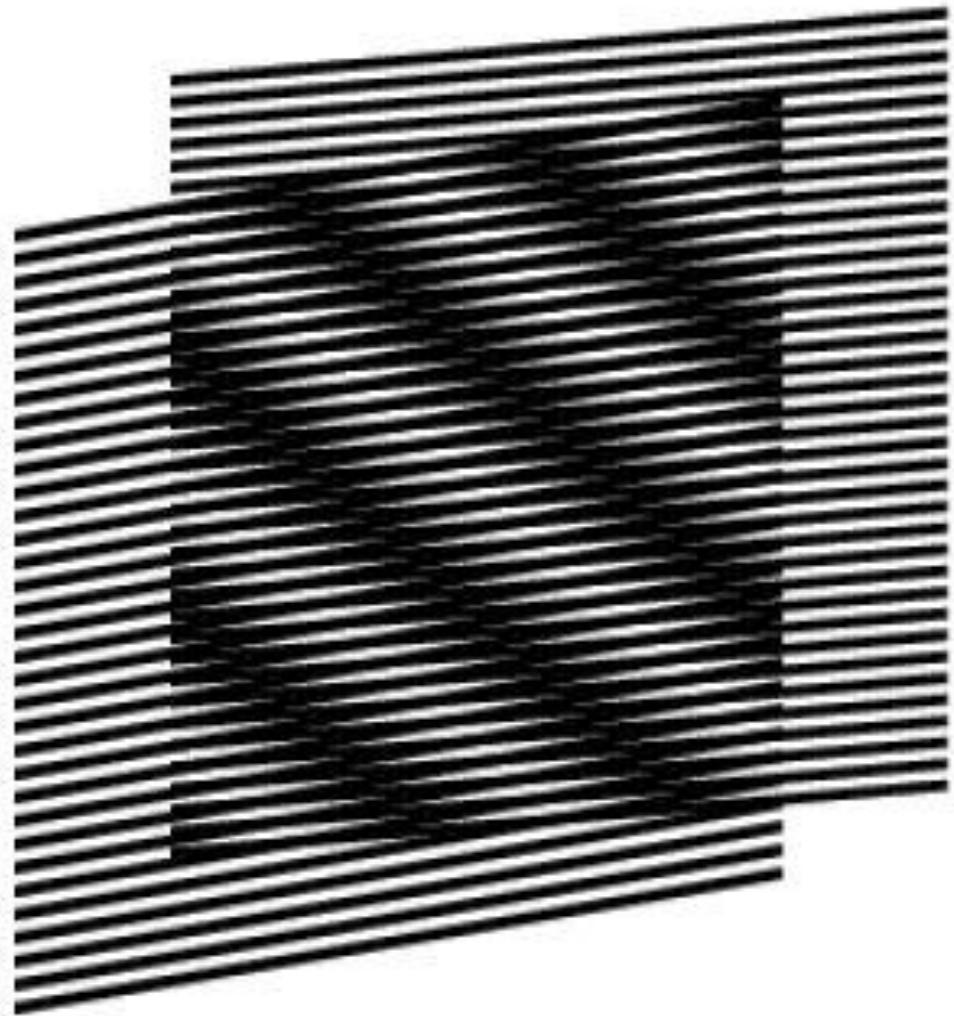


Team Russia

Reporter: Nika Gribova

Basic concept

Moiré pattern is a **pattern** that occurs when two periodic grids are overlapped.



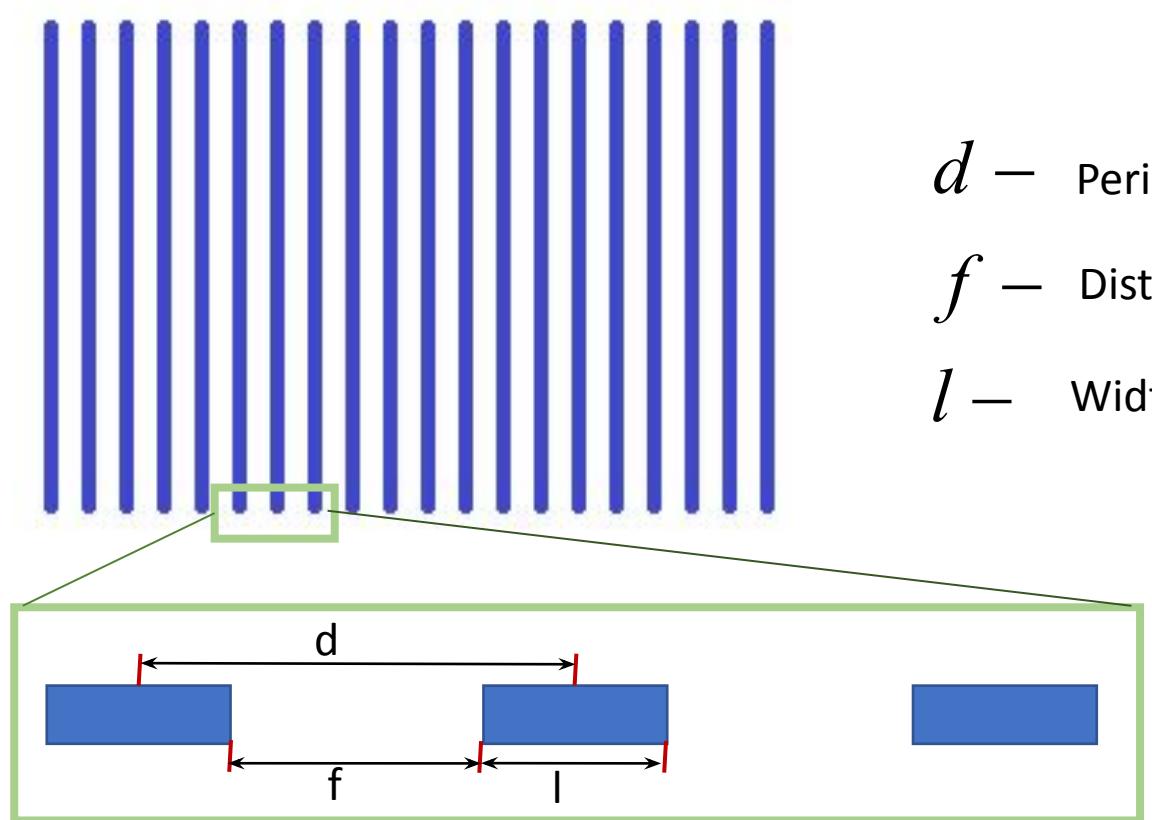
Review

Theoretical model

- Basic concepts(grid, period)
- Qualitative explanation of the moiré's pattern
- Geometric moiré
- Determination of the formula's accuracy
- Mathematical model and special cases
- Experimental comparison(direct and indirect measurement)
 - calculate the number of threads
 - Checking our method for complex fabric
 - dependences(period of the moiré pattern on angle and overlay's period)

Basic concepts

grid

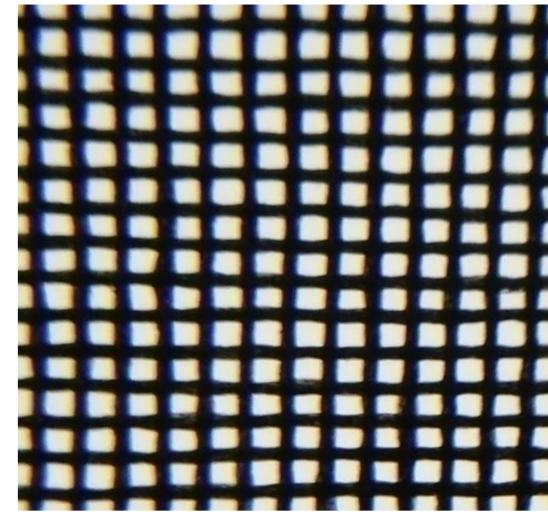
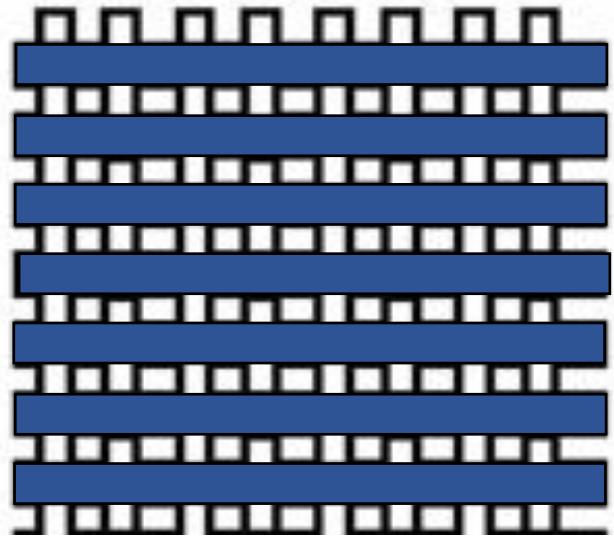


$$d = f + l$$

d — Period of fabric

f — Distance between the threads

l — Width of the thread

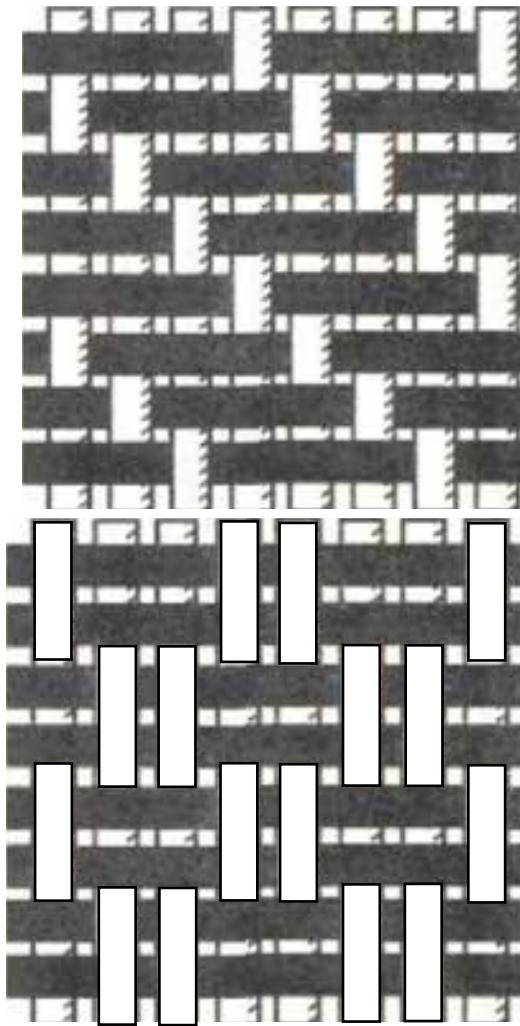
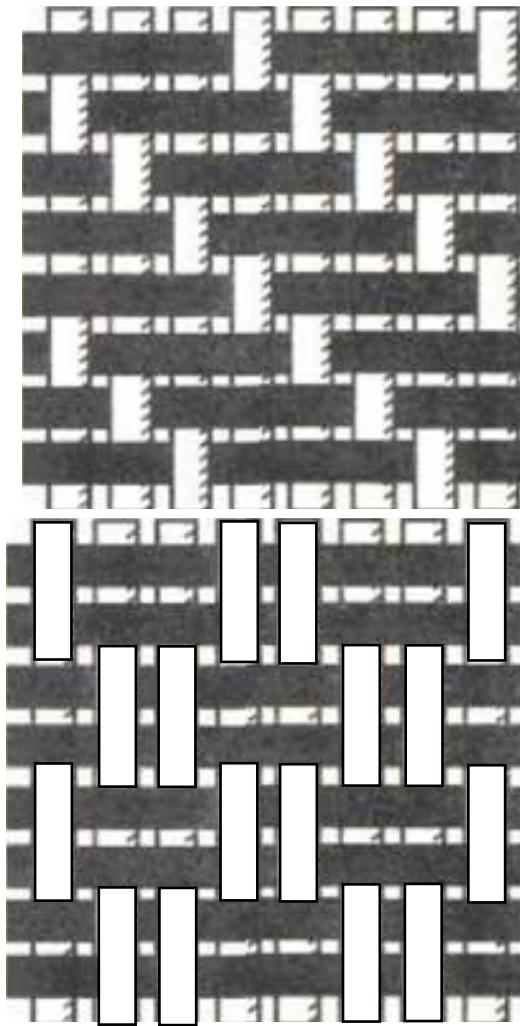


Complex weave

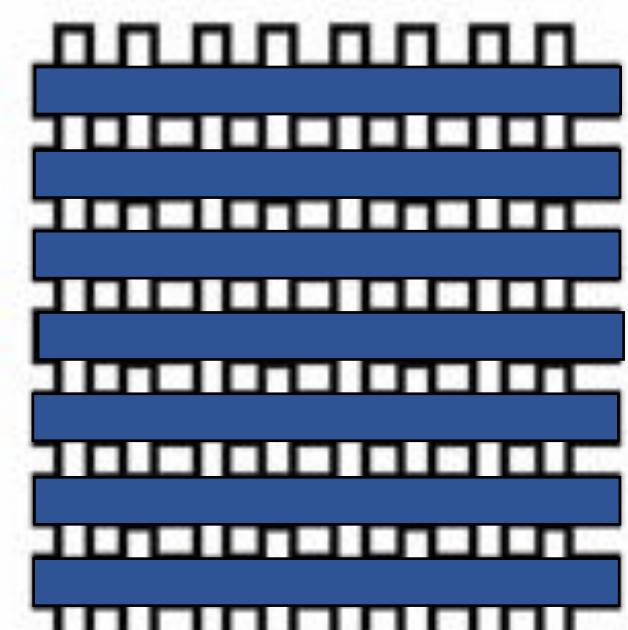
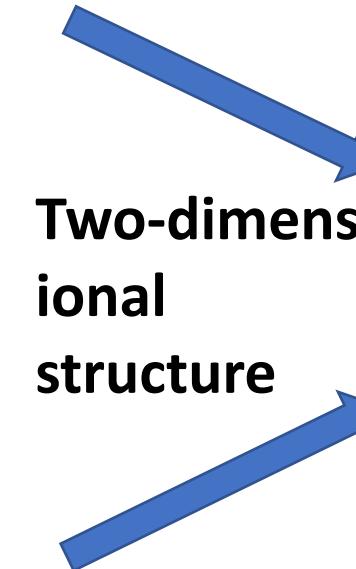
Denim (jeans fabric)



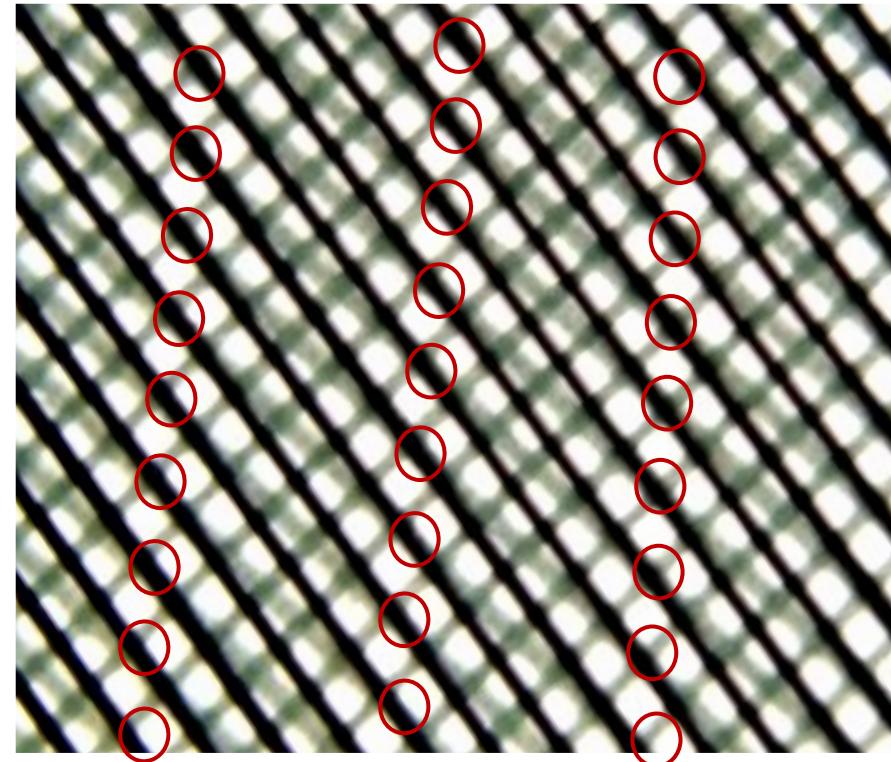
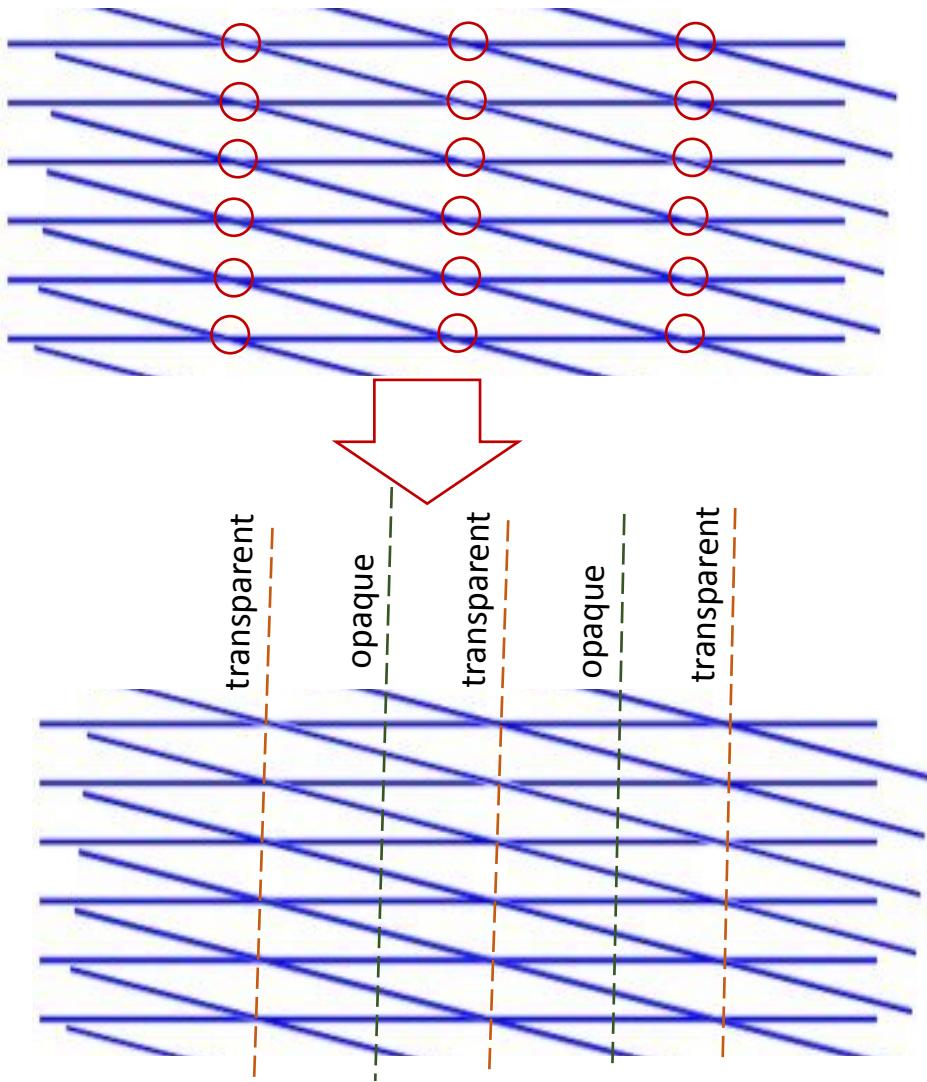
Fabric «Oxford»



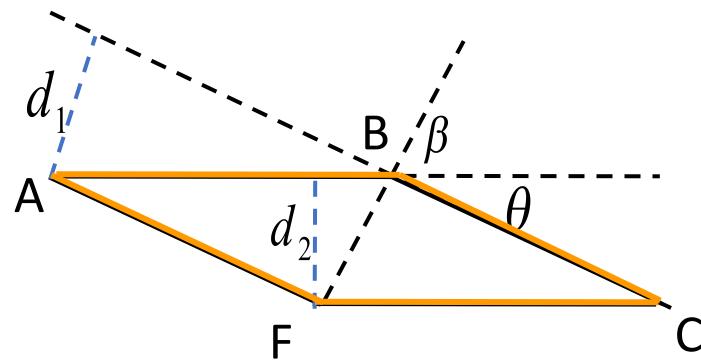
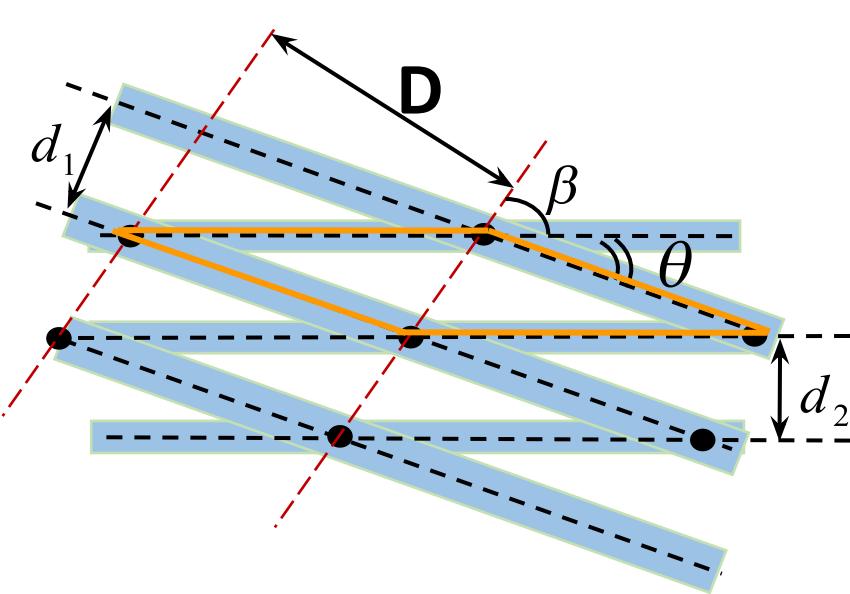
Two-dimensional
structure



