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# Reservoir Pressure Evaluation using Multi-rate SNL

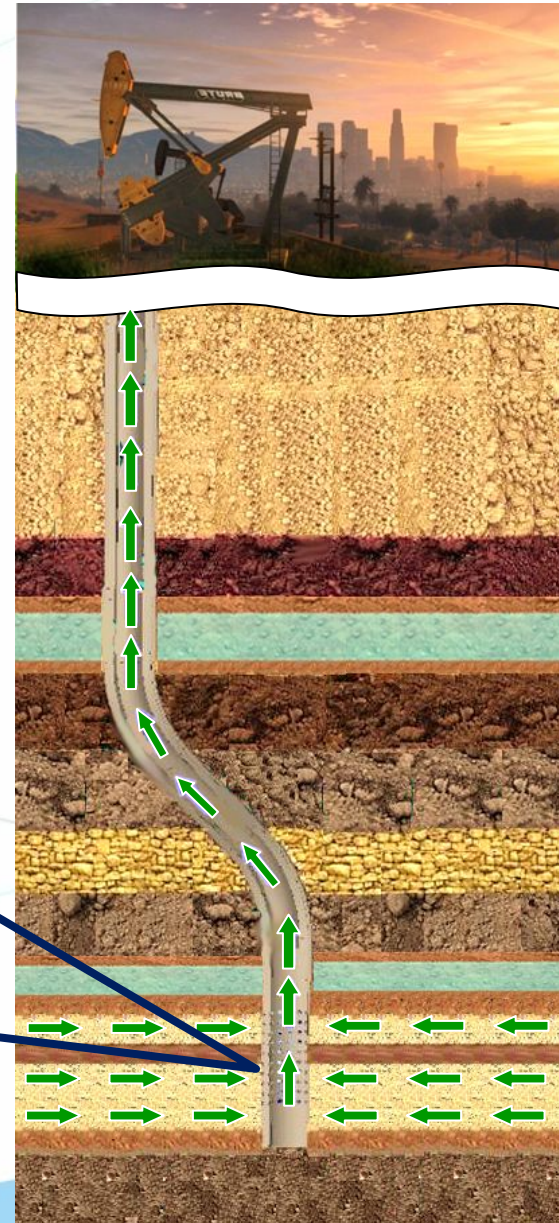
- Dr. Yulia Maslennikova, Sergey Prosvirkin,  
Dr. Irina Aslanyan
- TGT Oilfield Services