Quality explanation

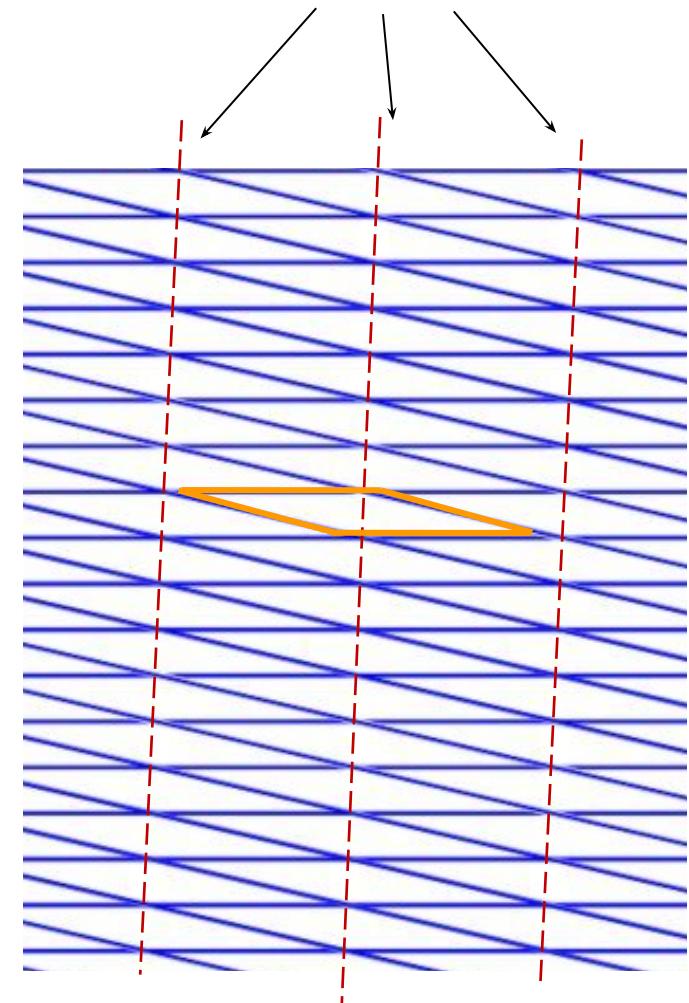


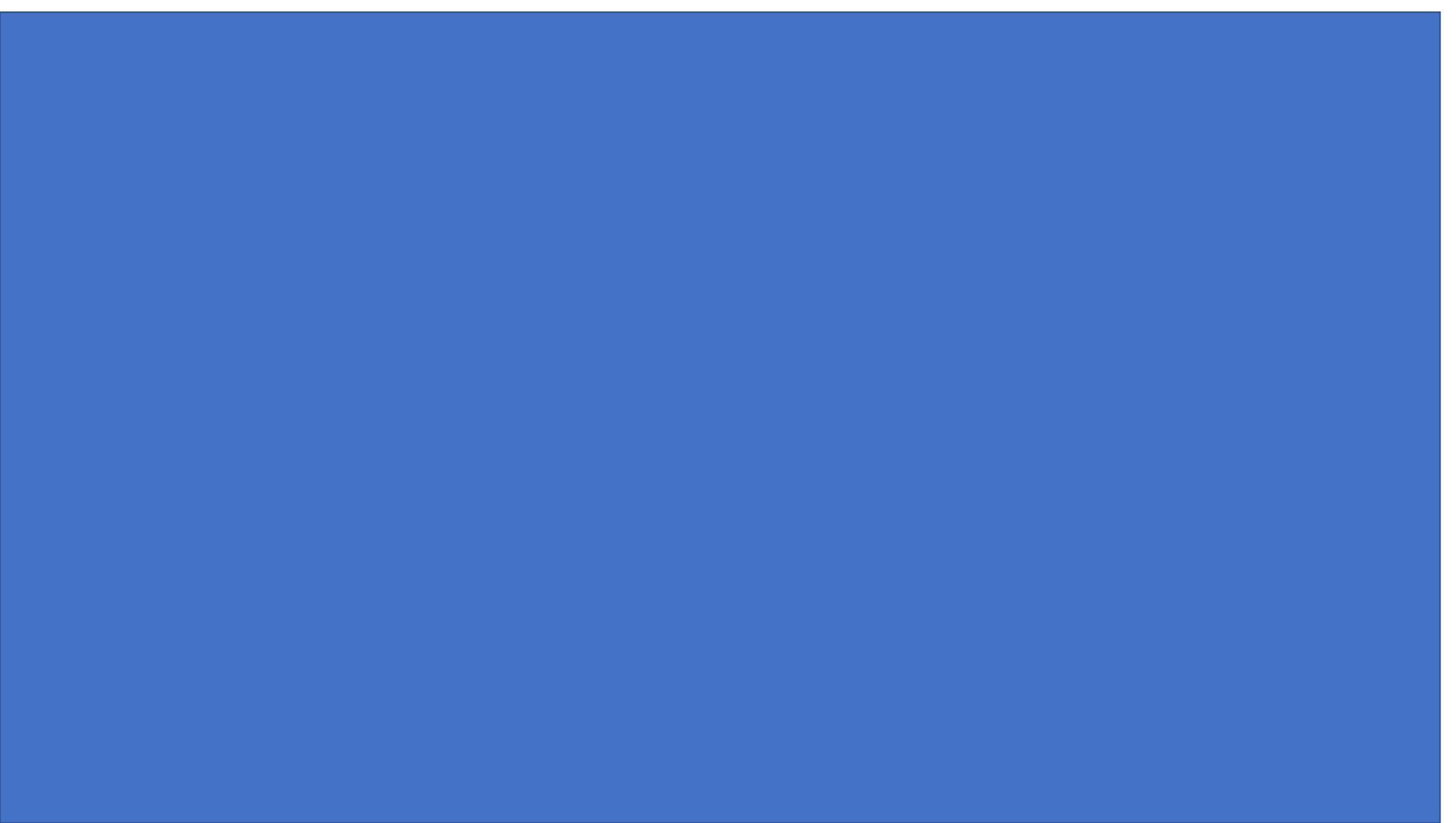
Geometric Moiré



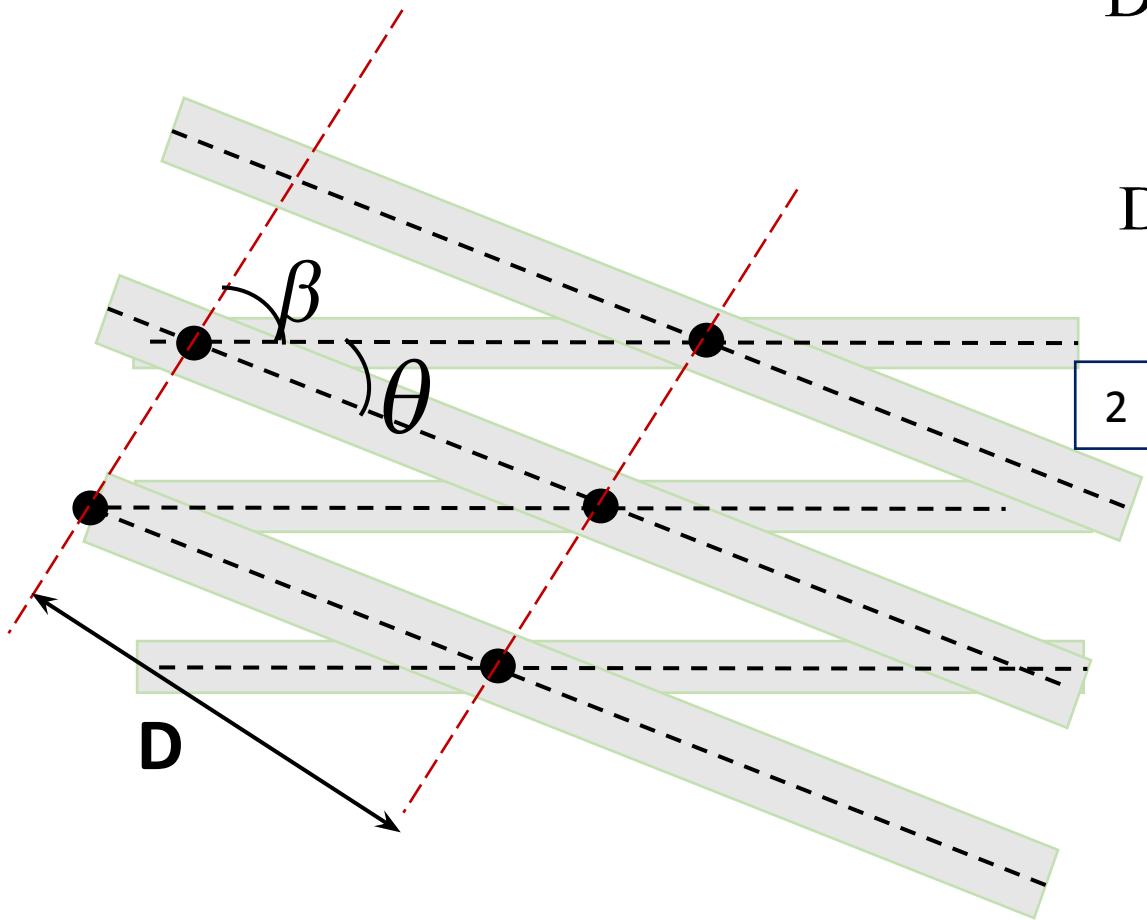
$$D = \frac{d_1 \cdot d_2}{\sqrt{d_1^2 + d_2^2 - 2 \cdot d_1 \cdot d_2 \cdot \cos \theta}}$$

Transparent lines





Special case



1 $\theta = 0$

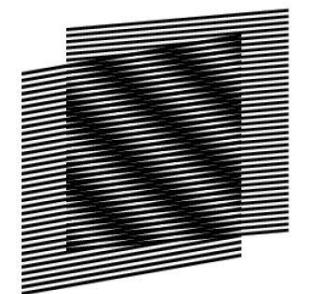
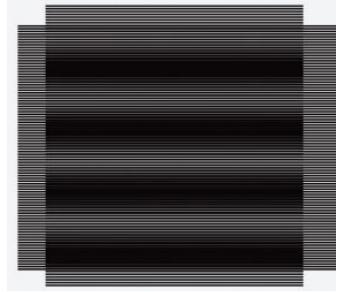
$$D = \frac{d_1 d_2}{\sqrt{d_1^2 + d_2^2 - 2d_1 d_2 \cos 0^\circ}}$$

$$D = \frac{d_1 d_2}{|d_1 - d_2|}$$

2 $d_2 = d_1$

$$\cos \beta = -2 \cdot \sin^2 \frac{\beta}{2} + 1$$

$$D = \frac{d}{\left| 2 \sin \frac{\beta}{2} \right|} \quad n = \frac{1}{2D \cdot \left| \sin \frac{\beta}{2} \right|}$$

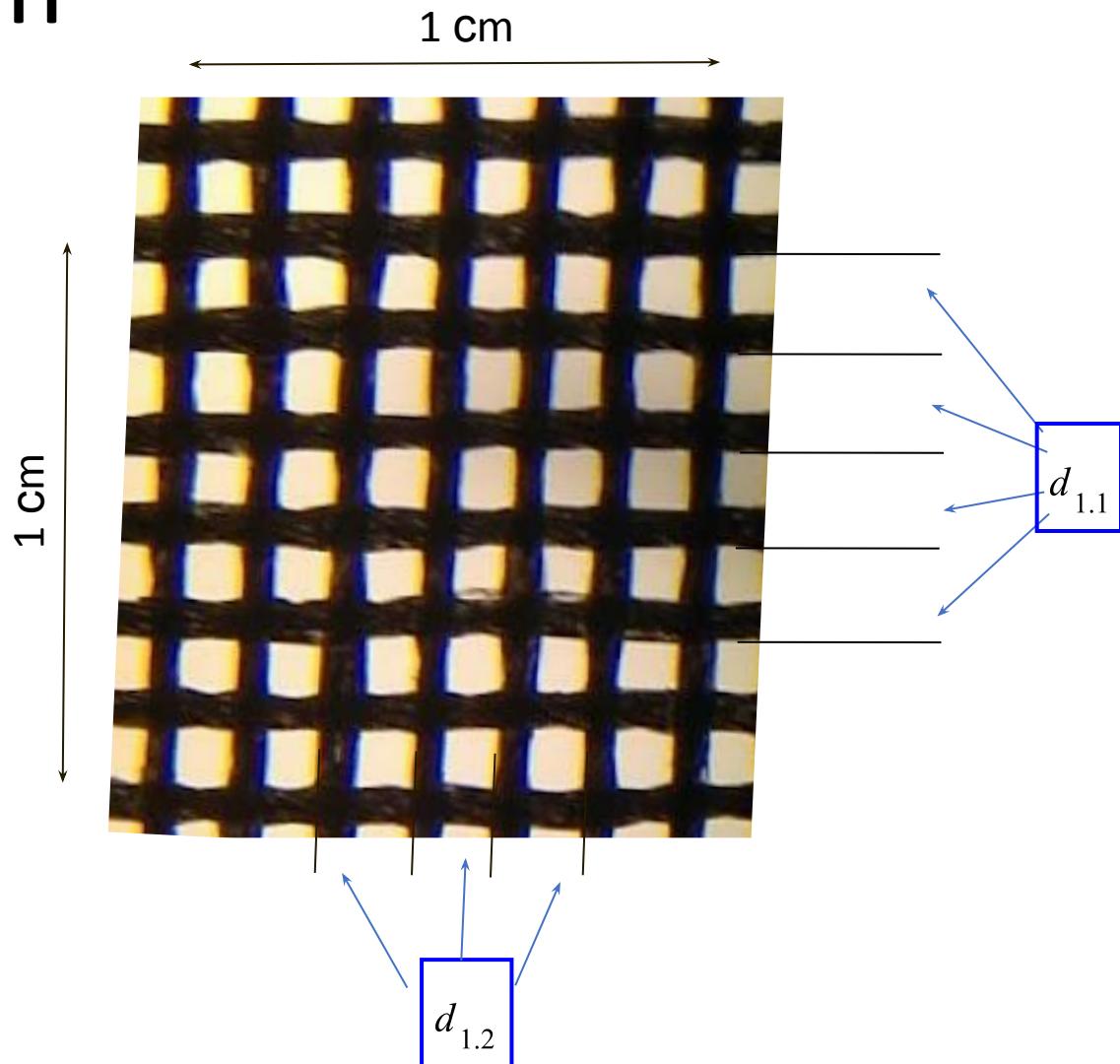


Number of threads per 1 cm

$$n_1 = \frac{1}{d_1} \cdot cm^{-1}$$

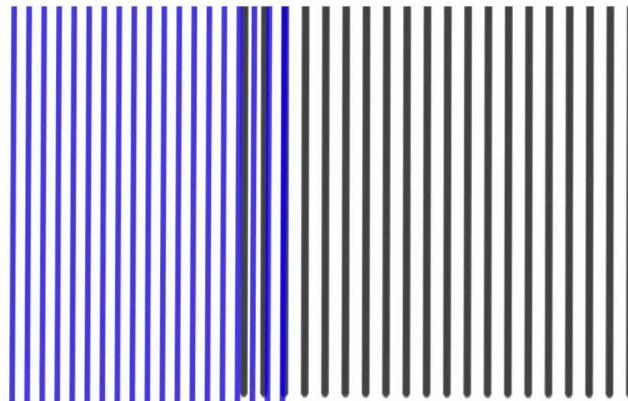
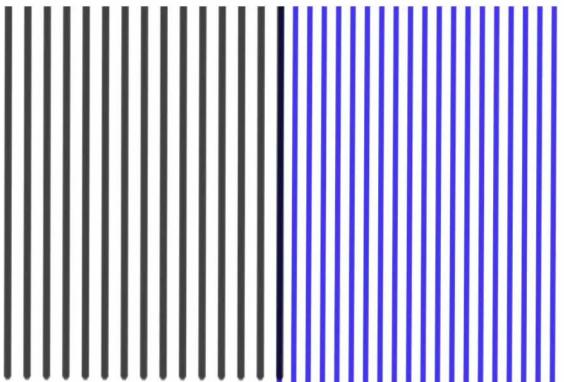
$$D = \frac{\frac{1}{n_1} \cdot d_2}{\sqrt{\frac{1}{n_1^2} + d_2^2 - \frac{2 \cdot d_2 \cdot \cos \theta}{n_1}}}$$

$$n_1(\theta, D, d_2) = \frac{D \cos \theta \pm \sqrt{d_2^2 - D^2 \sin^2 \theta}}{d_2 D}$$

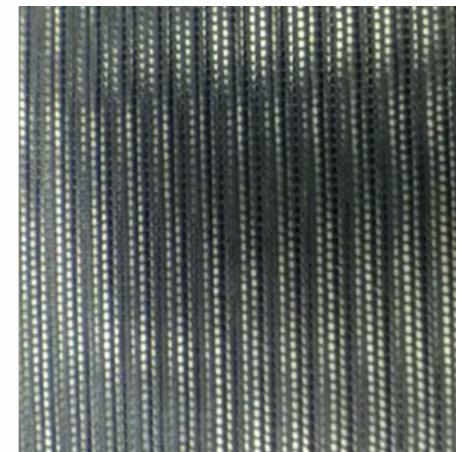




Fabric with less period



Fabric with bigger period

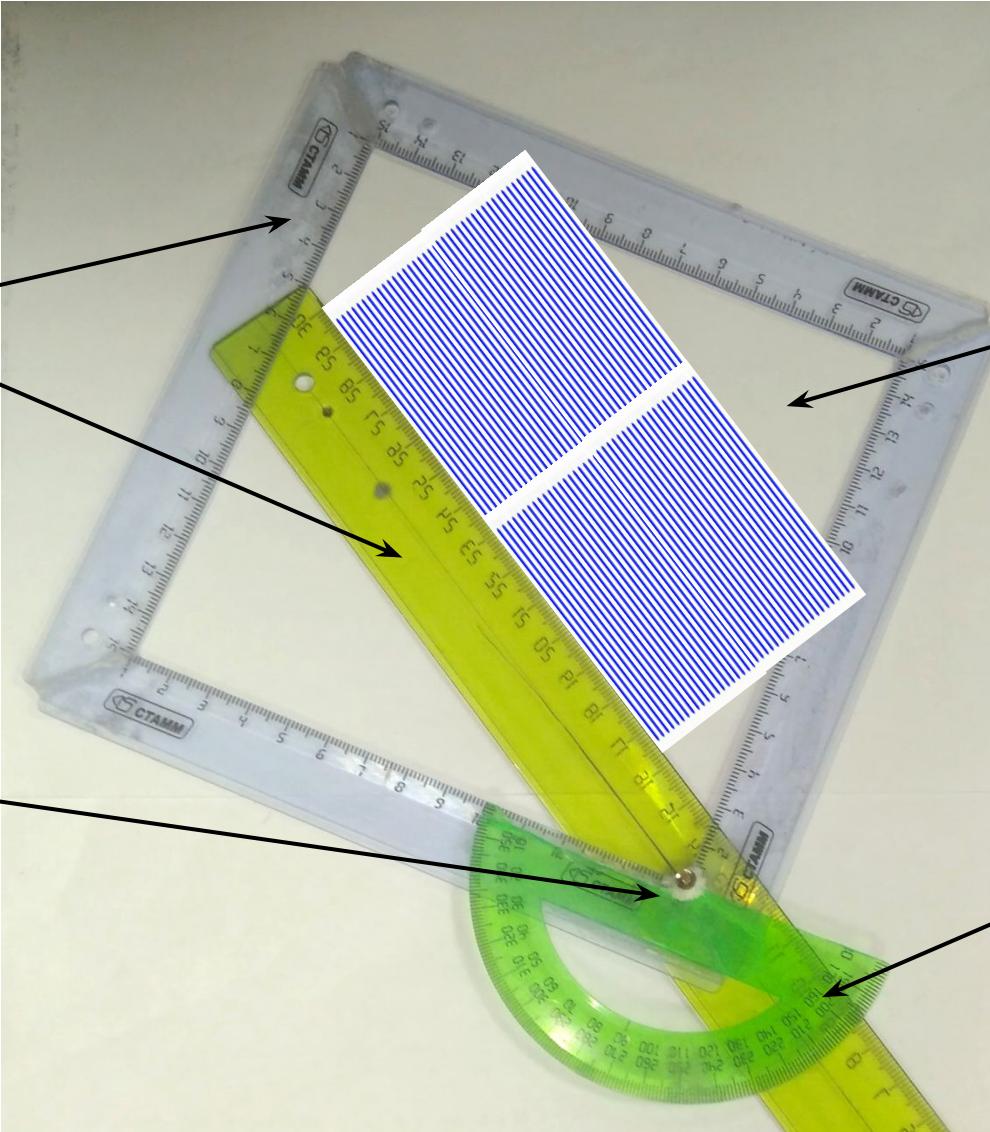


$$n_1(\theta, D, d_2) = \frac{D \cos \theta - \sqrt{d_2^2 - D^2 \sin^2 \theta}}{d_2 D}$$

Experimental set-up

rulers

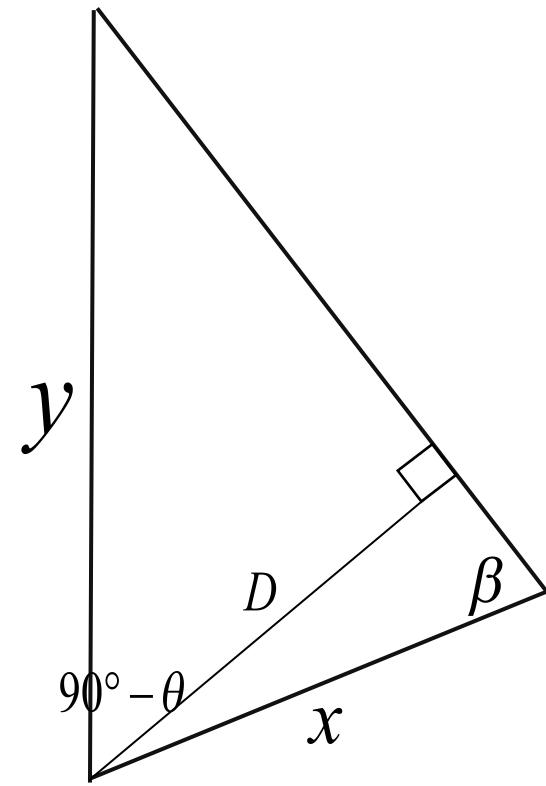
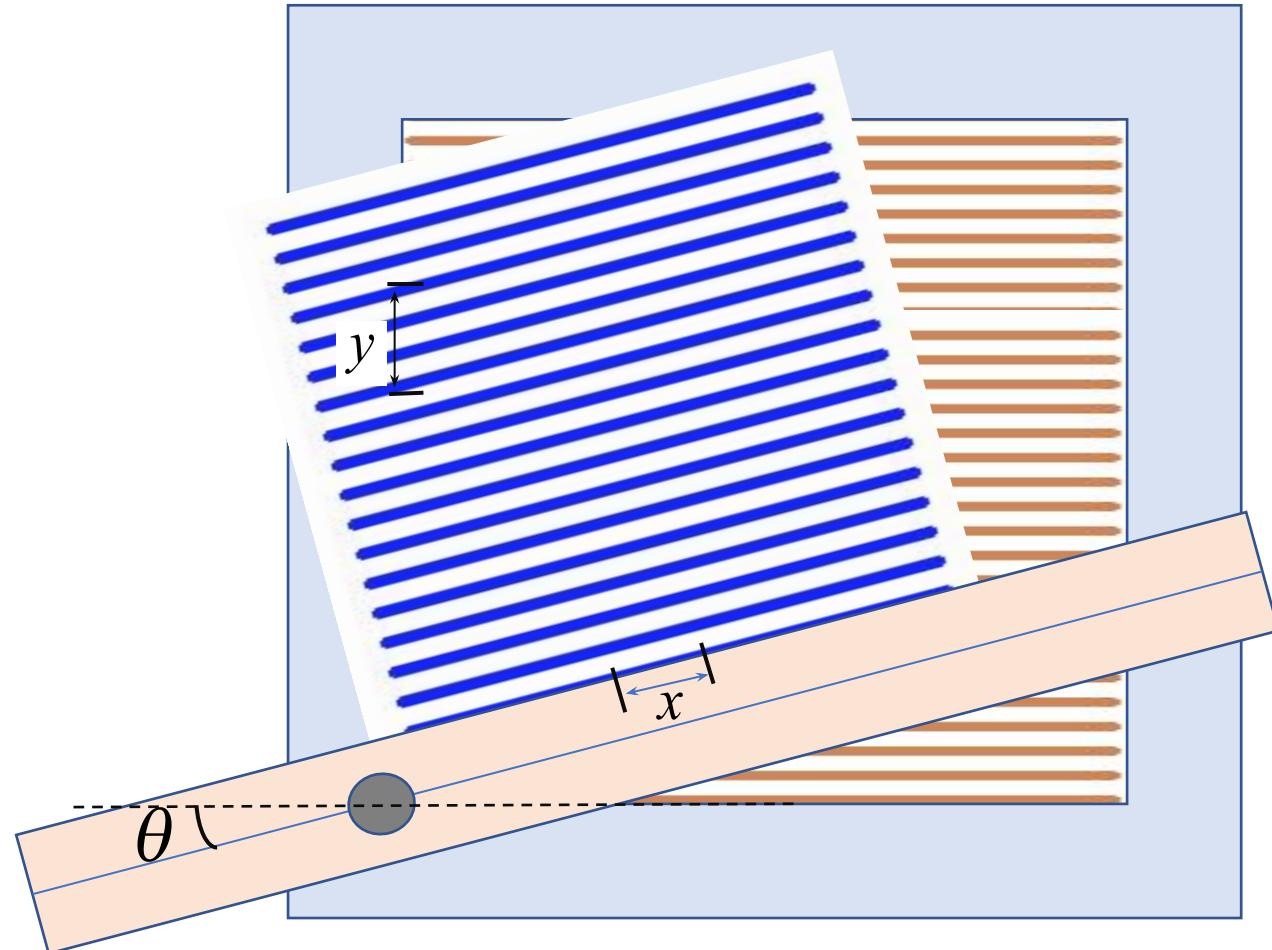
Screw with nut



overlay
0,5MM
0,2MM
0,1MM

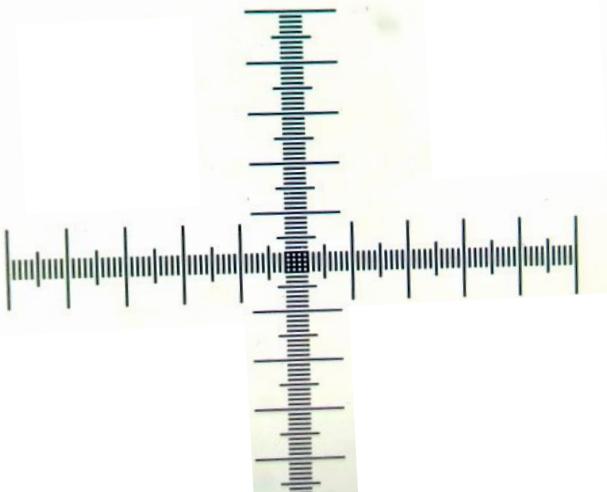
protractor

The calculation of the period of moiré



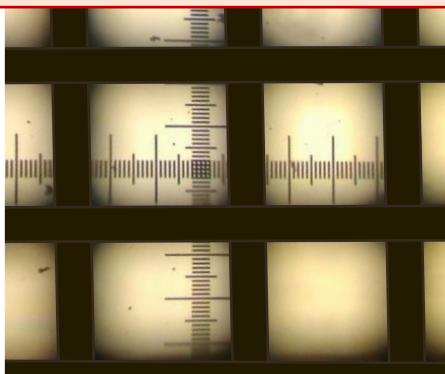
$$D = \frac{x \cdot y \cdot \cos \theta}{\sqrt{x^2 + y^2 - 2xy \cdot \sin \theta}}$$

Direct measurement of the number of threads



Errors of the number
of threads of direct
method:

We take around 20 measurements and average them.



Error of set up

$$n_1(\theta, D, d_2) = \frac{D \cos \theta - \sqrt{d_2^2 - D^2 \sin^2 \theta}}{d_2 D}$$

$$\Delta D = \sqrt{\left(\frac{\partial D}{\partial x} \Delta x \right)^2 + \left(\frac{\partial D}{\partial y} \Delta y \right)^2 + \left(\frac{\partial D}{\partial \theta} \Delta \theta \right)^2}$$

$$\Delta n_1 = \sqrt{\left(\frac{\partial n_1}{\partial d_2} \Delta d_2 \right)^2 + \left(\frac{\partial n_1}{\partial \theta} \Delta \theta \right)^2 + \left(\frac{\partial n_1}{\partial D} \Delta D \right)^2}$$

$$T = \frac{1}{\Delta n_{omh}} = \frac{n}{\Delta n_{abc}}$$

$$\begin{aligned}\Delta d_2 &= \pm 0,01 \text{ mm} \\ \Delta \theta &= \pm 1^\circ\end{aligned}$$

$$D = \frac{x \cdot y \cdot \cos \theta}{\sqrt{x^2 + y^2 - 2xy \cdot \sin \theta}}$$

Table values at 15[☒]

\backslash y, MM	0,1	0,15	0,2	...	6
x, MM	0,1	0,15	0,2	...	6
0,1	0,079	0,87	0,105		0,174
	0,03	0,031	0,031		0,045
0,15	0,87	0,119	0,13		0,186
	0,031	0,032	0,034		0,063
0,2	0,105	0,13	0,1586		0,195
	0,031	0,034	0,0356		0,65
...					
8	0,096	0,01	0,012		5,347
	0,1	0,11	0,11		1,54

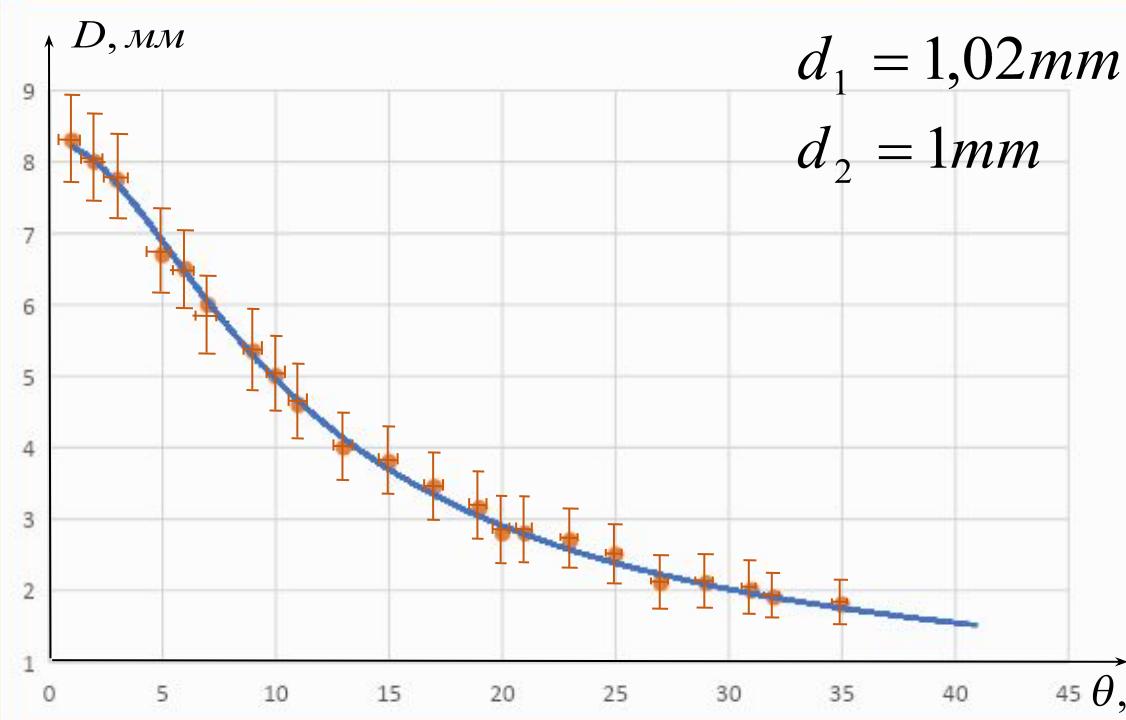
The period of moiré, MM overlay, MM	0,079	0,87	...
0,42	14,9 2,14	12,3 1,5	...
0,82	14,6 2,1	12,26 1,7	...
1,15	14,2 1,96	12,1 1,94	...

The period of
moiré
error of moire
period

Number of
threads per cm
Error of set up

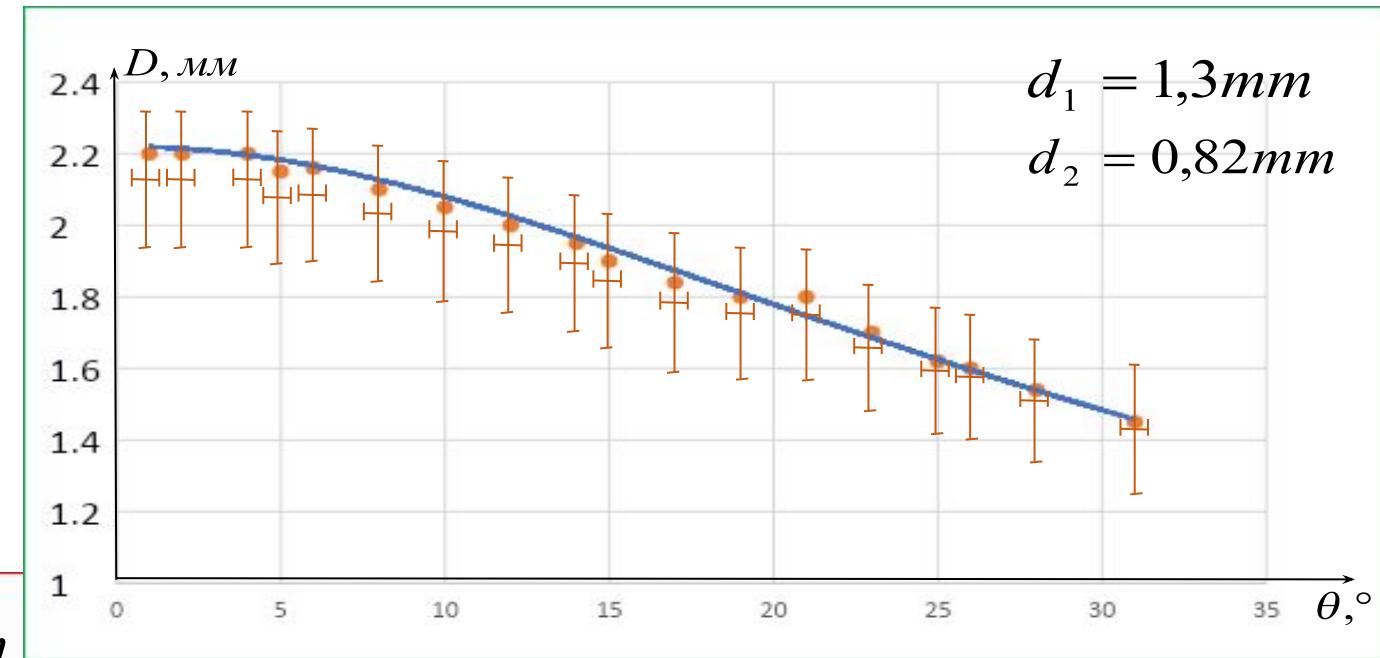
Dependence of the moiré pattern period on the rotation angle

$$D = \frac{d_1 \cdot d_2}{\sqrt{d_1^2 + d_2^2 - 2 \cdot d_1 \cdot d_2 \cdot \cos \theta}}$$



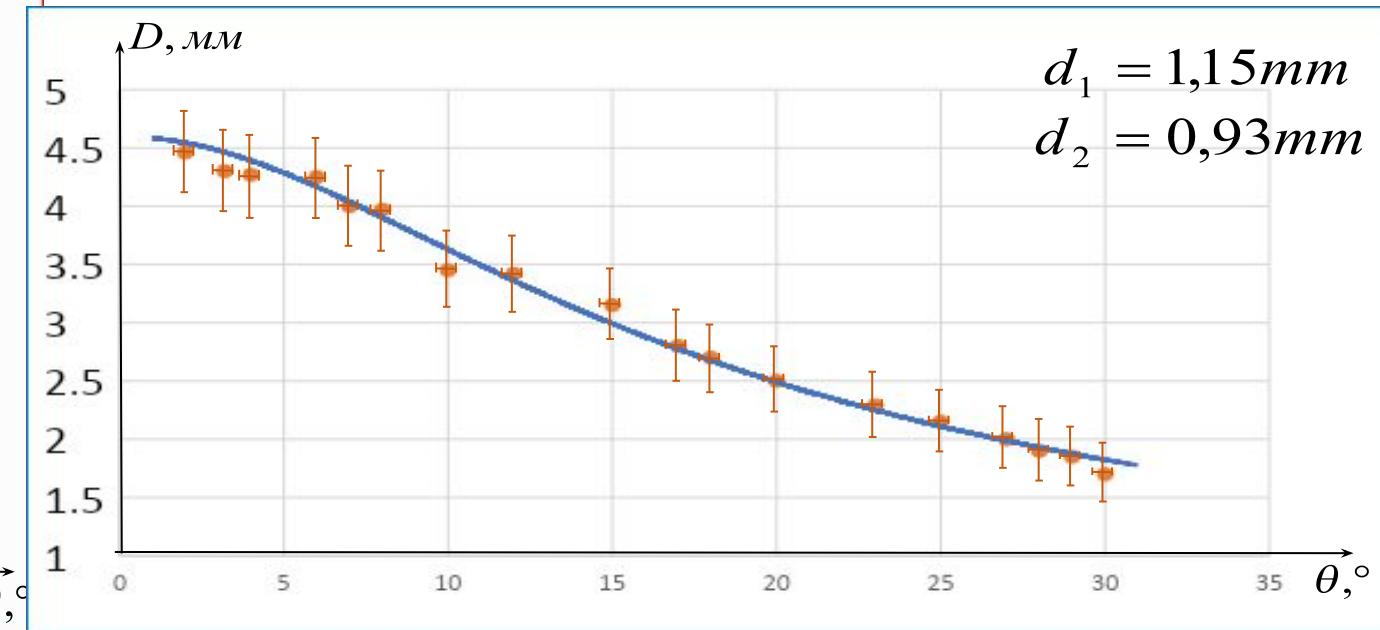
$$d_1 = 1,02 \text{ mm}$$

$$d_2 = 1 \text{ mm}$$



$$d_1 = 1,3 \text{ mm}$$

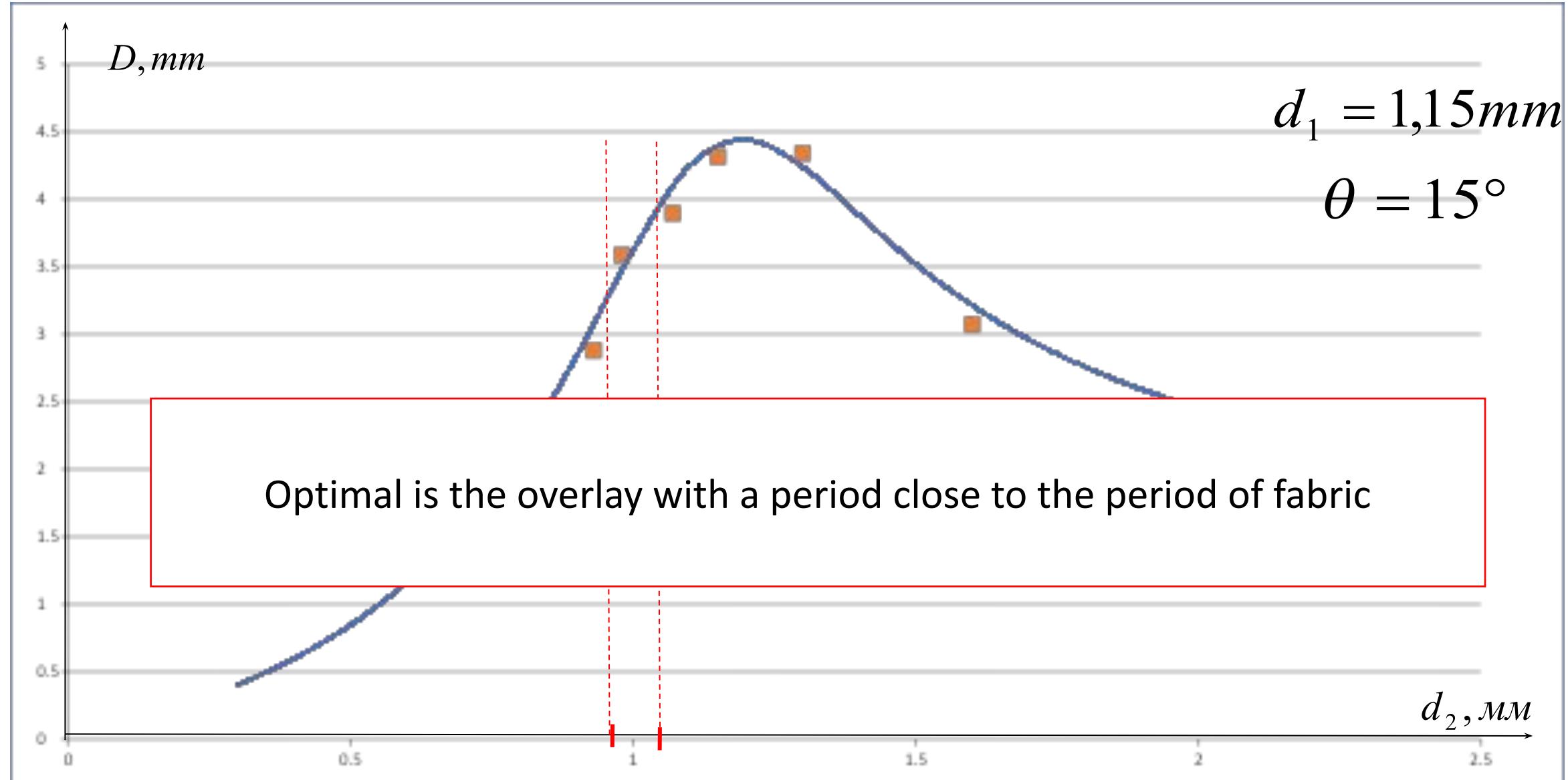
$$d_2 = 0,82 \text{ mm}$$



$$d_1 = 1,15 \text{ mm}$$

$$d_2 = 0,93 \text{ mm}$$

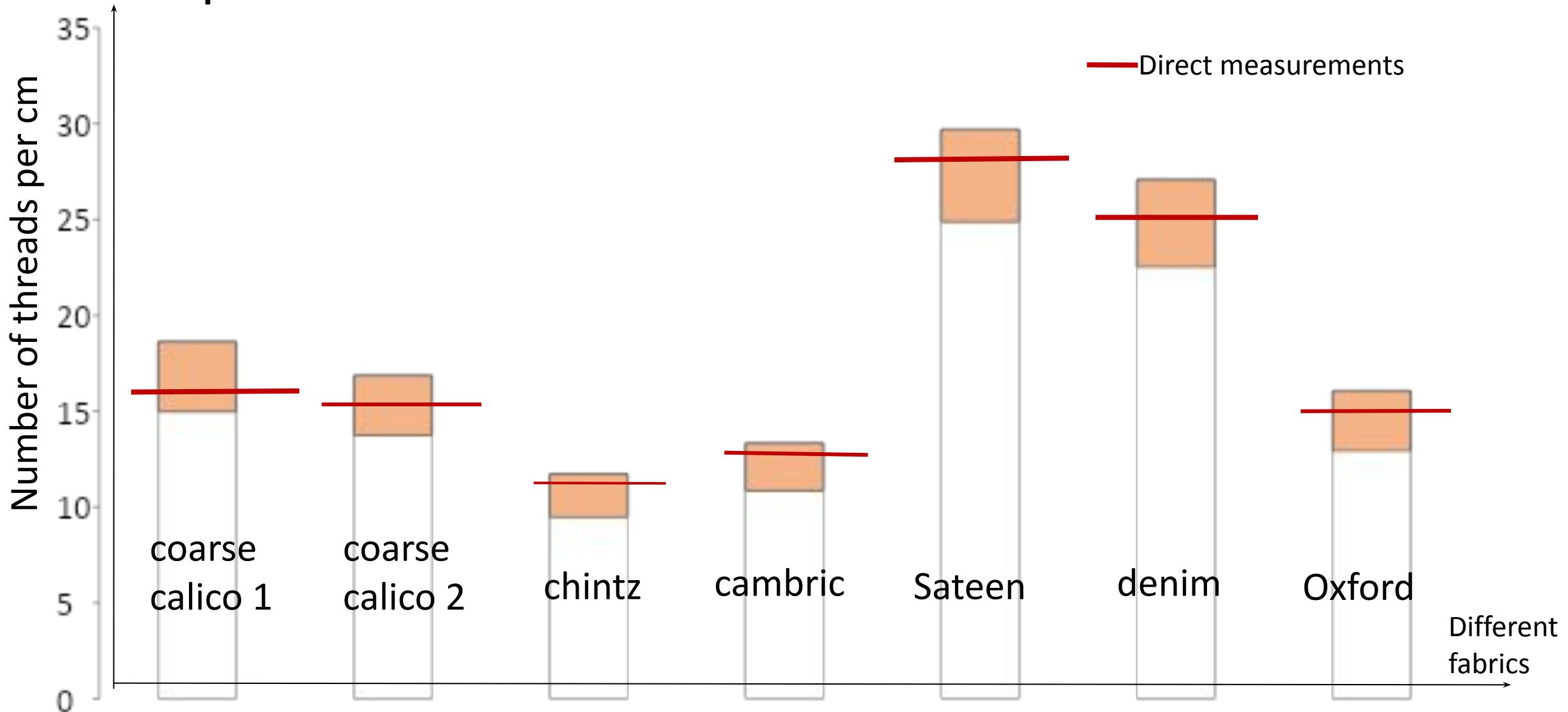
Dependence of the moire period on the overlay



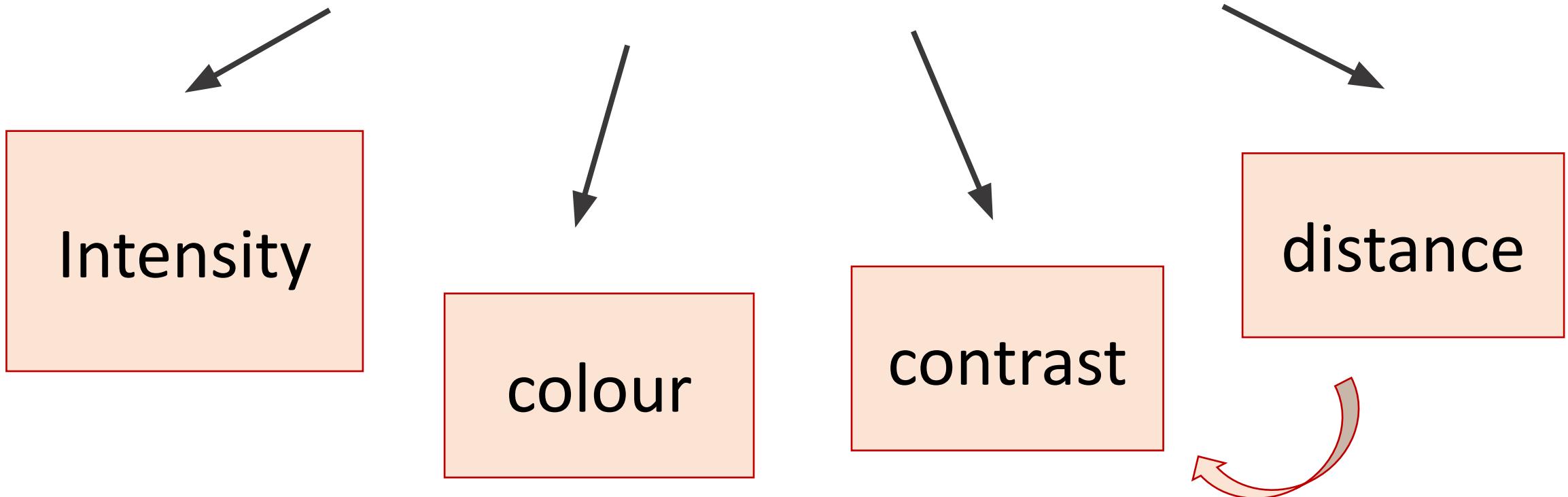
Comparison between direct and undirect measurement

Fabric	Moiré pattern(undirect)	Microscope(direct)
coarse calico 1	14,97<16,80<18,63	15,87<15,90<15,93
coarse calico 2	13,73<15,30<16,87	15,58<15,60<15,62
chintz	9,48<10,60<11,72	10,79<10,80<10,81
cambric	10,86<12,10<13,34	12,78<12,80<12,82
Sateen	24,89<27,30<29,71	28,62<28,70<28,78
Denim	22,52<24,80<27,08	24,98<25,05<25,11
Oxford	12,93<14,50<16,07	14,68<14,70<14,72

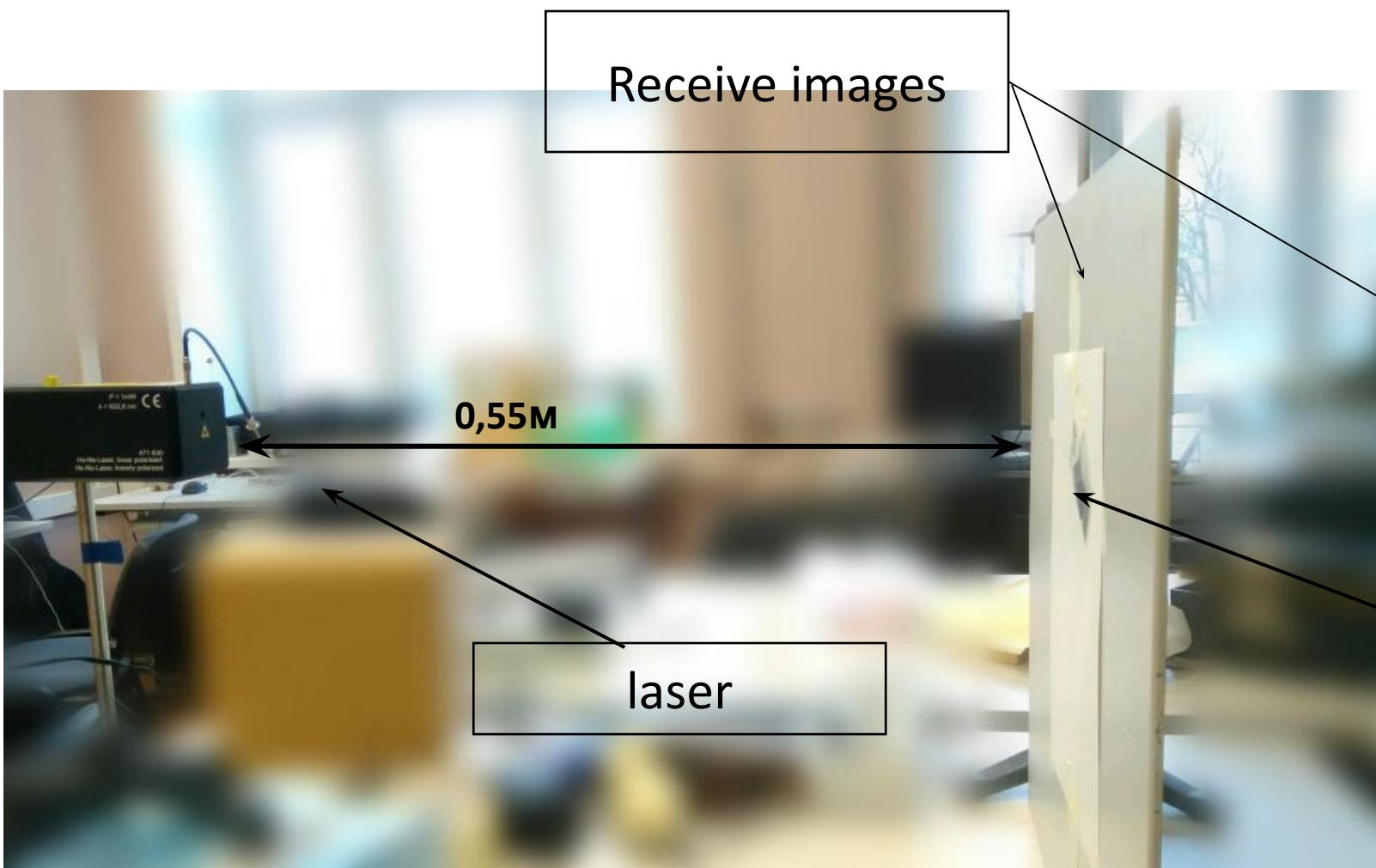
Comparison between direct and indirect measurement