# Agenda



1. Introduction
2. Theory and Lab Tests
3. Calculation procedure
4. Case Study

# Introduction



$P_R$  – Reservoir Pressure

$$Q = \eta(P_R - P_{wf})$$

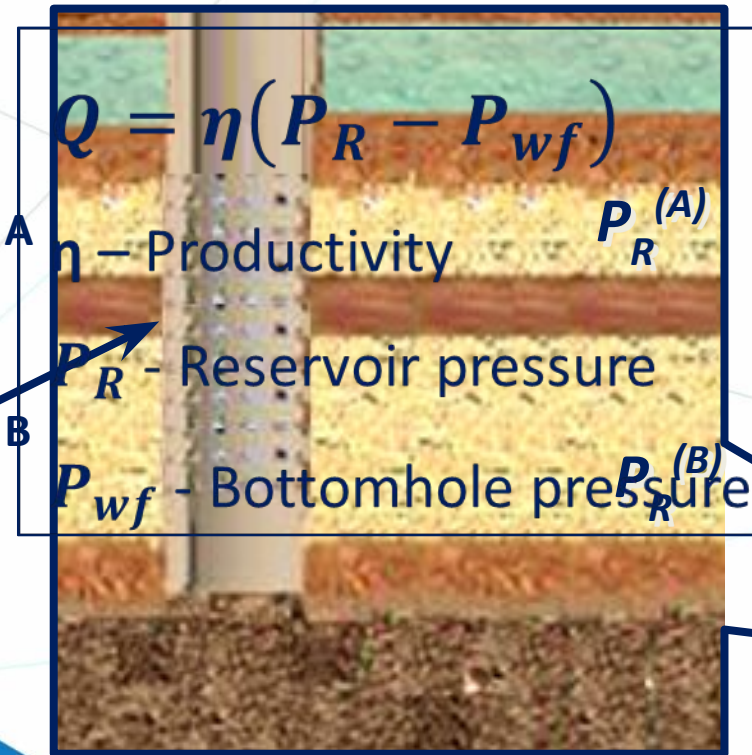
Unit A

$\eta$  – Productivity  $P_R^{(A)}$