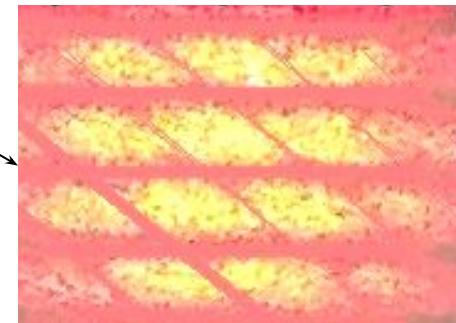
Applicability of designed overlay



Set up with improved resolution



**800 kilo
lux-sensor of
(order of 1000
lux-sensor)**

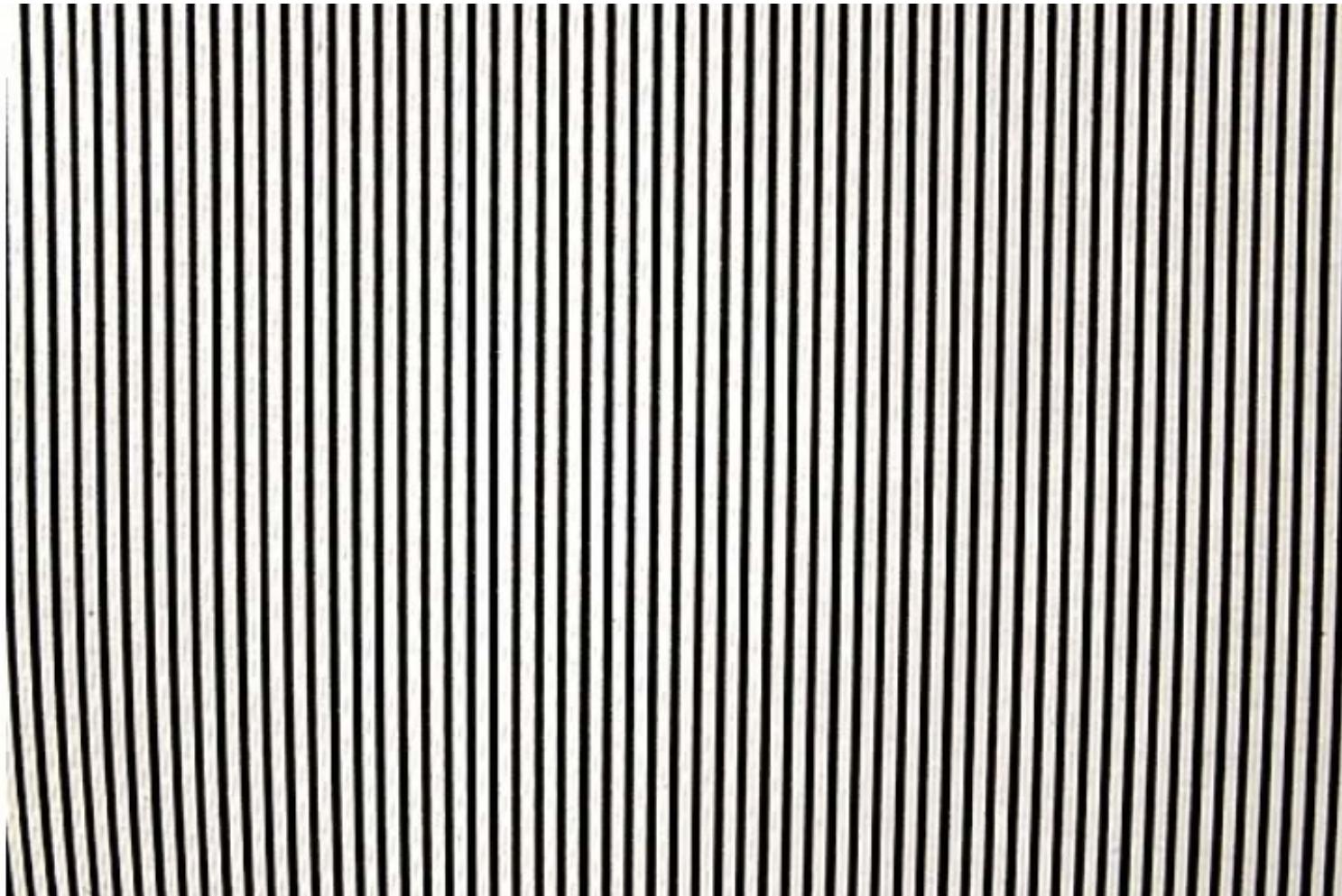


**60 kilo
lux-sensor**

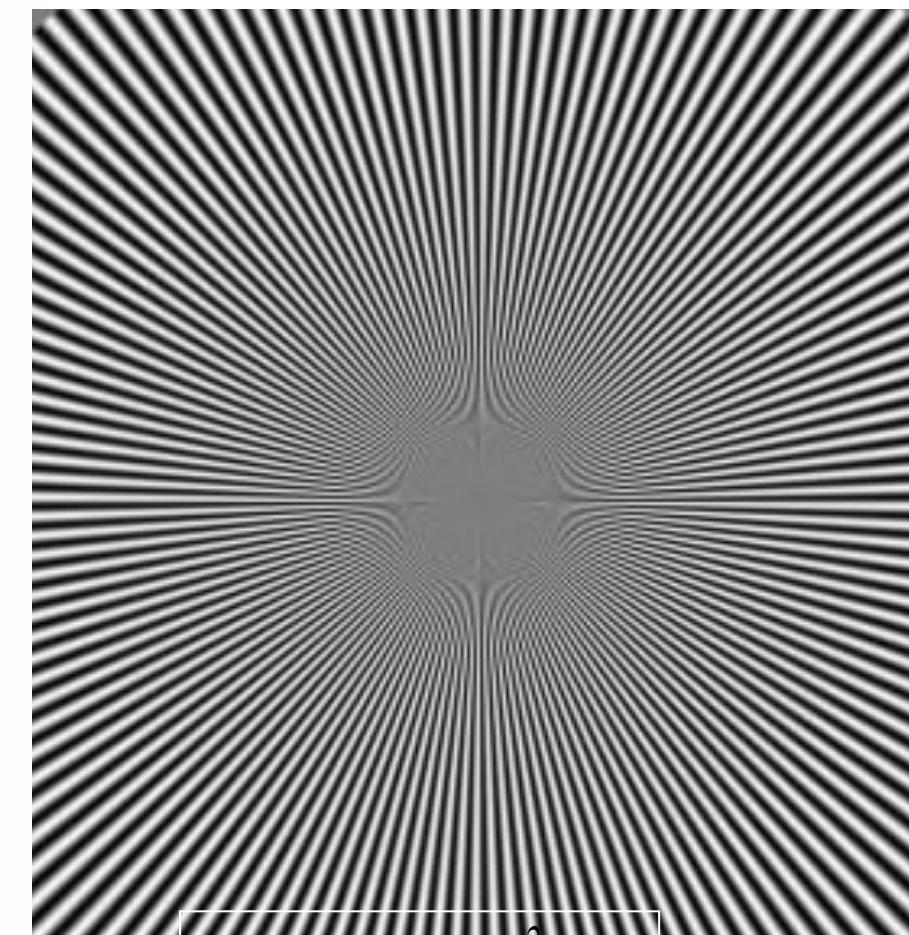
overlay

Limitations of the visibility of a moiré pattern

Critical angle

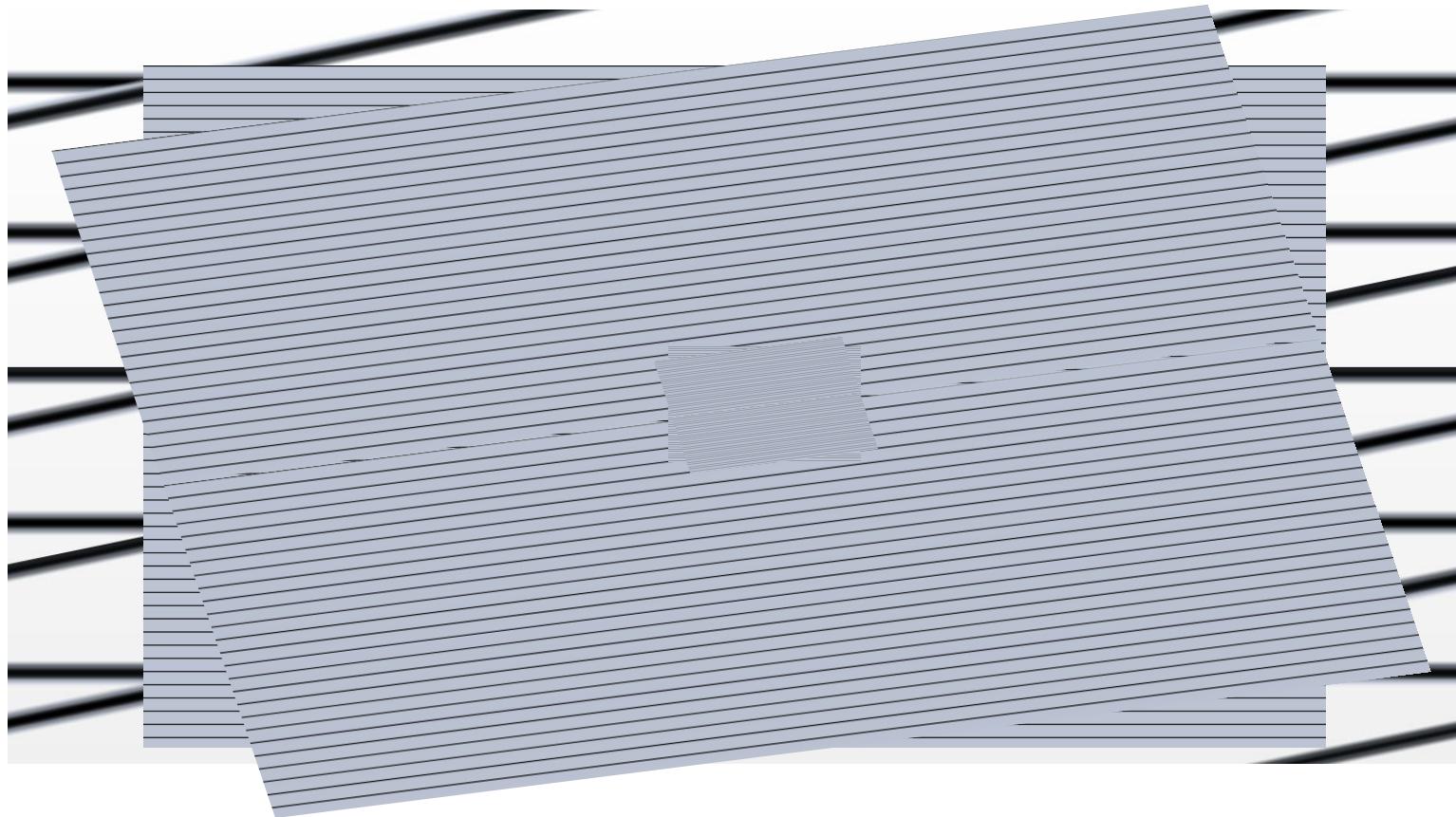


Angular resolution



$$Q = 1.220 \frac{\lambda}{D_{\text{аппертуры}}}$$

Applicability of designed overlay

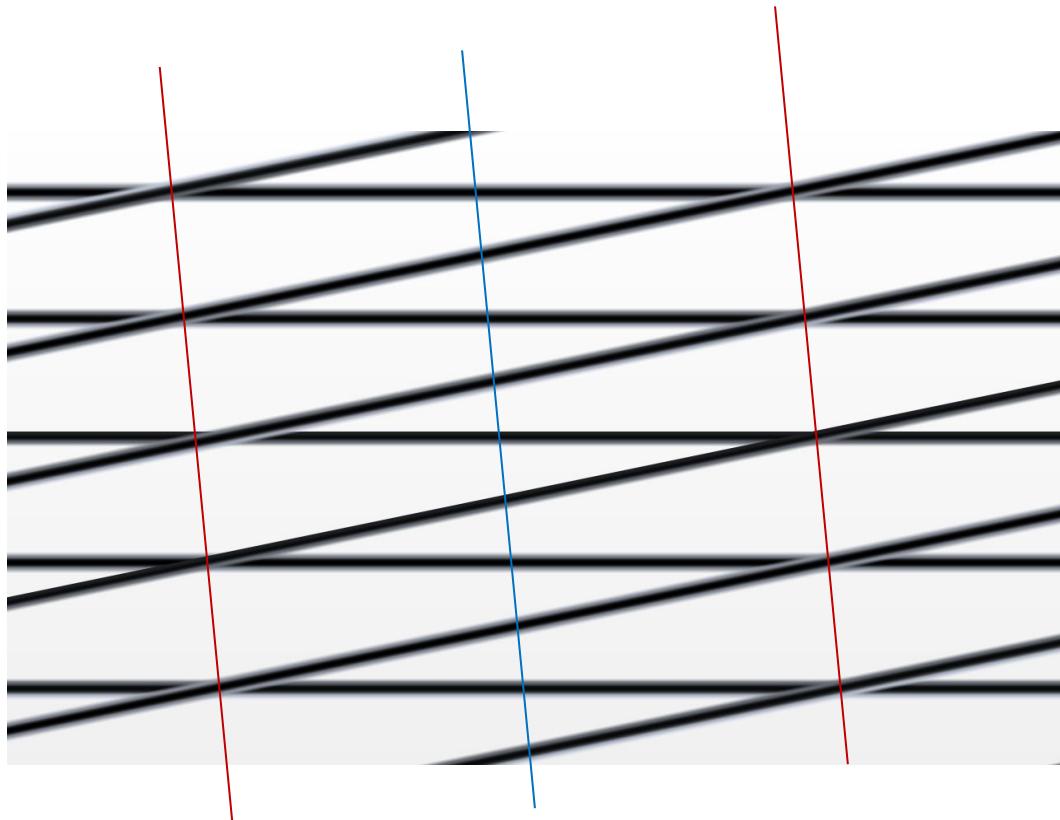


We don't see the moiré pattern(the distance between our eyes or camera and overlay with the fabric is too small)

We see the moiré pattern

We don't see the moiré pattern(the distance between our eyes or camera and overlay with the fabric is too big)

Applicability of designed overlay



Thickness of the overlay's line

Thickness of the thread

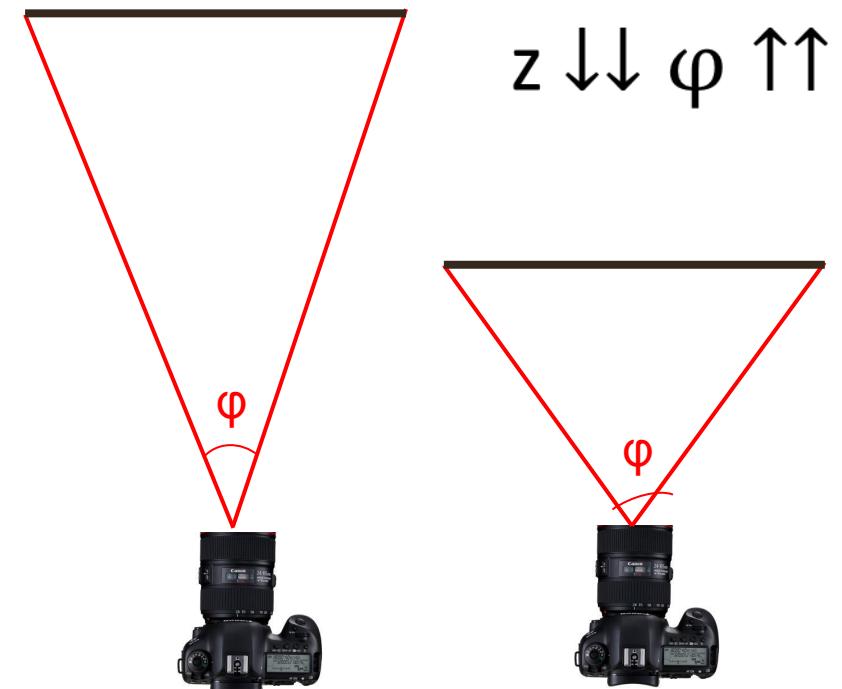
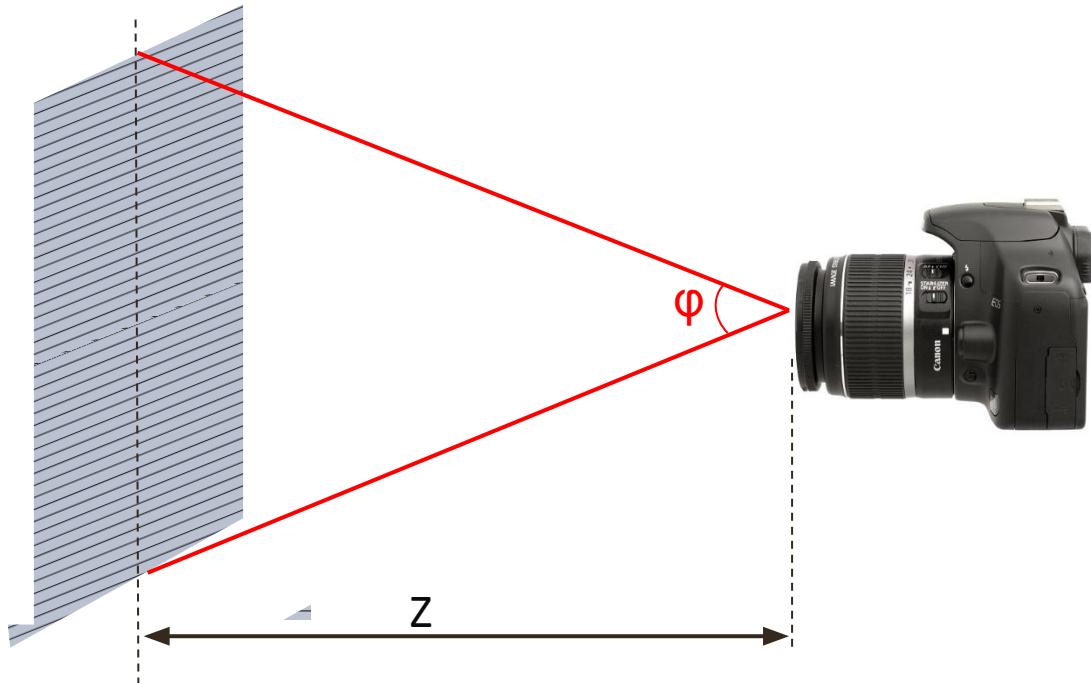
$$C = \frac{1 - \frac{t_{overlay}}{d_{overlay}}}{1 - \frac{t_{overlay}}{d_{overlay}} - \frac{t_{thread}}{d_{thread}}}$$

Period of the overlay

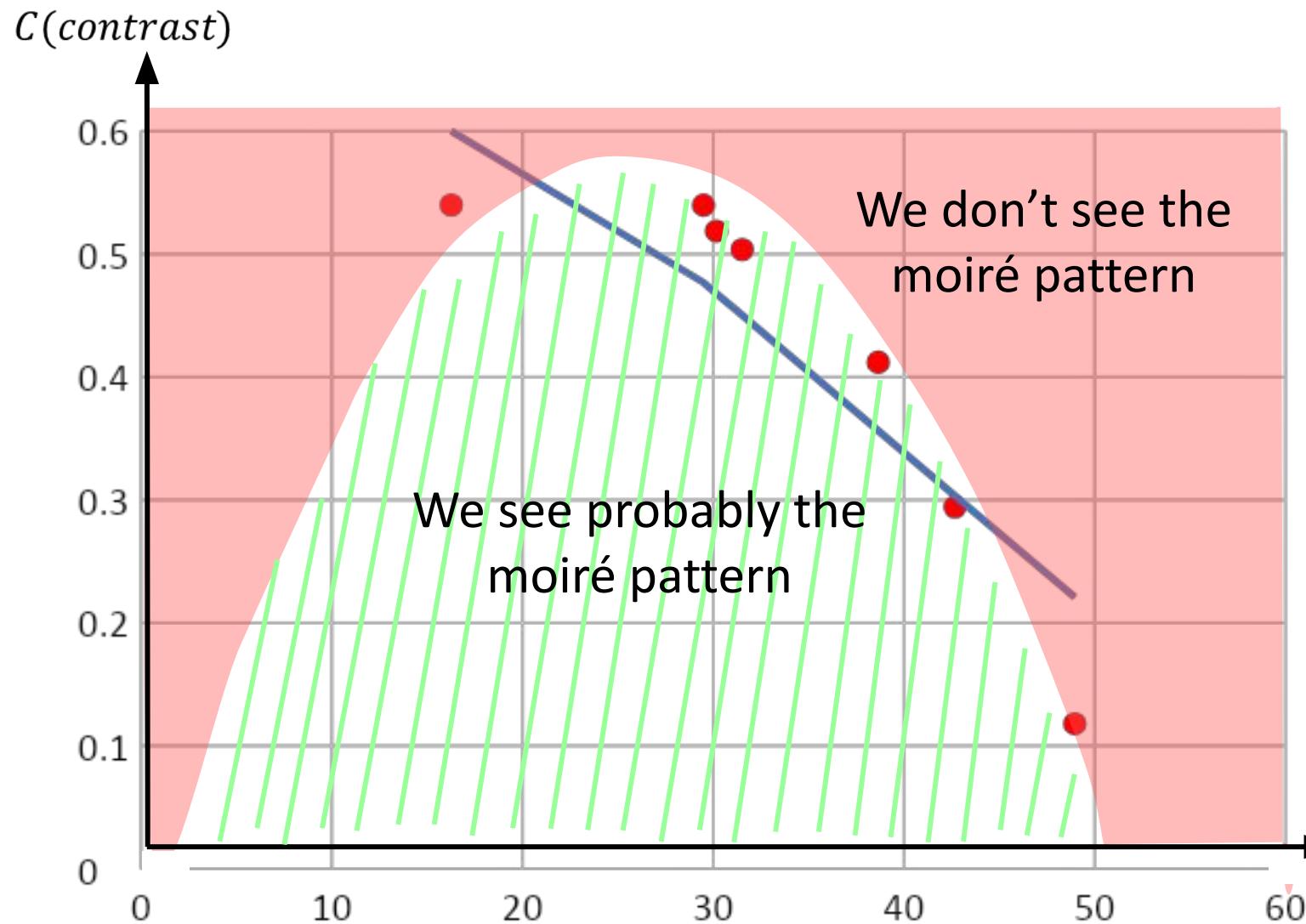
Period of the fabric

The influence of the distance

The angle, which our eyes(or camera) see the overlay at, decreases if the distance increases



The applicability of our method



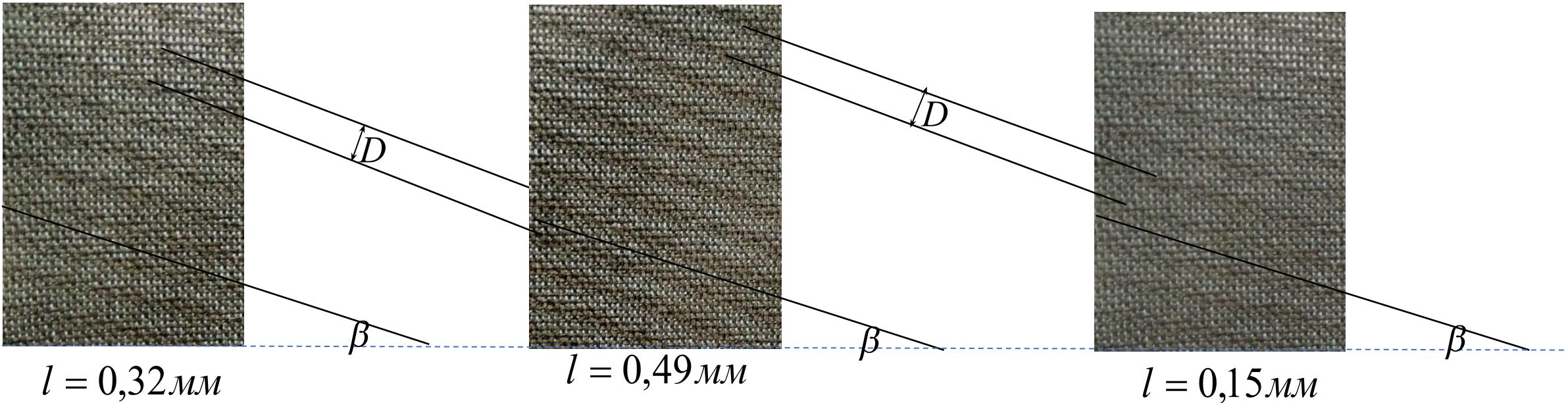
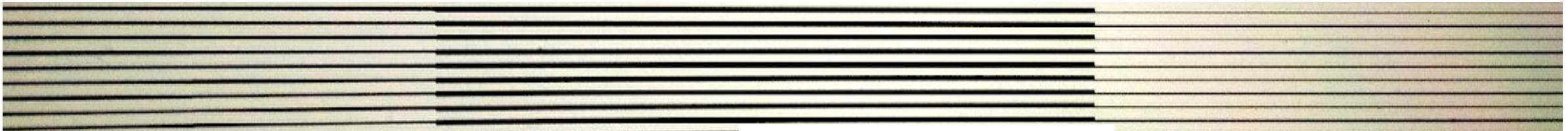
Value $\frac{1}{\alpha}$ is the number of lines per one degree

Value contrast C is the value that provide the transparent and opaque lines in the moiré pattern.