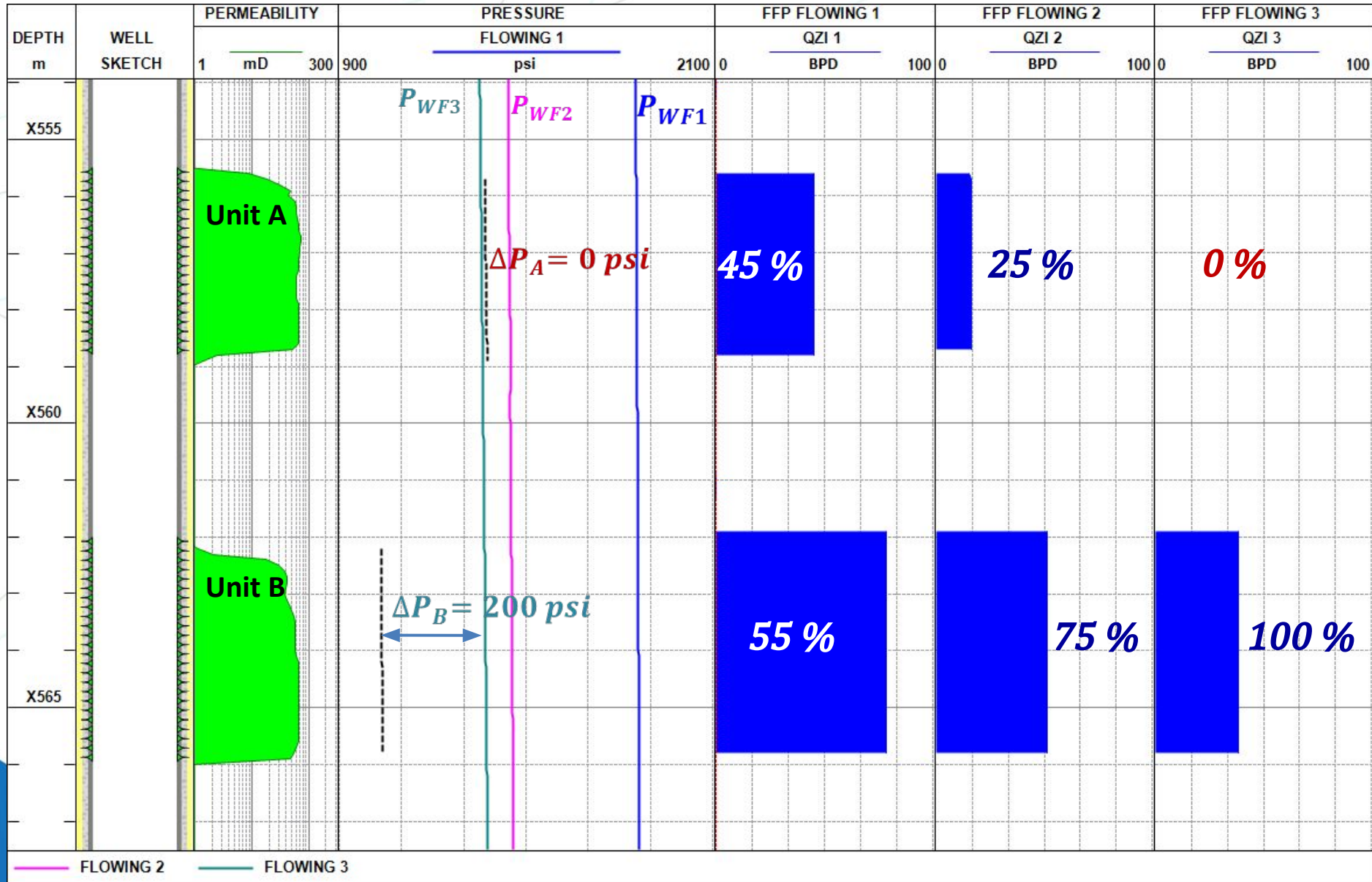
$P_R$  – Reservoir pressure

$P_{wf}$  – Bottomhole pressure  $P_R^{(B)}$

Crossflow

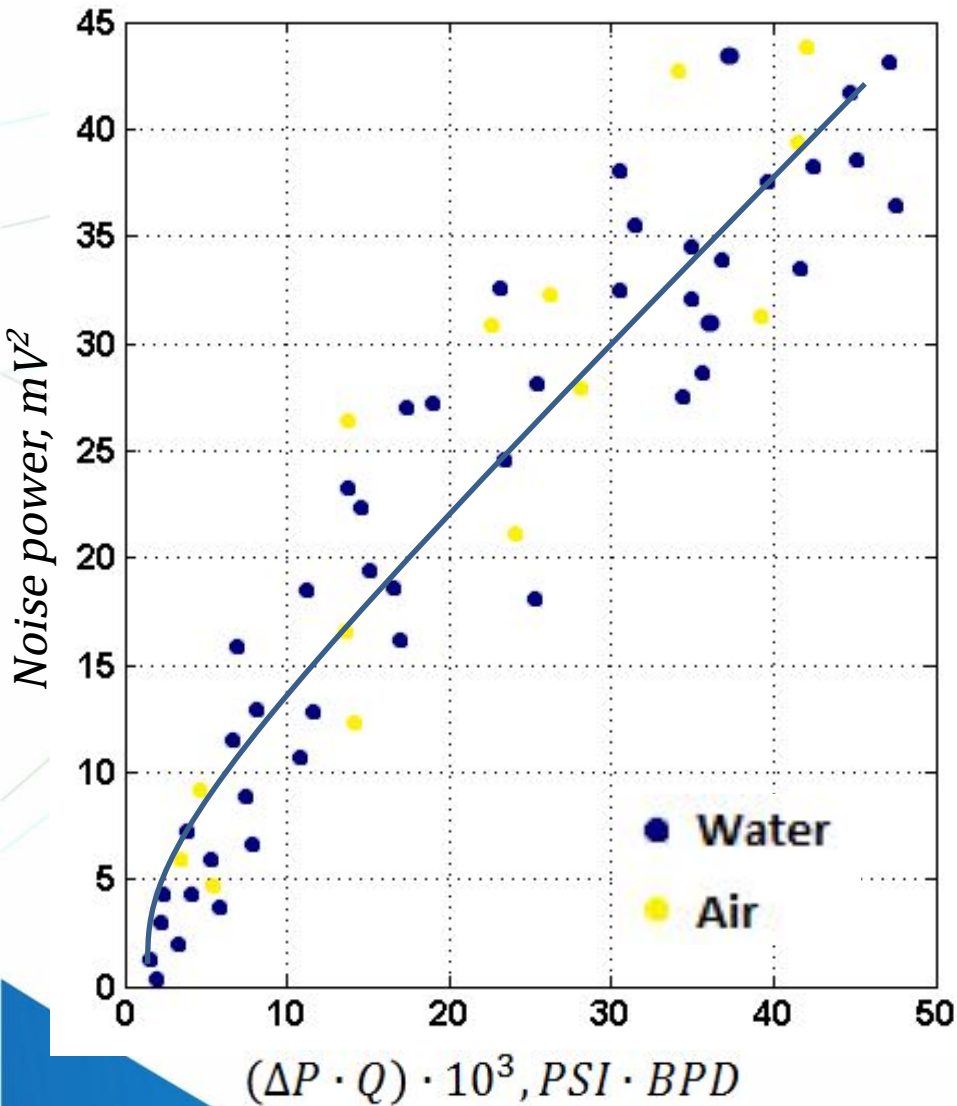


# Simulated Multi - Layered Injector



# Theory

McKinley (1994):