Dependence of the moire period on the thickness of the overlay's line

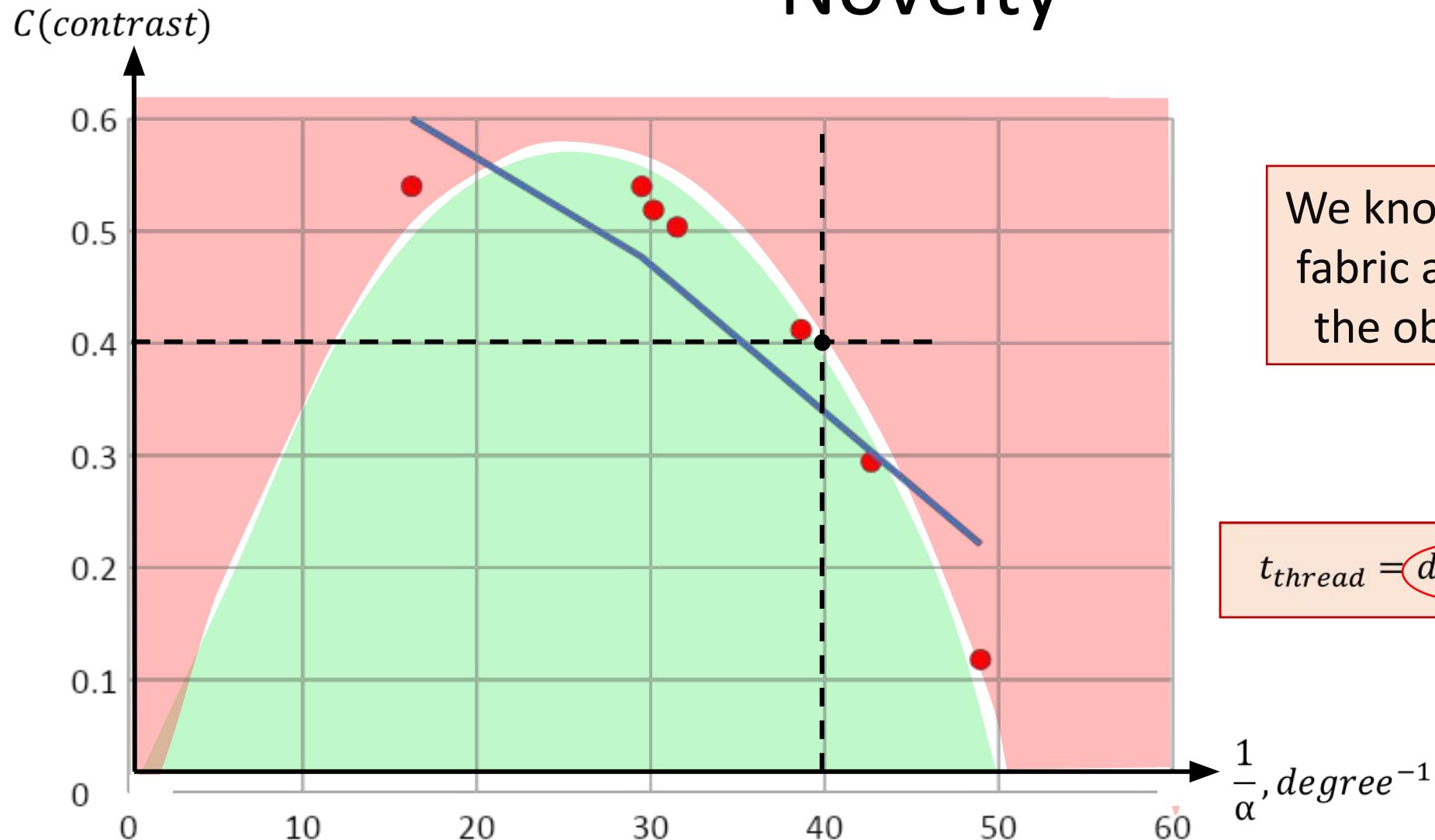
$d = 1,45\text{MM}$ – Period of the overlay

$$d_2 = f + l = \text{const}$$



The thickness affects the contrast of the pattern

Novelty

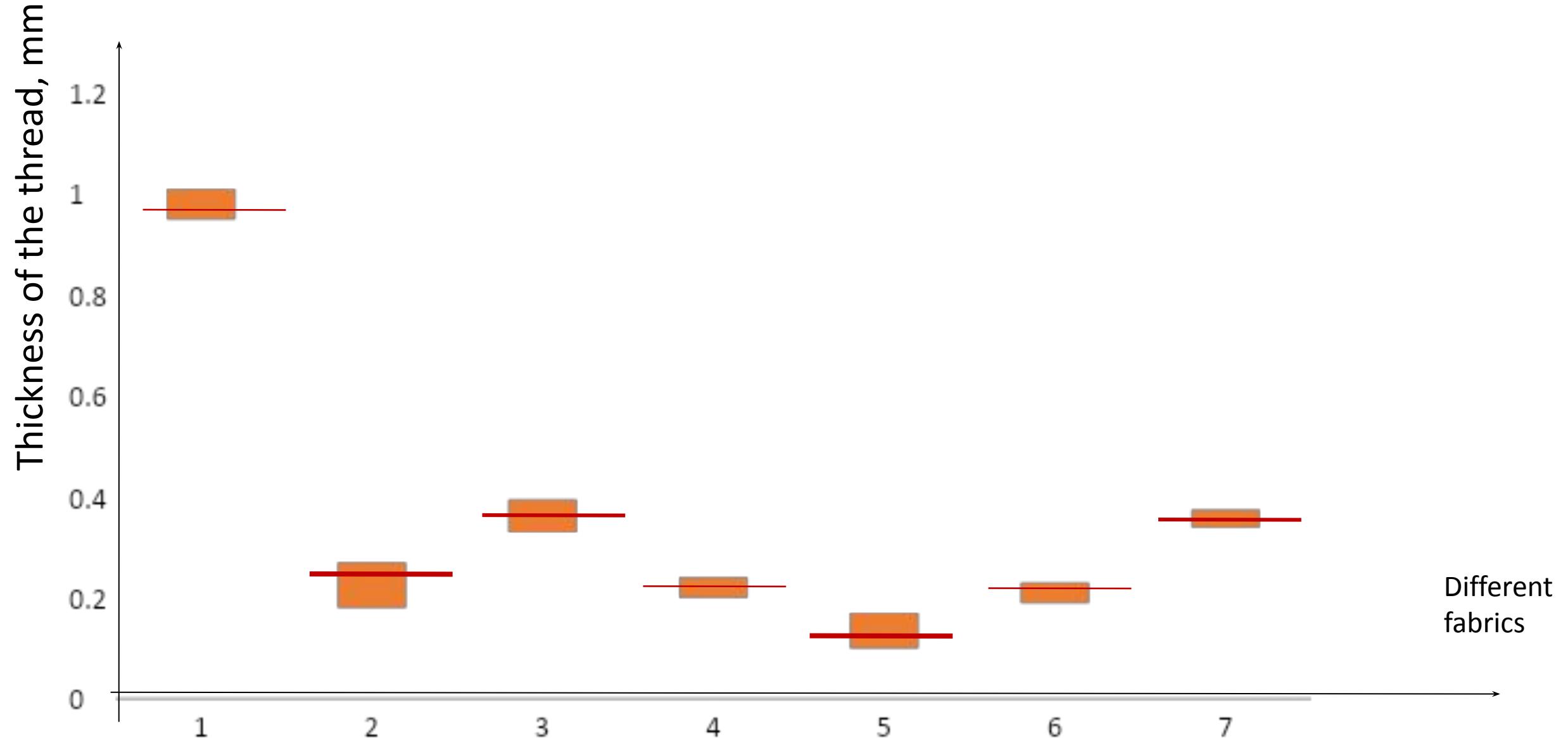


We know the period of the fabric and the moiré from the obtained equations.

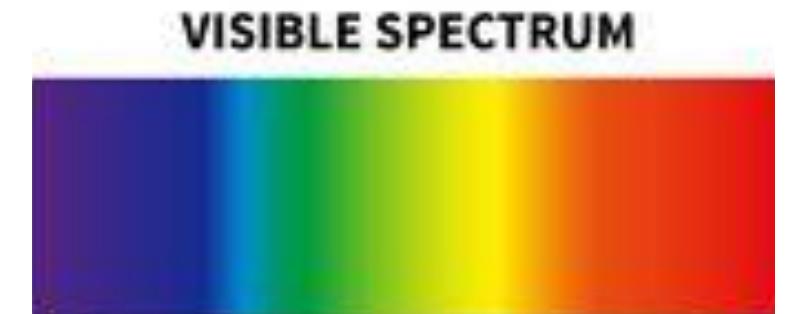
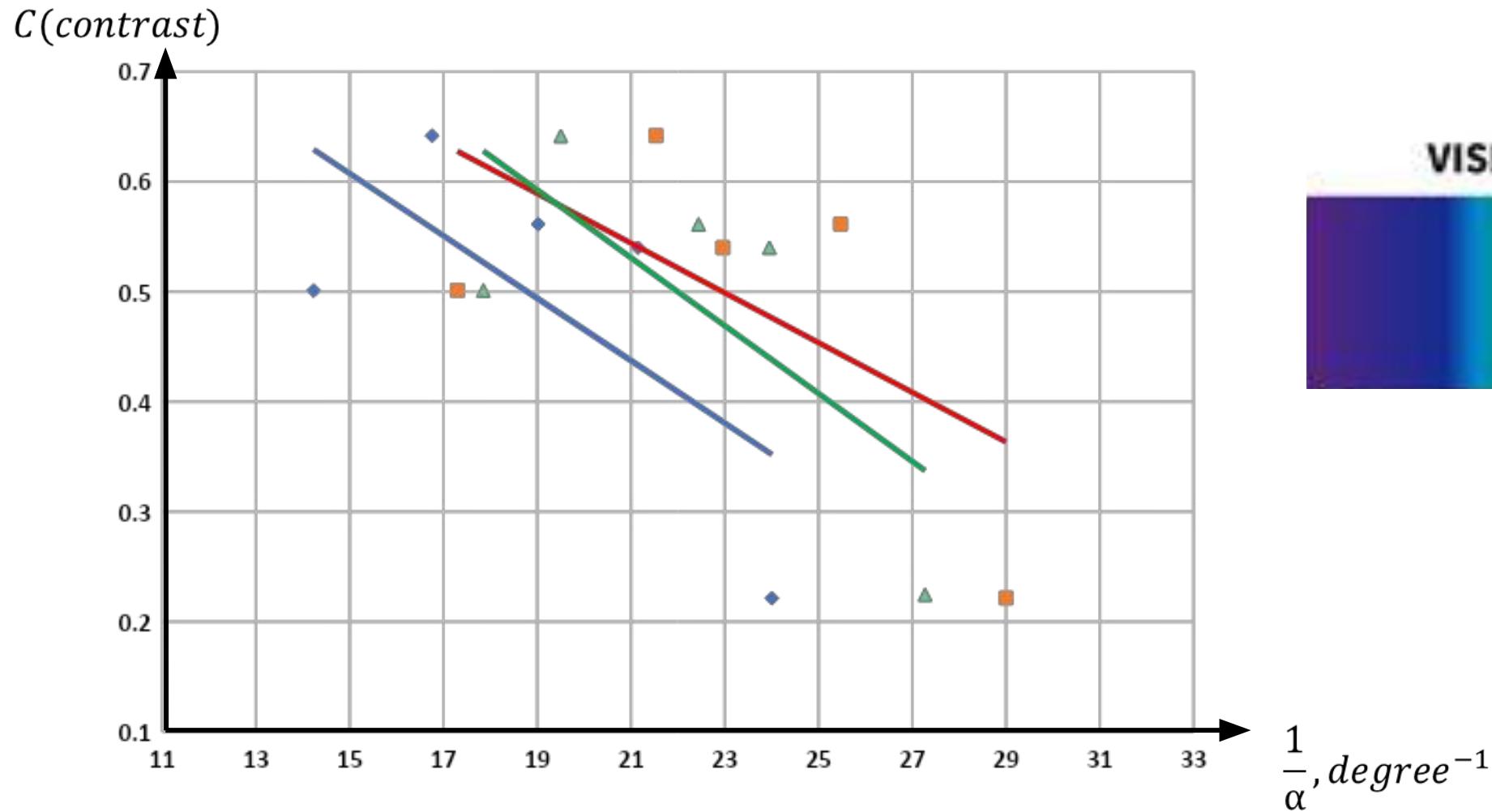
$$t_{\text{thread}} = d_{\text{thread}} \left(1 - c\right) \left(1 - \frac{t_{\text{overlay}}}{d_{\text{overlay}}}\right)$$

KNOWN!!!

Comparison for the thickness of the threads



For different colours

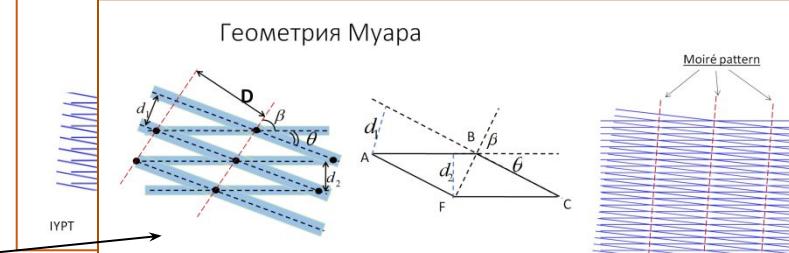


Conclusions

1) Qualitative explanation of the appearance of the moiré pattern (geometry)



2) Mathematical description based on geometrical neglect



3) An experimental setup was created to determine the number of fabric threads with a minimum accuracy of 62 and a maximum of 202

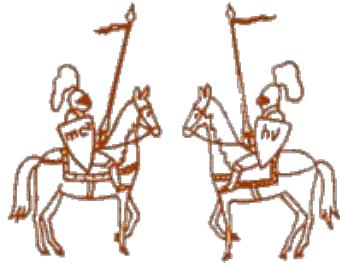


4) Experimentally studied different types of fabric, the set-up allows you to determine the number of threads in all fabrics



Сравнение теории с практикой			
Название ткани	Количество нитей экспериментальное	Количество нитей на микроскопе	Погрешность ε
Бязь 1	16,8	14,9	17%
Бязь 2	15,3	15,6	18,6%
Ситец	10,6	10,8	26,8%
Батист	12,1	12,8	23,5%
Сatin	27,3	28,7	10,4%
Джинса	24,8	25,05	11,45%
Оксфорд	14,5	14,7	19,5%

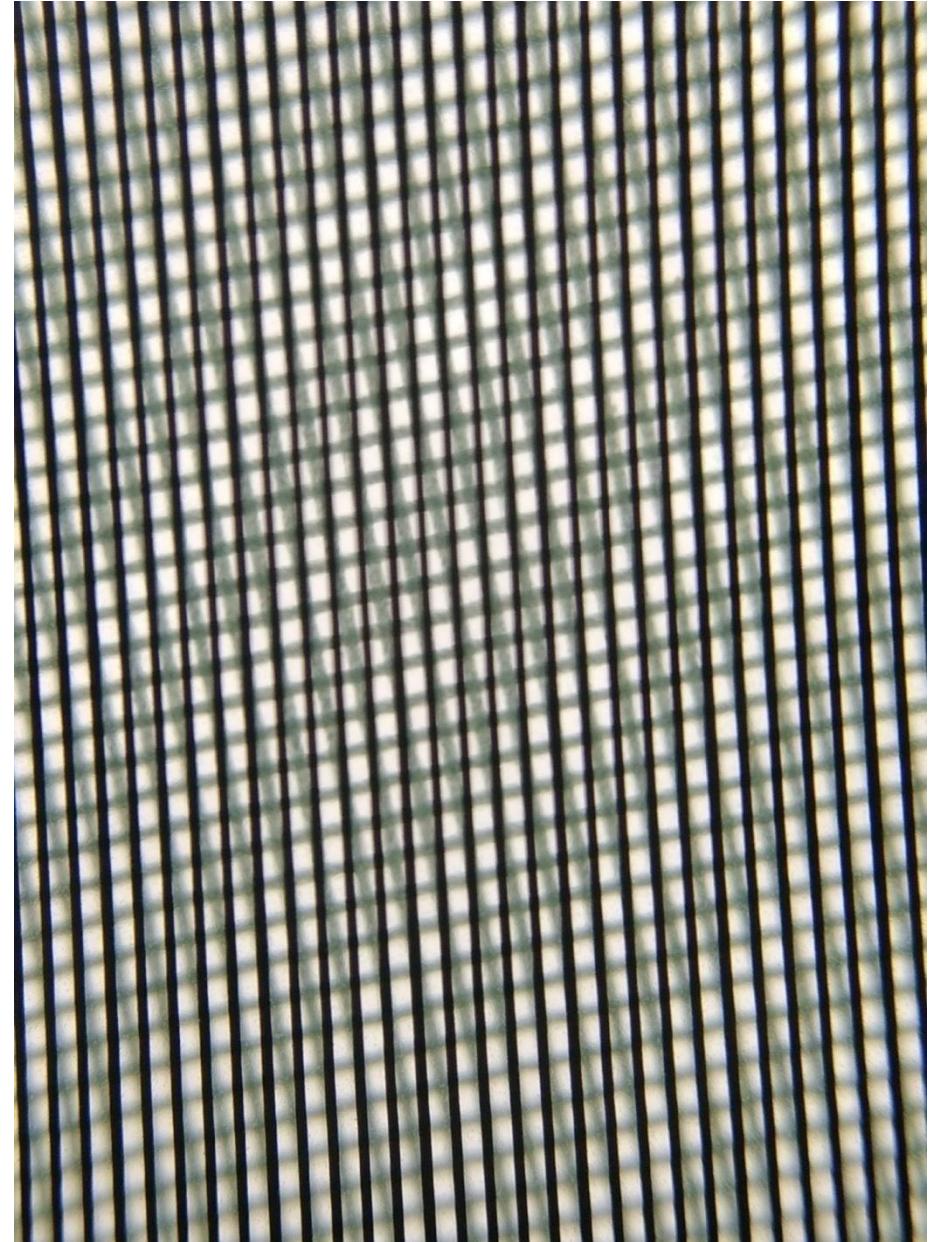
IYPT Experimental Setup Theory Model Optimization



Thank you for your attention!

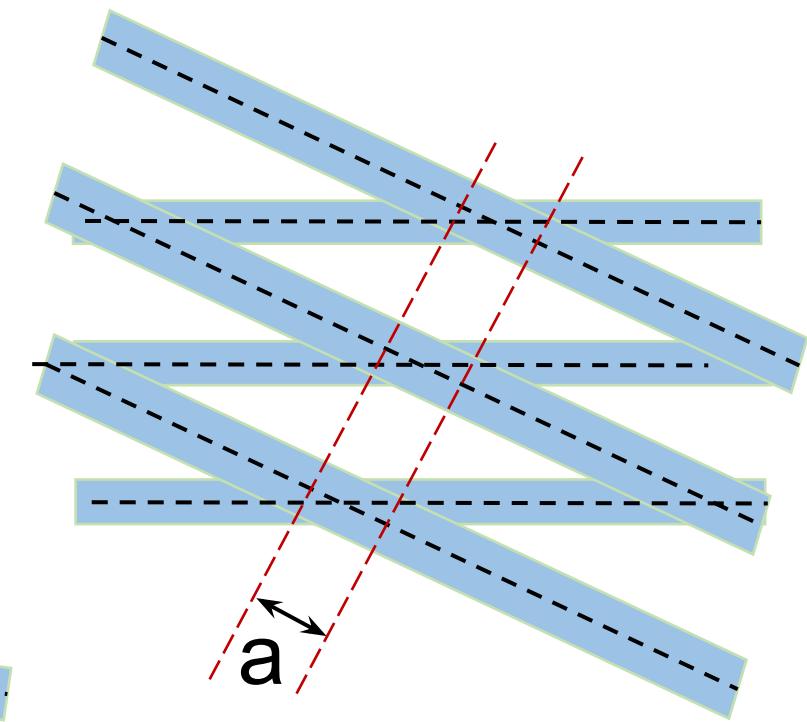
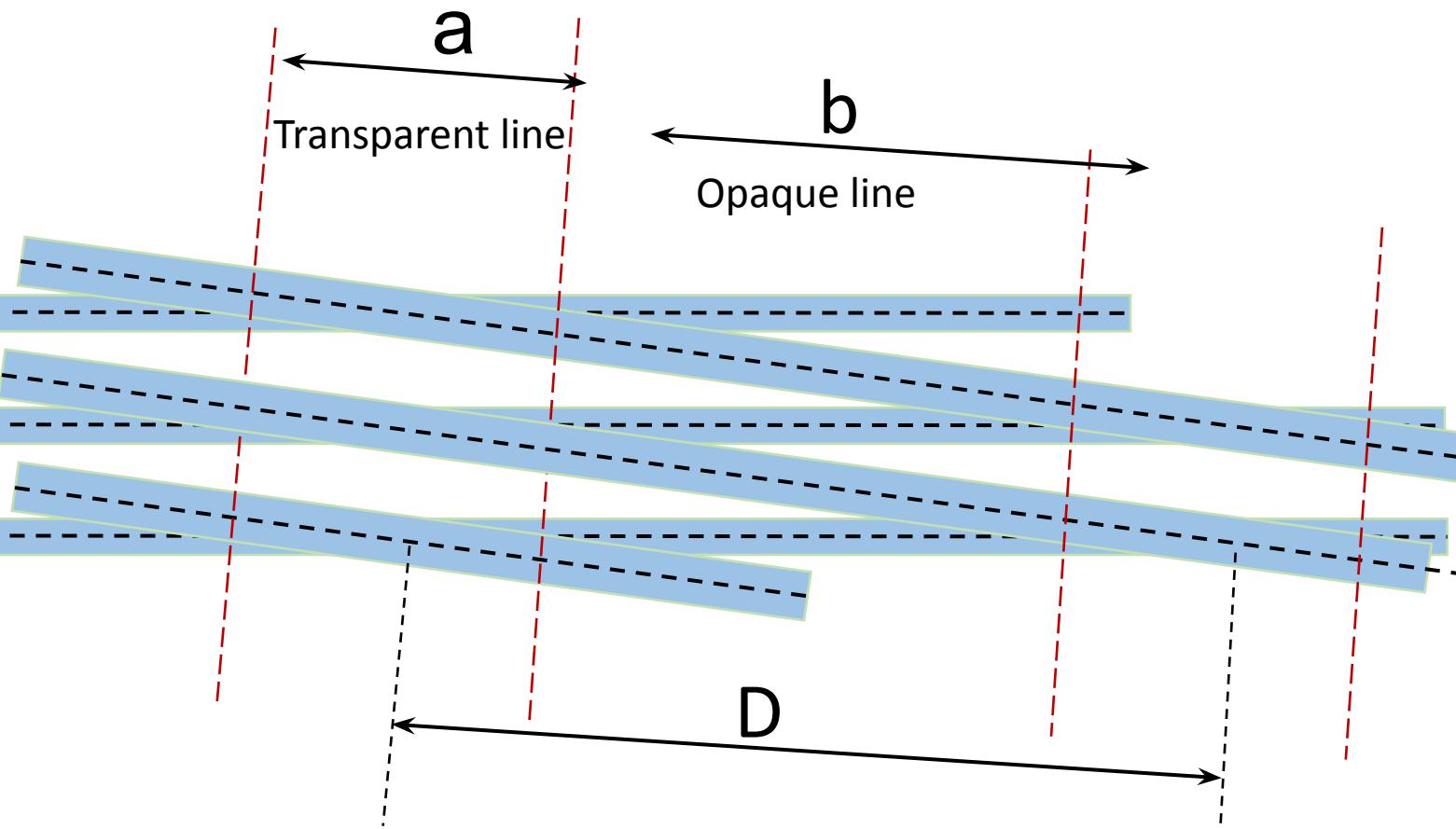
Bibliography:

- A Moiré Pattern-Based Thread Counter (Gary Reich)
 - Isaac Amidror_The_theory_of_the_moire_769_phenomen_Volume_I
 - The Effects of a Visual Fidelity Criterion on the Encoding of Images JAMES L. MANNOS, MEMBER, IEEE, AND DAVID J. SAKRISON (IEEE TRANSACTIONS ON INFORMATION THEORY, VOL. IT-20, NO. 4, JULY 1974)



Limitations of the visibility of a moiré pattern

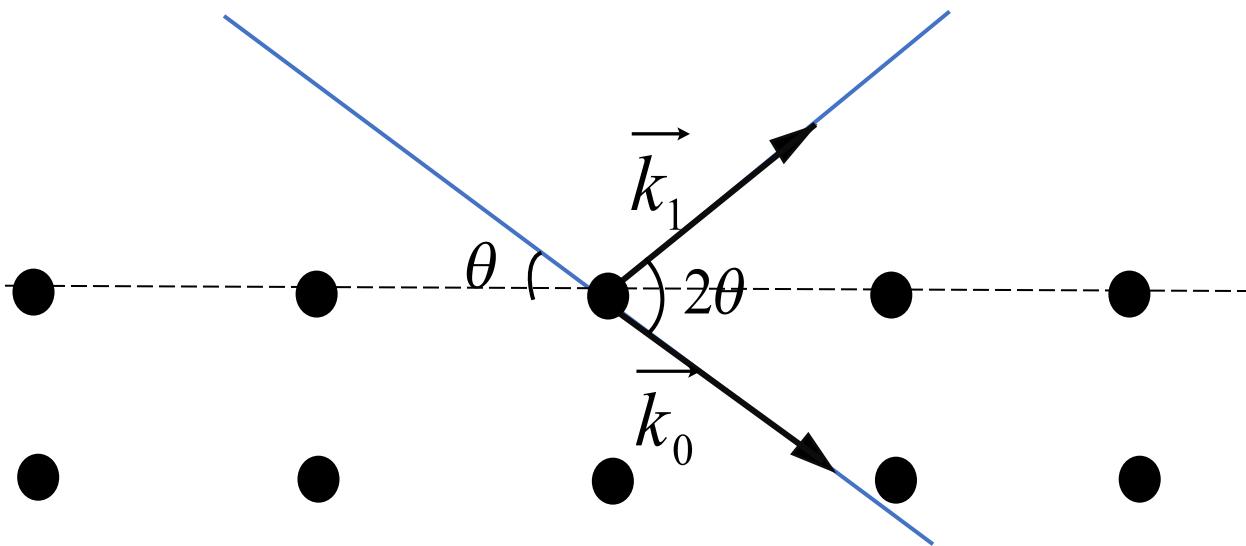
$$D = a + b$$



Дифракция рентгеновского излучения

Формула Вульфа-Брэгга:

$$2d \cdot \sin \theta = n * \lambda, n \in N$$



$$\boxed{V = \frac{\lambda}{2\pi} \omega = \frac{\omega}{k}}$$
$$\boxed{k = \frac{2\pi}{\lambda}}$$

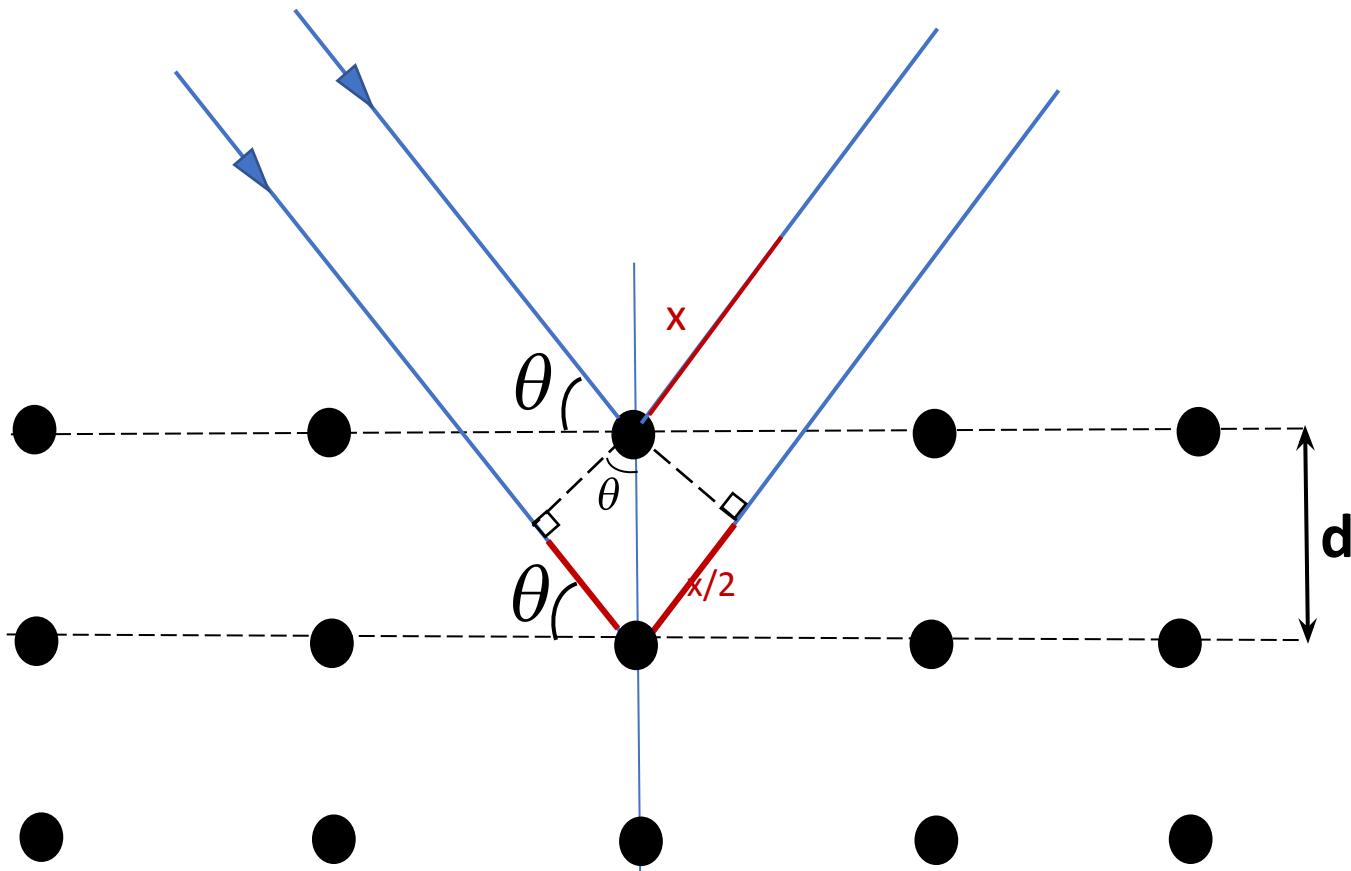
$$k = \frac{2\pi}{\lambda}$$

-Волновое
число

$$\boxed{n}$$

- Волновой
вектор

Условия возникновения максимумов и минимумов



Разность хода: $x = 2d \cdot \sin \theta$

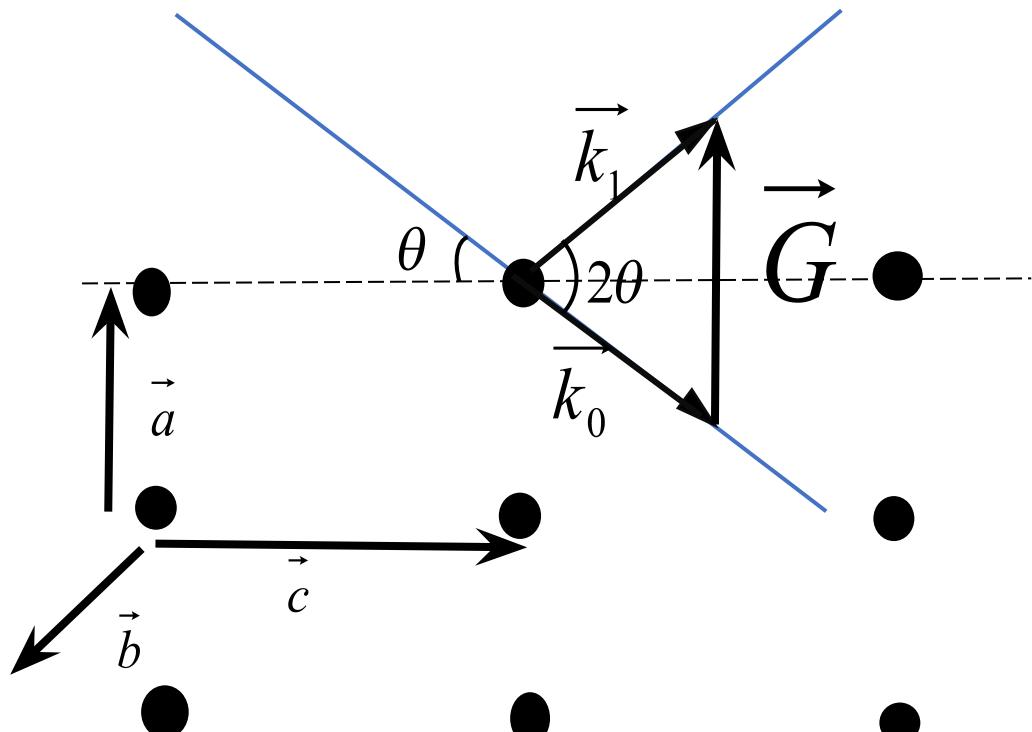
Условия
появления
максимума:

$$x = n * \lambda$$

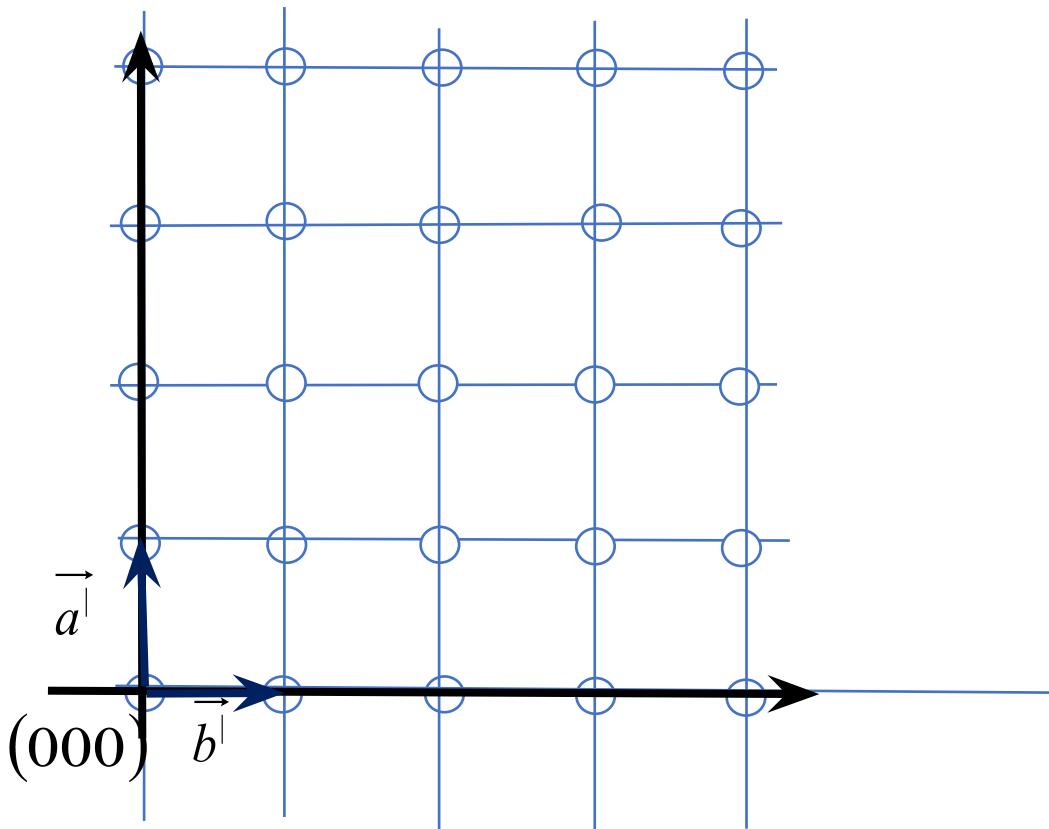
Условия появления
минимума:

$$x = (2n - 1) \frac{\lambda}{2}$$

Задаём обратную решётку



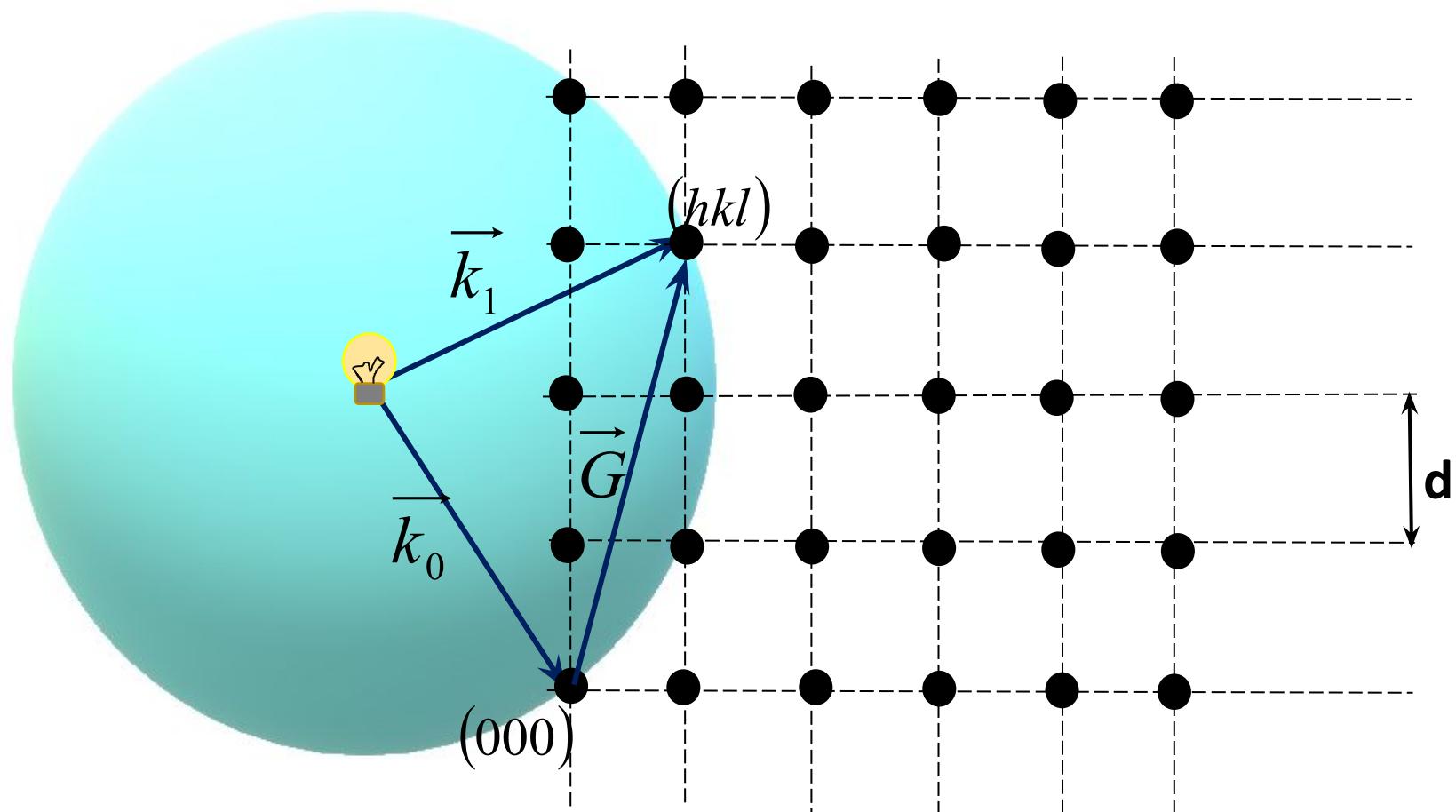
$$\vec{a} \cdot \vec{a}^* = 2\pi$$
$$\vec{a} \cdot \vec{b}^* = 0$$
$$|\vec{a}^*| = \frac{2\pi}{a}$$
$$\vec{a}^* \uparrow \uparrow \vec{b} \times \vec{c}$$



Слайд про точность,

Здесь надо рассказать про накладку и ткань, перескок с периода на период 45 градусов. Всегда две решётки()часть ткани и накладка

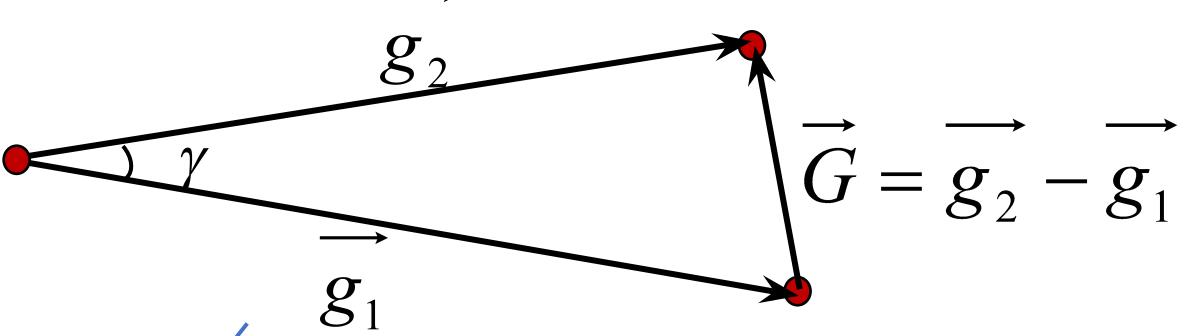
Задаём обратную решётку



$$|\vec{k}_0| = |\vec{k}_1|$$
$$\vec{G} = \vec{k}_1 - \vec{k}_0$$

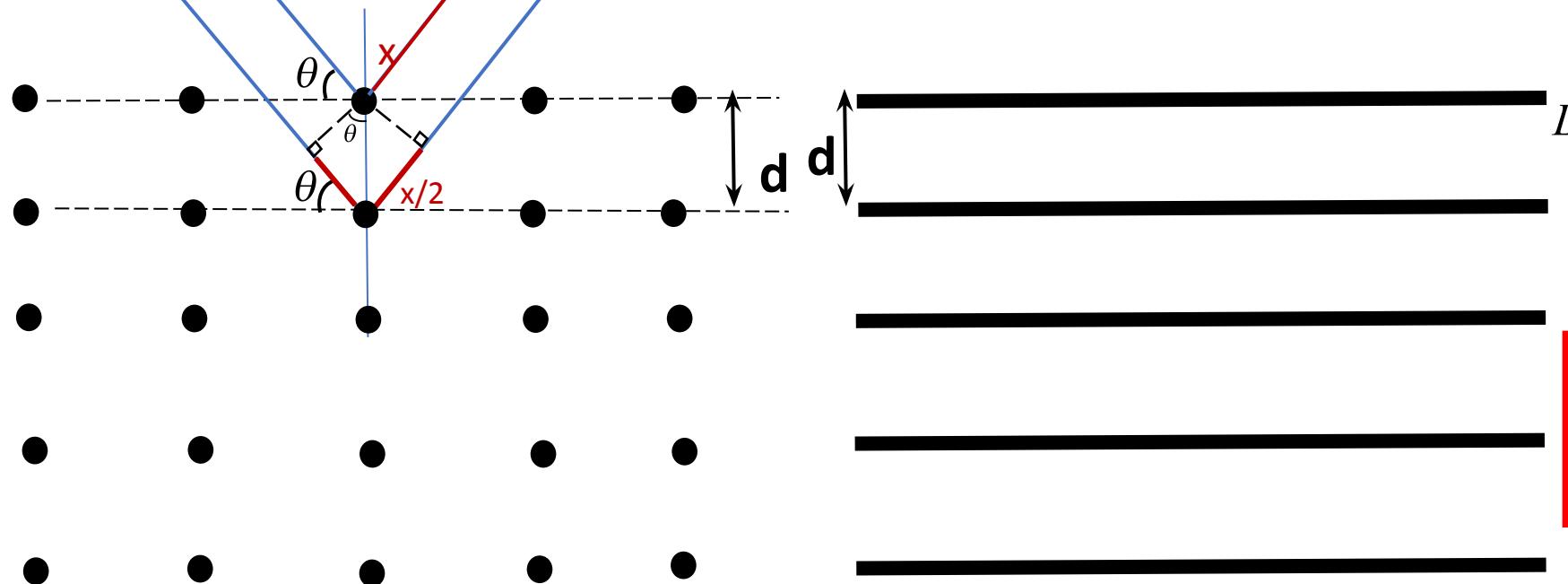
\vec{G} -рассеивающий вектор

Обратная решётка



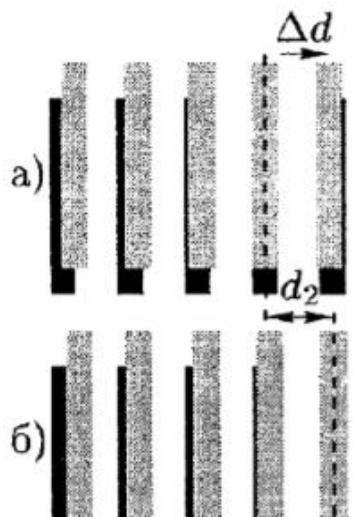
$$|\vec{g}_1| = \frac{2 \cdot \pi}{d_1} \quad |\vec{g}_2| = \frac{2 \cdot \pi}{d_2}$$

$$|\vec{G}| = |\vec{g}_2 - \vec{g}_1| = \frac{2 \cdot \pi}{D}$$



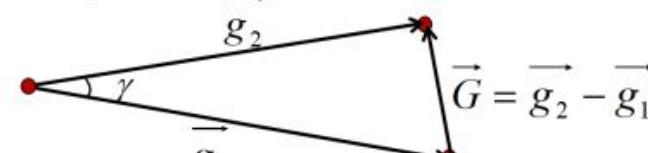
$$D = \frac{2\pi}{\sqrt{\frac{4\pi^2}{d_1^2} + \frac{4\pi^2}{d_2^2} + \frac{2\pi}{d_1} \cdot \frac{2\pi}{d_2} \cdot \cos \gamma}}$$

$$D = \frac{d_1 \cdot d_2}{\sqrt{d_1^2 + d_2^2 - 2 \cdot d_1 \cdot d_2 \cdot \cos \gamma}}$$