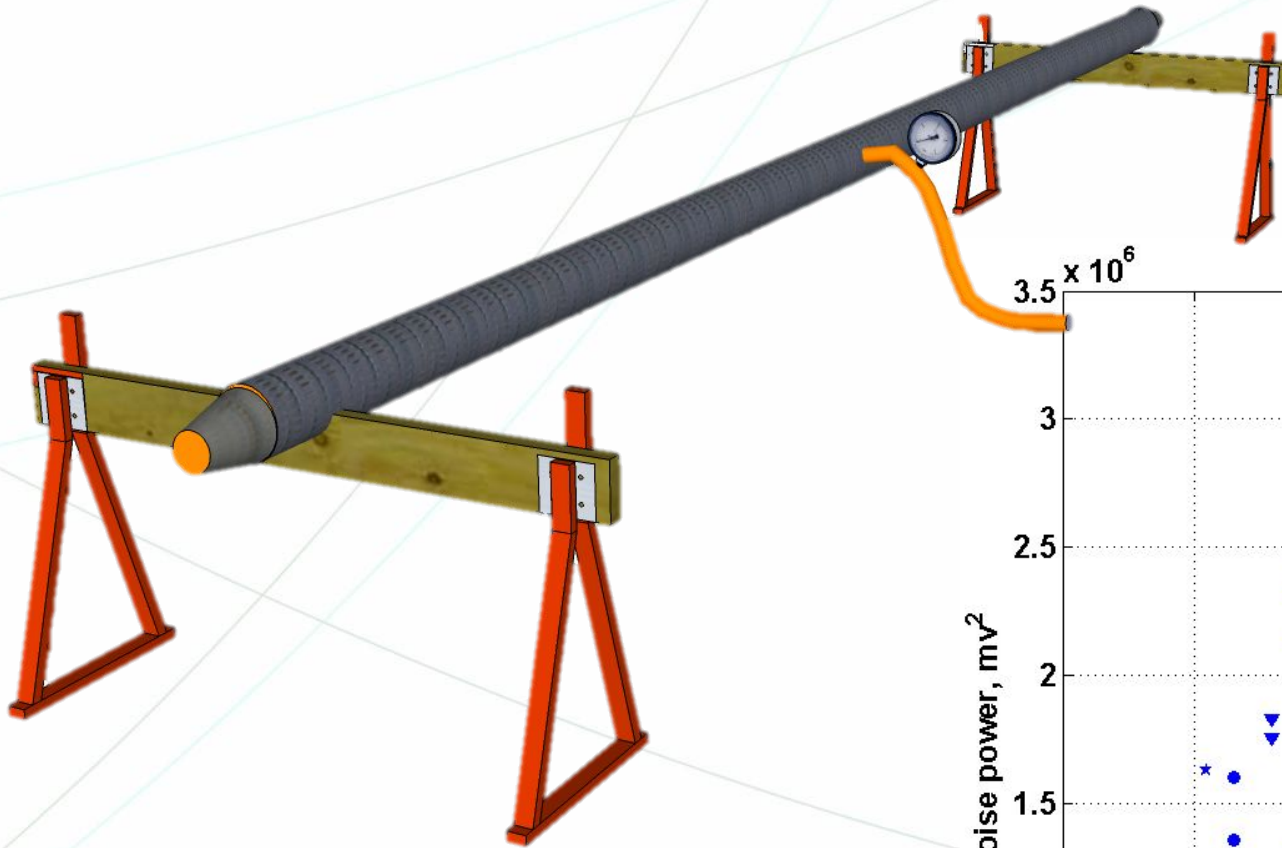
$$N \sim Q \cdot \Delta P$$

$N$  - Noise Power

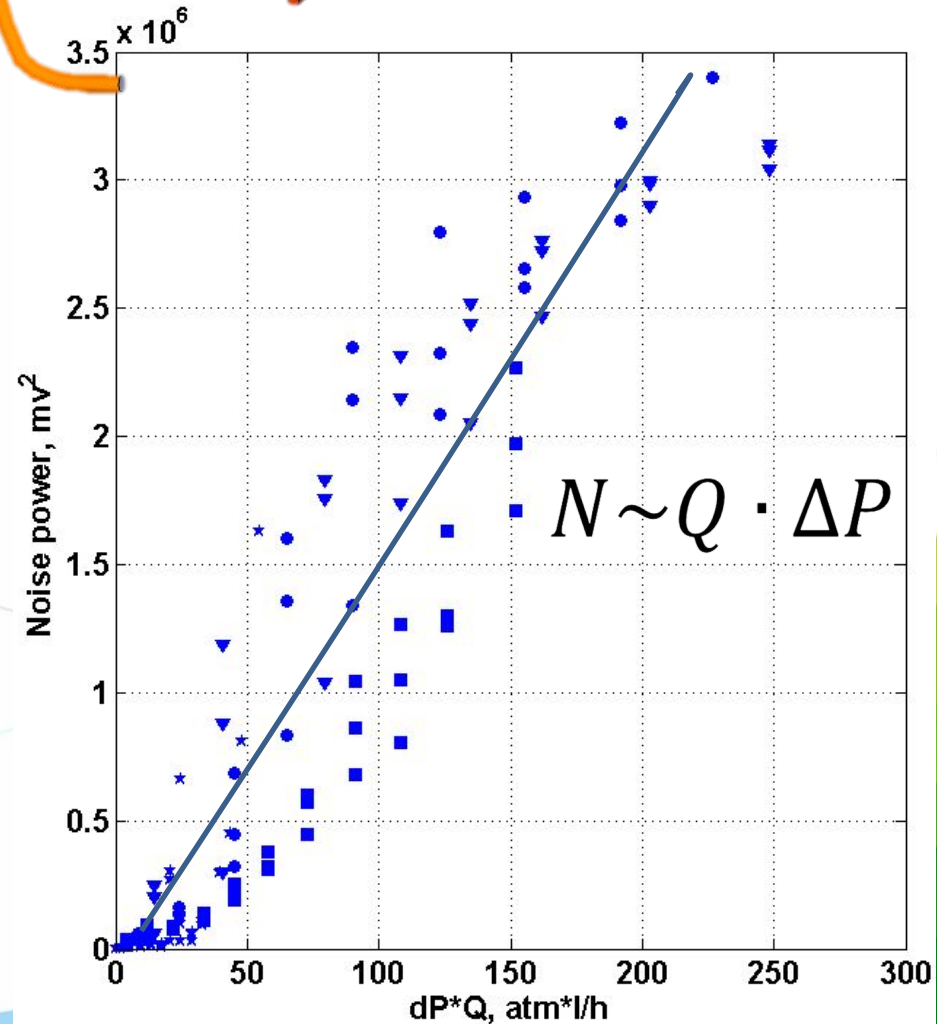
$Q$  - Volumetric rate

$\Delta P$  - Pressure drop

# Lab tests



Height	6 m
Ø Tube	3 ½"
Volume	0.029 m <sup>3</sup>
Pressure drop	0 – 5 atm