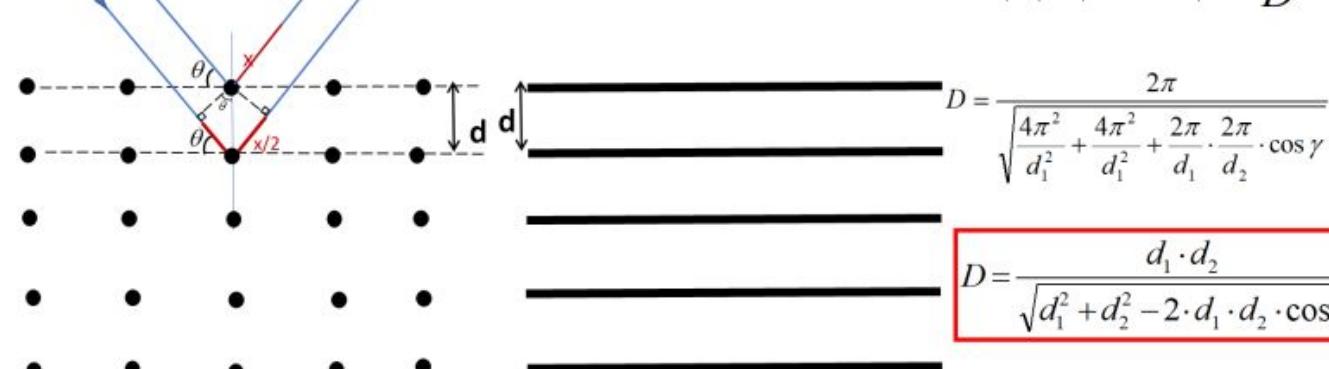
3. Если внимательно рассмотреть рисунок 11, то можно увидеть, что при смещении более частой решётки (на рисунке серой) вправо на расстояние Δd , совпадающие полосы (середи-

Обратная решётка



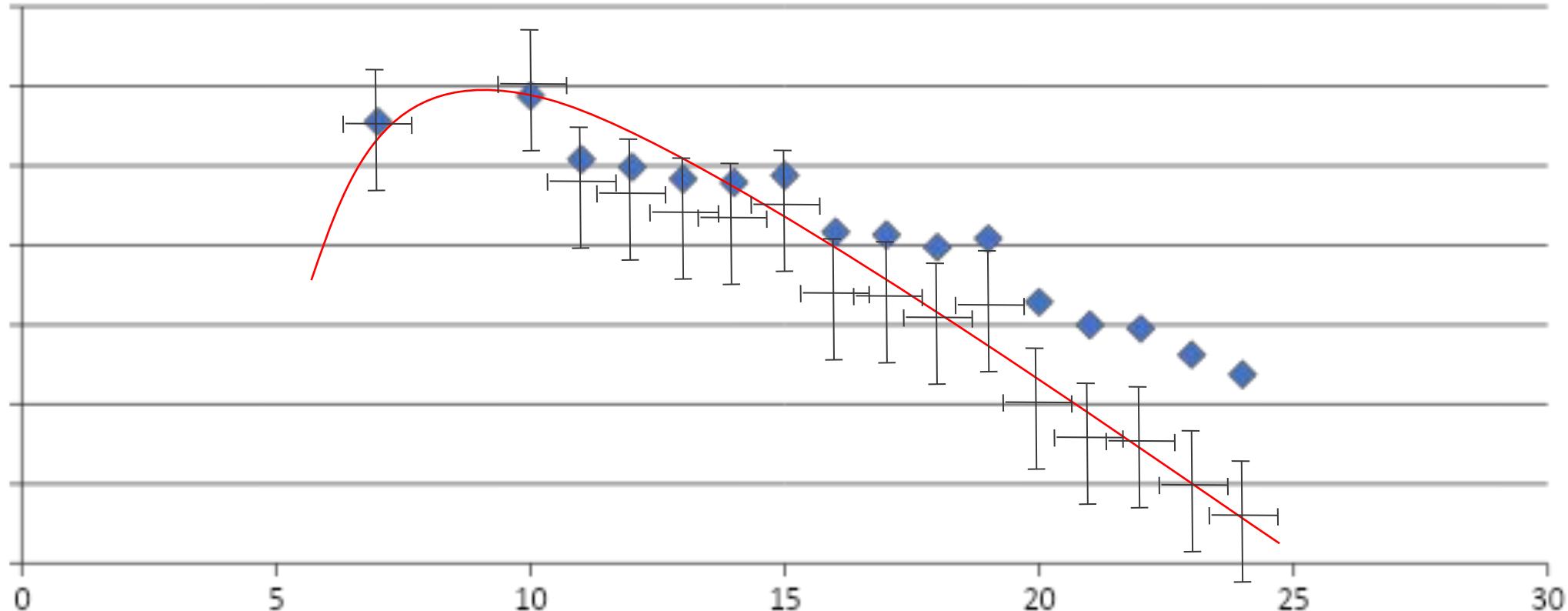
$$|\vec{g}_1| = \frac{2 \cdot \pi}{d_1} \quad |\vec{g}_2| = \frac{2 \cdot \pi}{d_2}$$

$$|\vec{G}| = |\vec{g}_2 - \vec{g}_1| = \frac{2 \cdot \pi}{D}$$

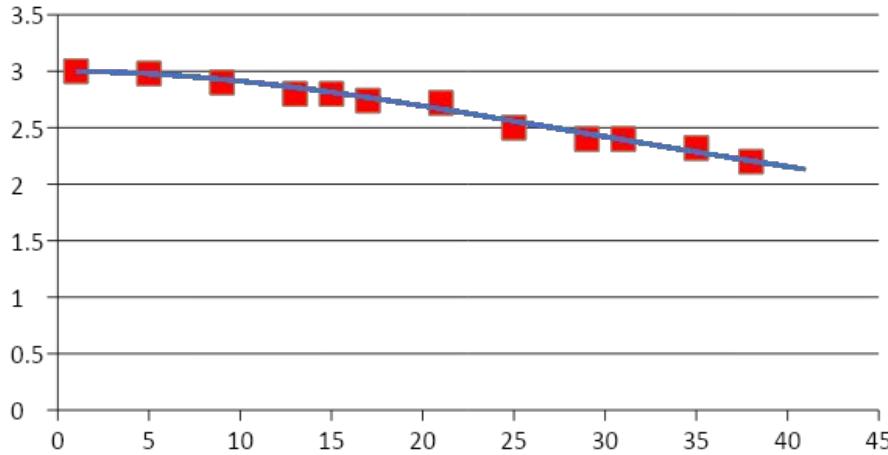


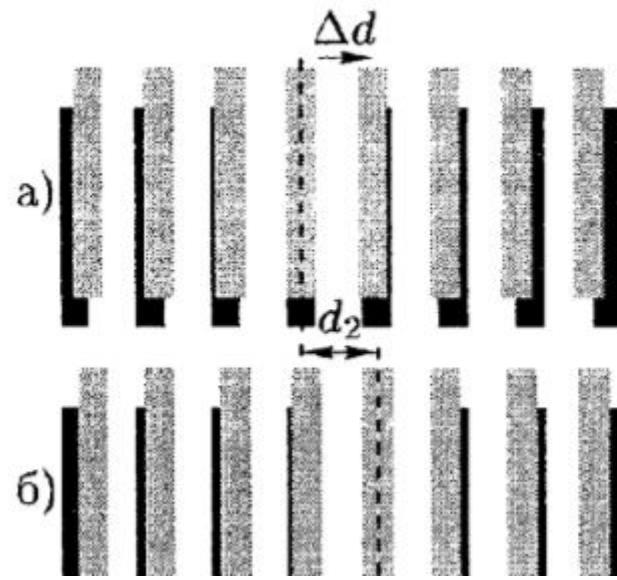
Зависимость β от θ

$$\beta = \arcsin\left(\frac{\sin \theta \cdot d_2}{\sqrt{d_1^2 + d_2^2 - 2 \cdot d_1 \cdot d_2 \cdot \cos \theta}}\right) = \arcsin\left(\frac{\sin \theta \cdot D}{d_1}\right)$$
$$\sin \beta = \frac{D \cdot \sin \theta}{d_1}$$



Оксфорд и джинсовая ткань





3. Если внимательно рассмотреть рисунок 11, то можно увидеть, что при смещении более частой решётки (на рисунке серой) вправо на расстояние Δd , совпадающие полосы (середина светлой полосы) переместятся на расстояние d_2 в ту же сторону. Поэтому, если мы будем сдвигать решётку A относительно B и полосы будут «бежать» в том же направлении, то это будет значить, что $d_A < d_B$; если же полосы будут «бежать» в обратном направлении, то $d_A > d_B$.

Где физика, что по смещениям.

$$n_1(D, \theta, d_2) = \frac{D \cdot \cos \theta \pm \sqrt{d_2^2 - D^2 \cdot \sin^2 \theta}}{D \cdot d_2} = \frac{\cos \theta}{d_2} \pm \frac{\sqrt{d_2^2 - D^2 \cdot \sin^2 \theta}}{D \cdot d_2}$$

$$\frac{\delta D}{\delta n_1} = \left(\frac{\cos \theta}{d_2} \right)' \pm \left(\frac{\sqrt{d_2^2 - D^2 \cdot \sin^2 \theta}}{D \cdot d_2} \right)' = \pm \frac{\left(\sqrt{d_2^2 - D^2 \cdot \sin^2 \theta} \right)' \cdot D \cdot d_2 - (D \cdot d_2)' \sqrt{d_2^2 - D^2 \cdot \sin^2 \theta}}{D^2 \cdot d_2^2}$$

$$\frac{\delta D}{\delta n_1} = \pm \frac{\frac{1}{2} \left(d_2^2 - D^2 \cdot \sin^2 \theta \right)' \cdot D \cdot d_2 - (D \cdot d_2)' (d_2^2 - D^2 \cdot \sin^2 \theta)}{D^2 \cdot d_2^2 \cdot \sqrt{d_2^2 - D^2 \cdot \sin^2 \theta}} = \pm \frac{-d_2^3}{D^2 \cdot d_2^2 \cdot \sqrt{d_2^2 - D^2 \cdot \sin^2 \theta}}$$

$$\frac{\delta D}{\delta n_1} = \pm \frac{d_2}{D^2 \cdot \sqrt{d_2^2 - D^2 \cdot \sin^2 \theta}}$$

$$\frac{\delta \theta}{\delta n_1} = \left(\frac{\cos \theta}{d_2} \right)' \pm \left(\frac{\sqrt{d_2^2 - D^2 \cdot \sin^2 \theta}}{D \cdot d_2} \right)' = \frac{-\sin \theta}{d_2} \pm \frac{-2D^2 \sin \theta \cdot \cos \theta}{2D \cdot d_2 \cdot \sqrt{d_2^2 - D^2 \cdot \sin^2 \theta}}$$

$$\frac{\delta \theta}{\delta n_1} = \frac{-\sin \theta}{d_2} \pm \frac{D \sin \theta \cdot \cos \theta}{d_2 \cdot \sqrt{d_2^2 - D^2 \cdot \sin^2 \theta}}$$

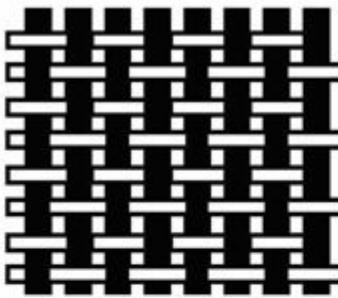
$$\frac{\delta d_2}{\delta n_1} = \left(\frac{\cos \theta}{d_2} \right)' \pm \left(\frac{\sqrt{d_2^2 - D^2 \cdot \sin^2 \theta}}{D \cdot d_2} \right)' = \frac{-\sin \theta \cdot d_2 - \cos \theta}{d_2^2} \pm \frac{\frac{2d_2}{2\sqrt{d_2^2 - D^2 \cdot \sin^2 \theta}} \cdot d_2 - \sqrt{d_2^2 - D^2 \cdot \sin^2 \theta}}{D \cdot d_2^2}$$

$$\frac{\delta d_2}{\delta n_1} = \frac{-\sin \theta \cdot d_2 - \cos \theta}{d_2^2} \pm \frac{d_2^2 - d_2^2 + D^2 \cdot \sin^2 \theta}{D \cdot d_2^2 \sqrt{d_2^2 - D^2 \cdot \sin^2 \theta}} = \frac{-\sin \theta \cdot d_2 - \cos \theta}{d_2^2} \pm \frac{D \cdot \sin^2 \theta}{d_2^2 \sqrt{d_2^2 - D^2 \cdot \sin^2 \theta}}$$

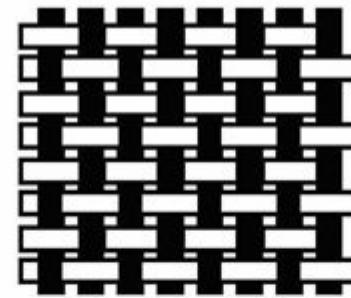
$$D = \frac{d_1 \cdot d_2}{\sqrt{d_1^2 + d_2^2 - 2 \cdot d_1 \cdot d_2 \cdot \cos \theta}}$$

Производство счетчиков counters

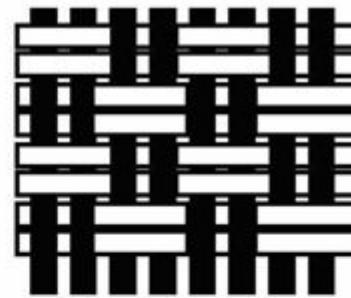
Сделать счётчик с ограничением. То есть, неподвижно накладываем и смотрим по длине полосы. Будет сделана градуировка



Plain weave
(directional)



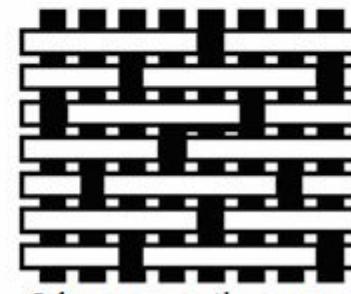
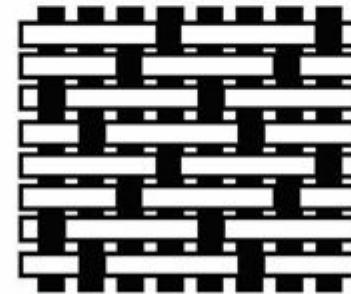
Plain weave
(uniform)



Basket (panama) weave



Various twill weaves



5-harness satin weave

Что-то про маленький уголок

1. Расстояние между полосами l будет равно половине длиной диагонали ромба, образованного пересечениями центров линий (рис. 9). Поскольку из геометрии $nl = S = L/\cos(\theta/2)$, то:

$$d_A = 2 \frac{L \sin(\theta/2)}{n \cos(\theta/2)}, \quad \text{или} \quad \operatorname{tg} \frac{\theta}{2} = \frac{d_A}{2L} n.$$

Построим график зависимости $\operatorname{tg}(\theta/2)$ от n . По точкам проведём прямую и по значению углового коэффициента определим период решётки d_A по формуле $d_A = 2Lk$, где k – значение коэффициента наклона графика.

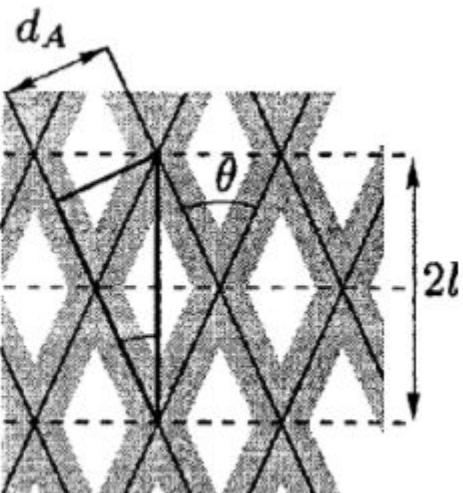


Рис. 9

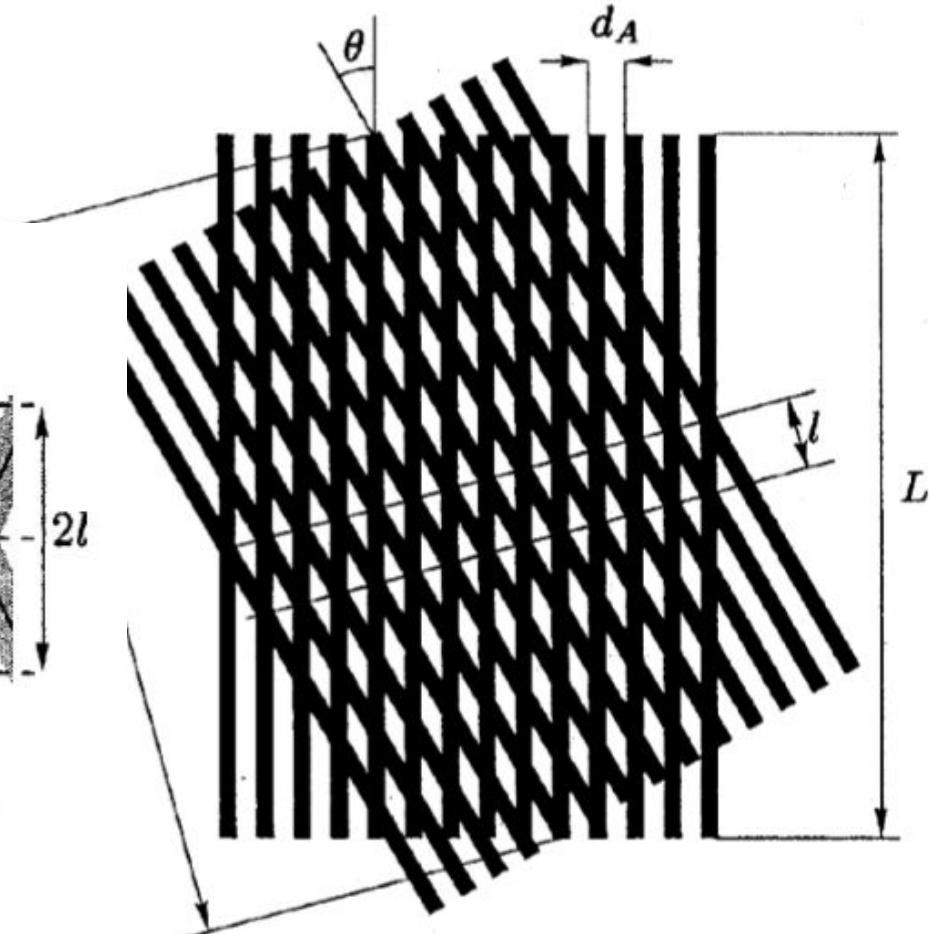
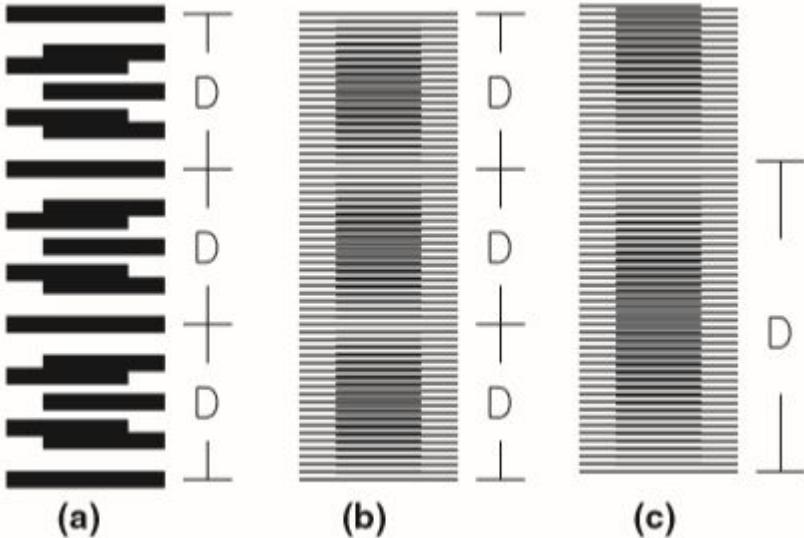


Рис. 1



phenomenon that occurs when patterns of lines with different spacings extend from the left toward the center with a spacing of $d = 1/6$ in. It extends from the left toward the center with a spacing of $d' = 1/8$ in. In the middle, a repeating pattern with period $D = 1/2$ in can be seen. At the position marked D in the figure, the lines extending from left and right overlap. The visual significance of being in phase is that in the underlying white paper they do not overlap. If we were to look at this pattern in phase would have an overlap greater than zero. (Visual significance of being in phase is that in the underlying white paper they do not overlap.) In Fig. 4(b) the spacings are $d = 1/40$ in and $d' = 1/42$ in, and in 4(c) $d = 1/40$ in and $d' = 1/41$ in. The lighter toned regions in the middle sections of those figures are places where the two sets of lines are in phase, producing light fringes (creating light stripes). Halfway between them are dark fringes where the lines do not overlap, and more of the underlying white paper is blacked out. An important qualitative feature of the moiré patterns, seen in Fig. 4(b) and (c), is that as the two spacings d and d' become closer to each other, the moiré fringes become broader (will become wider).

перестают совпадать — тёмные (рис. 10). Совпадение полос происходит через интервал L , на котором у решётки, например А, укладывается на один период большого элемента решётки. светлая полоса светлая полоса

ностью перекрываются в средней части, они в фазе) полностью перекрываются в средней части, они в фазе) fully overlap. The visual significance of being in phase is that in the underlying white paper they do not overlap. If we were to look at this pattern in phase would have an overlap greater than zero. (Visual significance of being in phase is that in the underlying white paper they do not overlap.) In Fig. 4(b) the spacings are $d = 1/40$ in and $d' = 1/42$ in, and in 4(c) $d = 1/40$ in and $d' = 1/41$ in. The lighter toned regions in the middle sections of those figures are places where the two sets of lines are in phase, producing light fringes (creating light stripes). Halfway between them are dark fringes where the lines do not overlap, and more of the underlying white paper is blacked out. An important qualitative feature of the moiré patterns, seen in Fig. 4(b) and (c), is that as the two spacings d and d' become closer to each other, the moiré fringes become broader(станет более широкой).

A quantitative measure of the distance D between successive light fringes can be derived as follows. If two lines overlap at one location, there will be another location of overlap at a distance D , where for so

$$D = kd = (k + 1)d' \quad (d' < d).$$

giving a general formula for the fringe

$$D = kd = \frac{dd'}{|d - d'|}.$$

As this formula makes clear, when the become closer, the denominator approaches zero, and the distance D between the fringes grows without bound. In Fig. 2(a), the overlay thread counter, d corresponds to the density of the parallel threads of the fabric (d is the number of threads per inch) and d' corresponds to the distance between the lines of the overlay. Since the lines of the overlay converge, d' decreases from left to right, approaching zero. The fringes converge from a spacing of $d_1 = 1/30$ inches to $d_2 = 1/60$ inches. The fabric of Fig. 2(b) is woven with 37 threads per inch. The transparency made from Fig. 2(a) laid on a fabric woven at 40 threads per inch shows the resulting interference pattern.

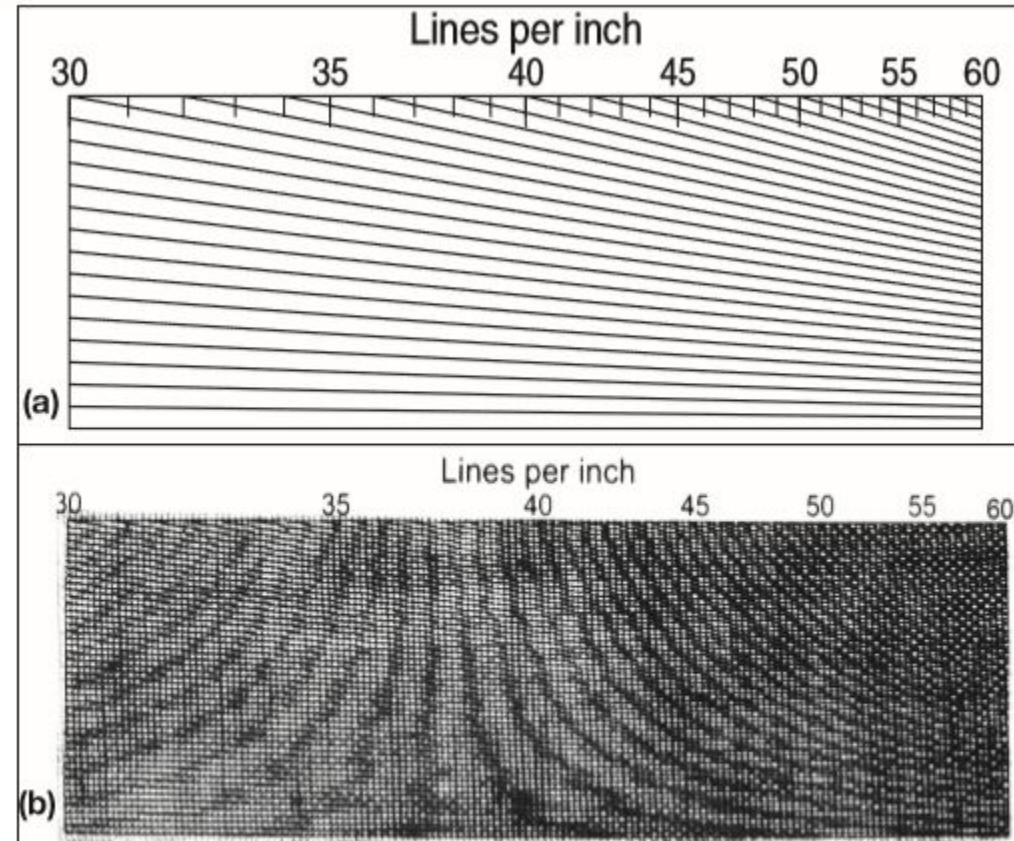
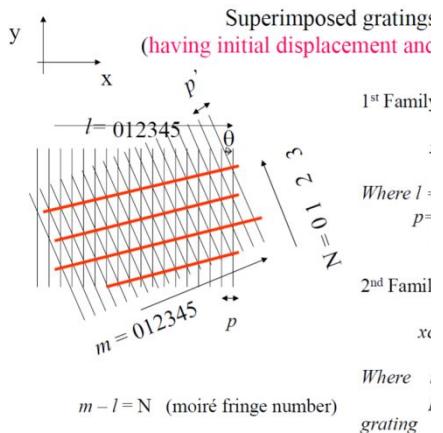


Fig. 2. (a) An overlay thread counter. (b) Transparency made from Fig. 2(a) laid on a fabric woven at 40 threads per inch.

формулы, когда два интервала d и d' становятся близкими, знаменатель приближается к нулю, и расстояние D между полосами растет без предела. В изображении Fig. 2 (a), линии перекрывающей нити соответствуют плотности параллельных нитей ткани (d - количество нитей на дюйм), а d' - расстоянию между линиями перекрывающей. Поскольку линии перекрывающей сходятся, d' уменьшается слева направо. В изображении Fig. 2 (a), линии сходятся с интервалом, равным 1/30 дюйма. Ткань Fig. 2 (b) сплетено с таким количеством нитей, что в некоторый момент вдоль ткани линии верхнего слоя D приближаются к нулю, создавая картину края, какую мы видим в изображении Fig. 2 (b).

УГОЛ

Small angle rotation and approximation approach



$$m - (p-p')/p = \text{length change/ original length} = \varepsilon_x \text{ (strain in x direction)}$$

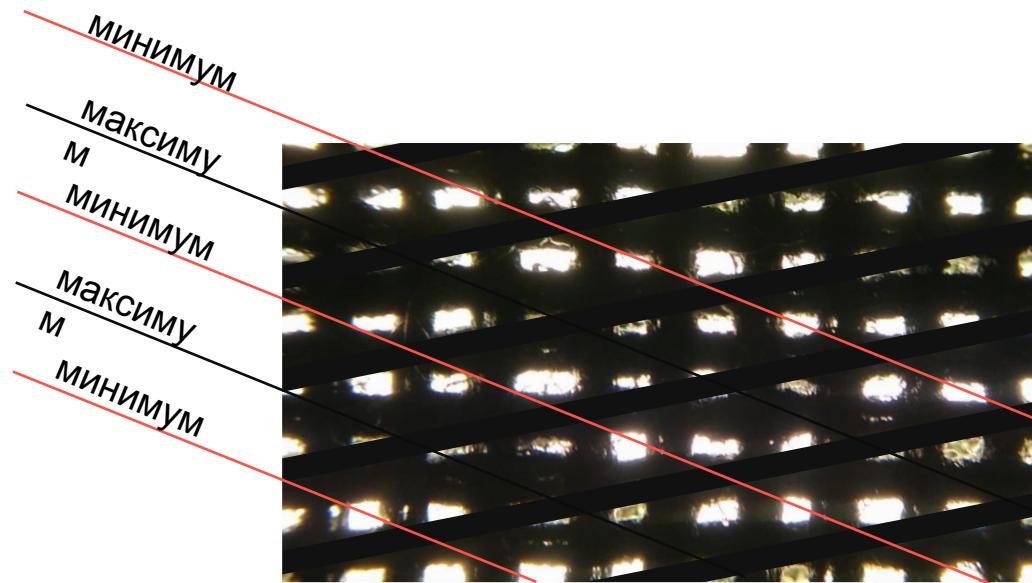
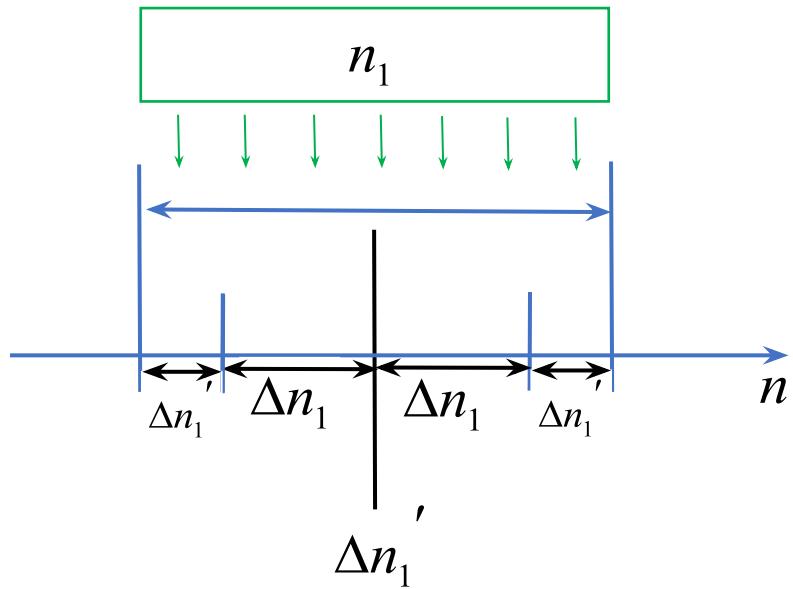
$$\varepsilon_x x + \theta y = Np'$$

If θ is small, then $\sin \theta \approx \theta$.
Equation implies N depends on the initial pitches of the the gratings, and their initial relative position and orientation.

Fringe shift can be used to measure the change of pitch (strain),
Or change in relative position (translation) and orientation (rotation)

$$x(p-p')/p + \theta y = Np'$$

Conclusions



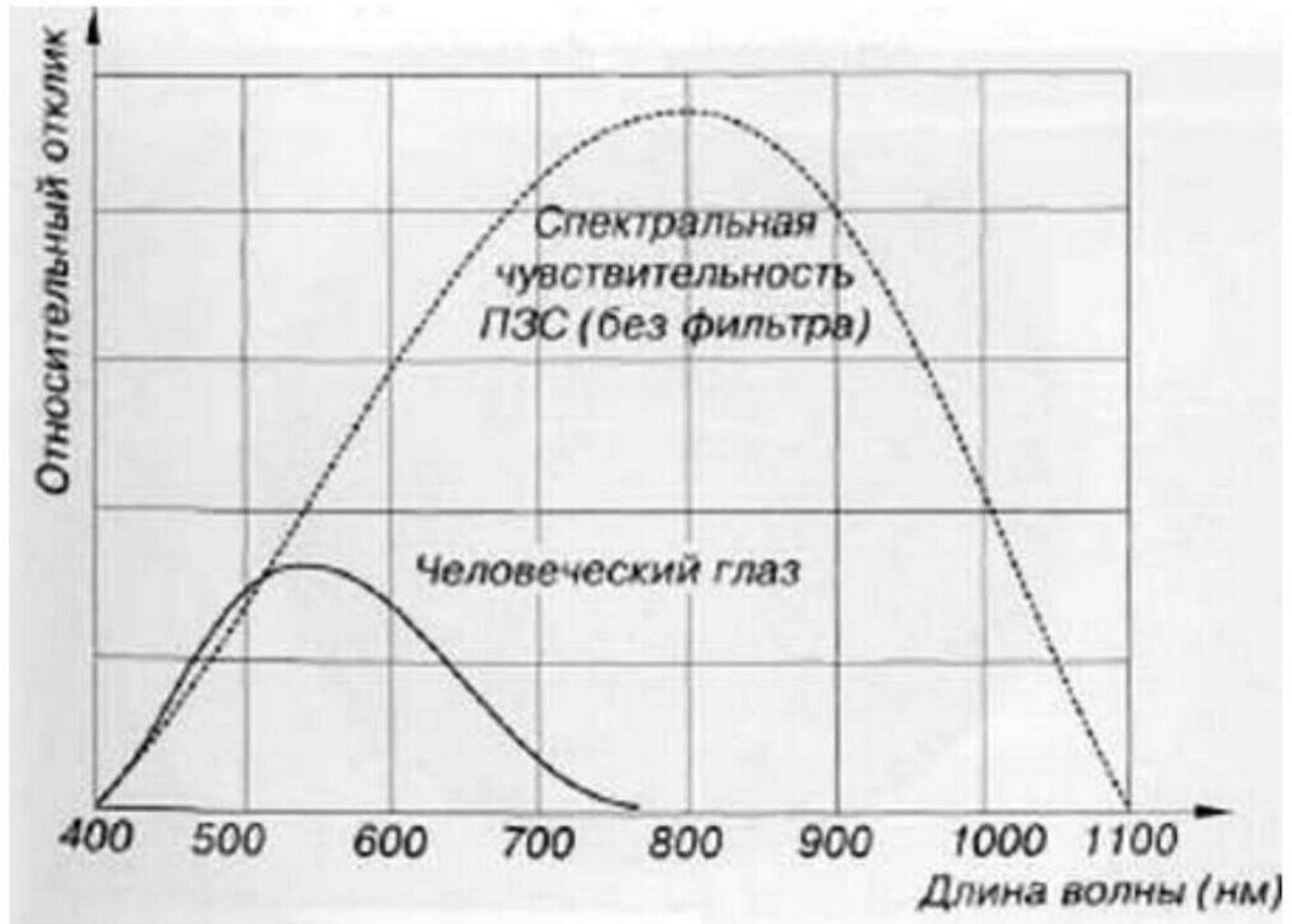
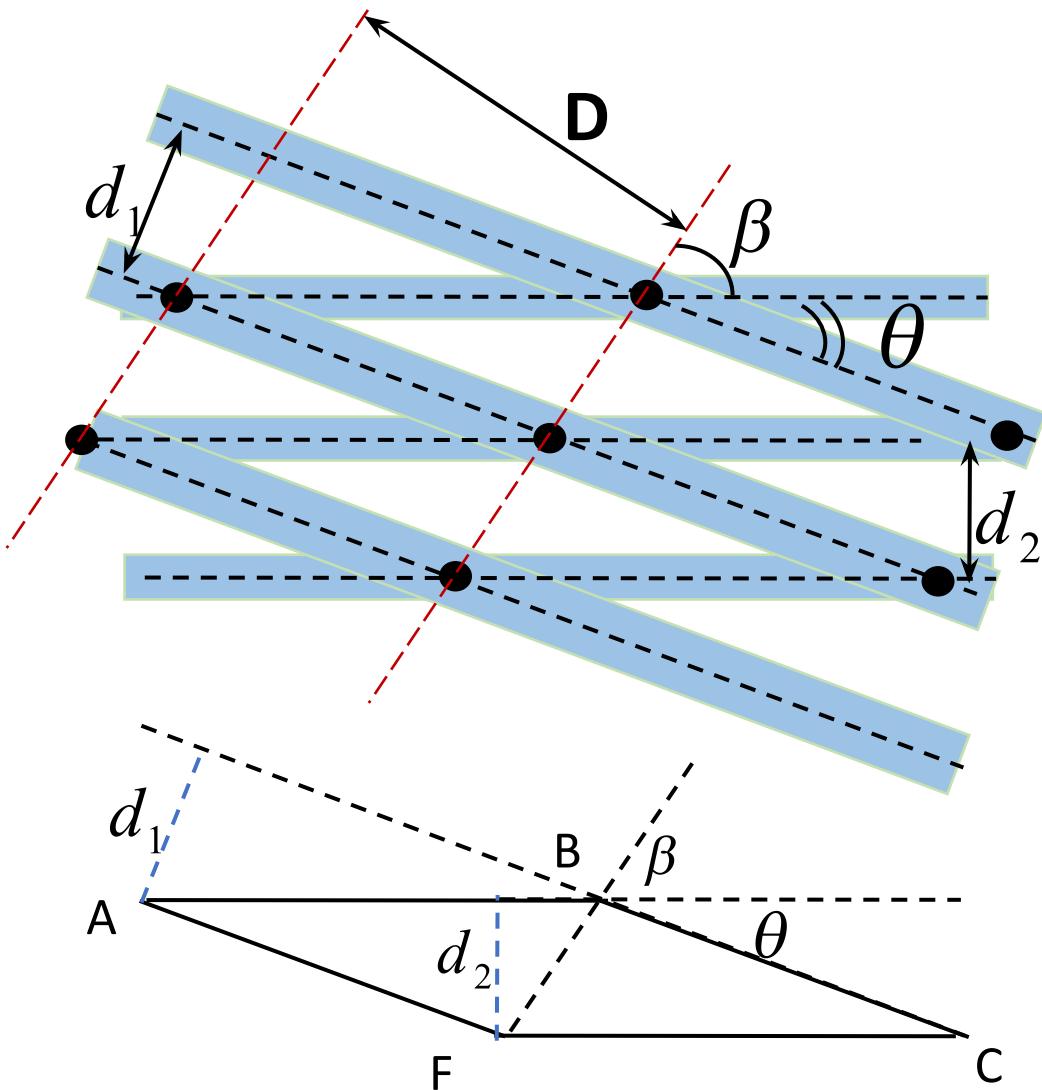


Рис. 5.15 . Спектральная чувствительность глаза и ПЗС-матрицы

Теперь. Будут спрашивать, что такое люкс. Люкс - это люмен на квадратный метр. Один люмен равен световому потоку, испускаемому точечным источником, с силой света, равной одной канделе, в телесный угол величиной в один стерадиан. Канделла -это единица силы света в СИ.

Geometric Moire'



$$d_1 = AB \cdot \sin \theta = FB \cdot \sin(\beta + \theta)$$

$$d_2 = AF \cdot \sin \theta = FB \cdot \sin \beta$$

$$D = FC \cdot \sin \beta = AB \cdot \sin \beta$$

$$\sin \beta = \frac{D \cdot \sin \theta}{d_1}$$

$$FB = \frac{d_1}{\sin(\beta + \theta)} = \frac{d_1}{\sin \beta \cdot \cos \theta + \cos \beta \cdot \sin \theta} =$$

$$= \frac{d_1}{\frac{D \cdot \sin \theta}{d_1} \cdot \cos \theta + \sqrt{1 - \frac{D^2 \cdot \sin^2 \theta}{d_1^2}} \cdot \sin \theta}$$

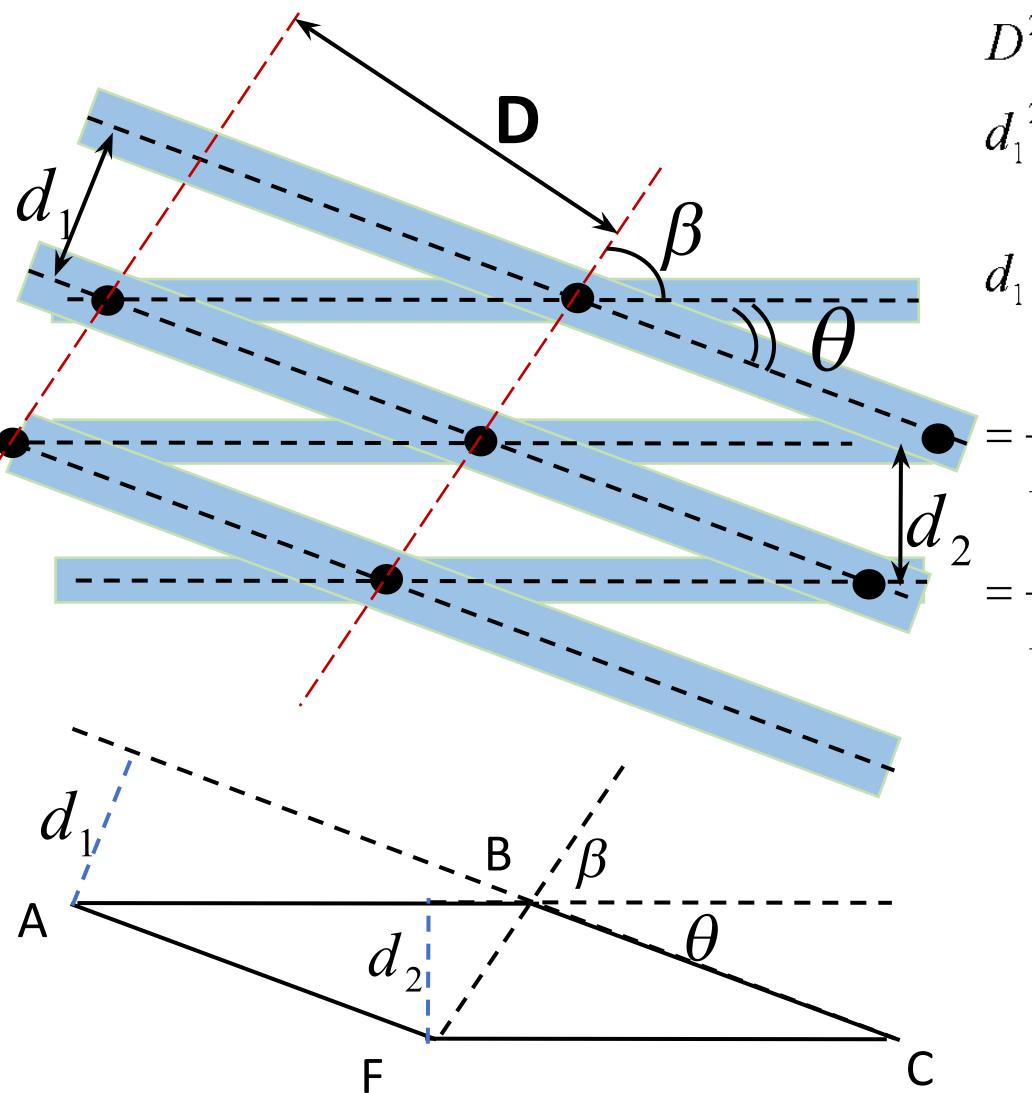
$$\cdot d_2 = \frac{d_1^2 \cdot D \cdot \sin \theta}{d_1 \cdot (D \cdot \sin \theta \cdot \cos \theta + \sqrt{d_1^2 - D^2 \cdot \sin^2 \theta} \cdot \sin \theta)} =$$

$$= \frac{d_1 \cdot D}{D \cdot \cos \theta + \sqrt{d_1^2 - D^2 \cdot \sin^2 \theta}}$$

$$D \cdot \cos \theta \cdot d_2 + \sqrt{d_1^2 - D^2 \cdot \sin^2 \theta} \cdot d_2 = d_1 \cdot D$$

$$D^2(d_1^2 - 2 \cdot d_1 d_2 \cdot \cos \theta + d_2^2 \cdot \cos^2 \theta) = d_2^2 \cdot d_1^2 - d_2^2 \cdot D^2 \cdot \sin^2 \theta$$

Geometric Moire'



$$D^2(d_1^2 - 2 \cdot d_1 d_2 \cdot \cos \theta + d_2^2 \cdot \cos^2 \theta) = d_2^2 \cdot d_1^2 - d_2^2 \cdot D^2 \cdot \sin^2 \theta$$

$$D^2 \cdot d_1^2 - 2 \cdot D^2 \cdot d_1 d_2 \cdot \cos \theta + D^2 \cdot d_2^2 \cdot \cos^2 \theta = d_2^2 \cdot d_1^2 - d_2^2 \cdot D^2 \cdot \sin^2 \theta$$

$$d_1^2(D^2 - d_2^2) - 2 \cdot D^2 \cdot d_1 d_2 \cdot \cos \theta + D^2 \cdot d_2^2 = 0$$

$$d_1 = \frac{D^2 \cdot d_2 \cdot \cos \theta \pm \sqrt{D^4 \cdot d_2^2 \cdot \cos^2 \theta - D^2 \cdot d_2^2 \cdot (D^2 - d_2^2)}}{(D^2 - d_2^2)} =$$

$$= \frac{D \cdot d_2}{D^2 - d_2^2} \cdot (D \cdot \cos \theta \pm \sqrt{D^2 \cdot (\cos^2 \theta - 1) + d_2^2}) =$$

$$= \frac{D \cdot d_2}{D^2 - d_2^2} \cdot (D \cdot \cos \theta \pm \sqrt{d_2^2 - D^2 \cdot \sin^2 \theta})$$

Errors

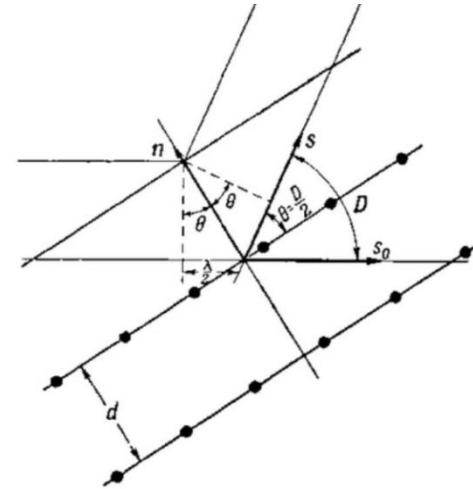
$$d_1(D, \theta, d_2) = \frac{D^2 \cdot d_2 \cdot \cos \theta \pm D \cdot d_2 \sqrt{d_2^2 - D^2 \cdot \sin^2 \theta}}{D^2 - d_2^2}$$

$$\Delta d_1 = \sqrt{\sum_{n=1}^i \left(\frac{\partial d_1}{\partial x_i} \Delta x_i \right)^2} = \sqrt{\left(\frac{\partial d_1}{\partial d_2} \Delta d_2 \right)^2 + \left(\frac{\partial d_1}{\partial \theta} \Delta \theta \right)^2 + \left(\frac{\partial d_1}{\partial D} \Delta D \right)^2}$$

$$\frac{\partial d_1}{\partial d_2} = \frac{D^4 \cdot \cos \theta \pm D^2 \frac{2Dd_2^2 - D^3 \cdot \sin^2 \theta}{\sqrt{d_2^2 - D^2 \cdot \sin^2 \theta}} \mp d_2^2 \frac{2Dd_2^2 - D^3 \cdot \sin^2 \theta}{\sqrt{d_2^2 - D^2 \cdot \sin^2 \theta}} + D^2 \cdot d_2^2 \cdot \cos \theta \pm 2D \cdot d_2^2 \sqrt{d_2^2 - D^2 \cdot \sin^2 \theta}}{(D^2 - d_2^2)^2}$$

$$D^2 = \frac{d_1^2 \cdot d_2^2}{d_1^2 + d_2^2 - 2 \cdot d_1 \cdot d_2 \cdot \cos \theta} d$$

$$D^2 = \frac{d_2^2}{n_1^2 \left(\frac{1}{n_1^2} + d_2^2 - \frac{2d_2 \cos \theta}{n_1} \right)}$$



Good afternoon,
my name is N.
Griboval.
represent
team SES
And I want
tell you my
vision of the
problem
number:
“Moiré Thr
Counter”.
address
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the problem

Here is a plan
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Considering
special case
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with practi
will make
conclusions

First it is necessary to define some concepts. In a fig1 you can see grid. It is 2-dimensional line pattern of regular nature(two-dimensional arrays with any kind of periodicity involving). The period of grid is the distance between the centers of the nearest bands of one grid. I will denote it d .

In my vision of the problem I will use number of threads per centimetre. In the fig2 we can see the example of the moire pattern. How can we get such picture?

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First it is necessary to define some concepts. In a fig1 you can see grid. It is 2-dimensional line pattern of regular nature(two-dimensional arrays with any kind of periodicity involving). The period of grid is the distance between the centers of the nearest bands of one grid. I will denote it d .

Small 'l' is the distance between the bands and 'f' is the width of the band.

In my vision of the problem I will use number of threads per centimetre.

In the fig2 we can see the example of the moire pattern. How can we get such picture?