Ø Hole	1– 10 mm



**Noise Power:**

$$N = K(P_R - P_{wf})^2$$

Dual-rate for a single-phase fluid:

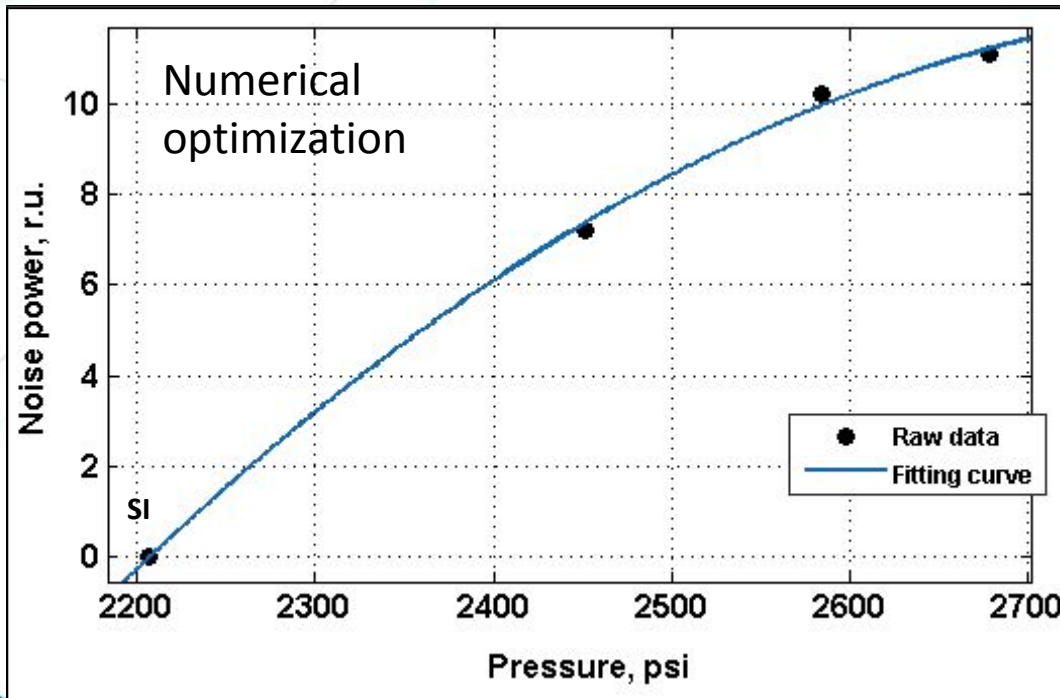
$$Q = k \cdot \Delta P$$

$$\begin{cases} N^{(1)} = K(P_R - P_{wf1})^2 \\ N^{(2)} = K(P_R - P_{wf2})^2 \end{cases}$$



$$P_R$$

$$N_{pow} = a(P_{wf} - P_R)^2 + b(P_{wf} - P_R)$$

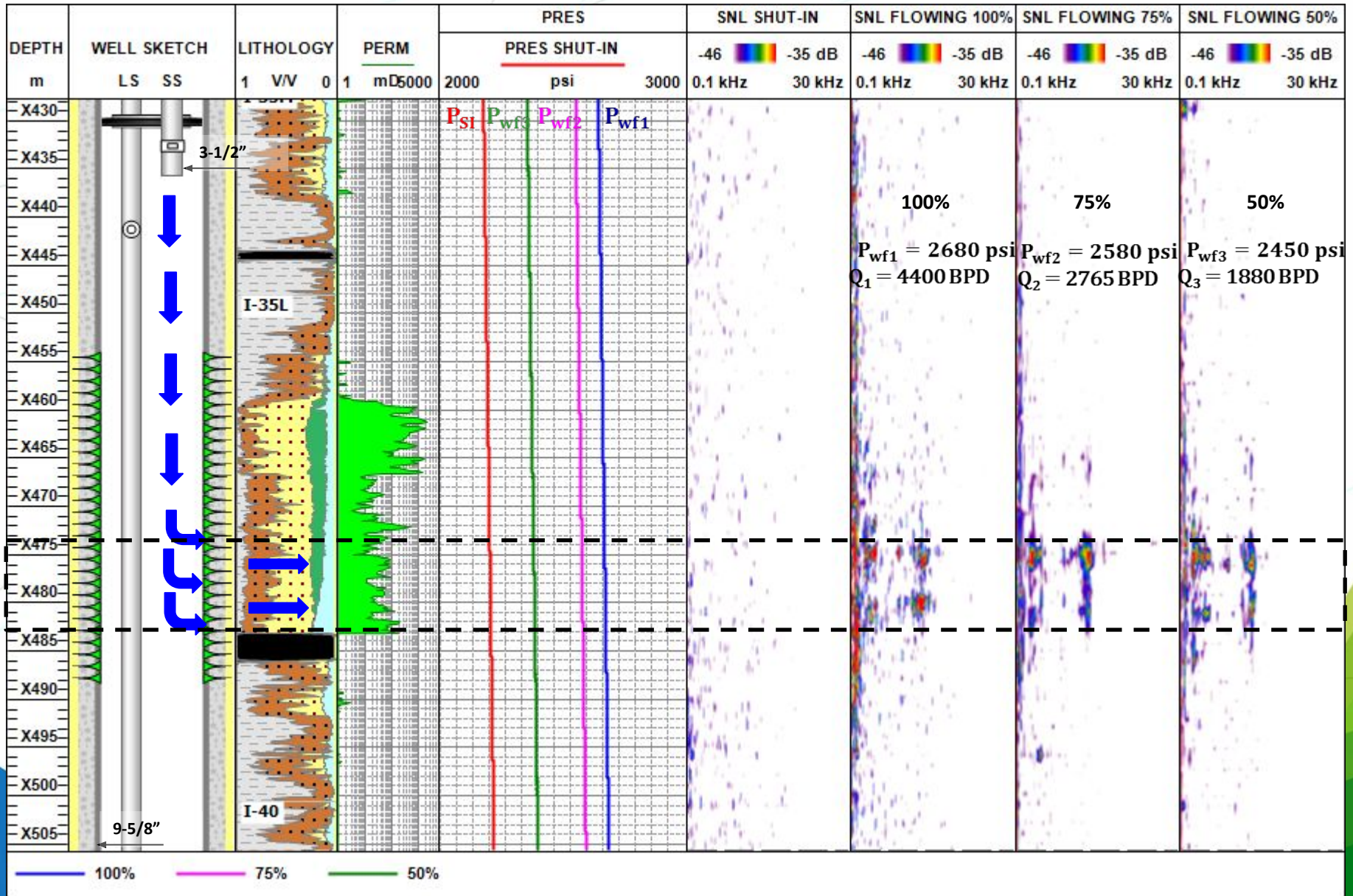


$P_R$

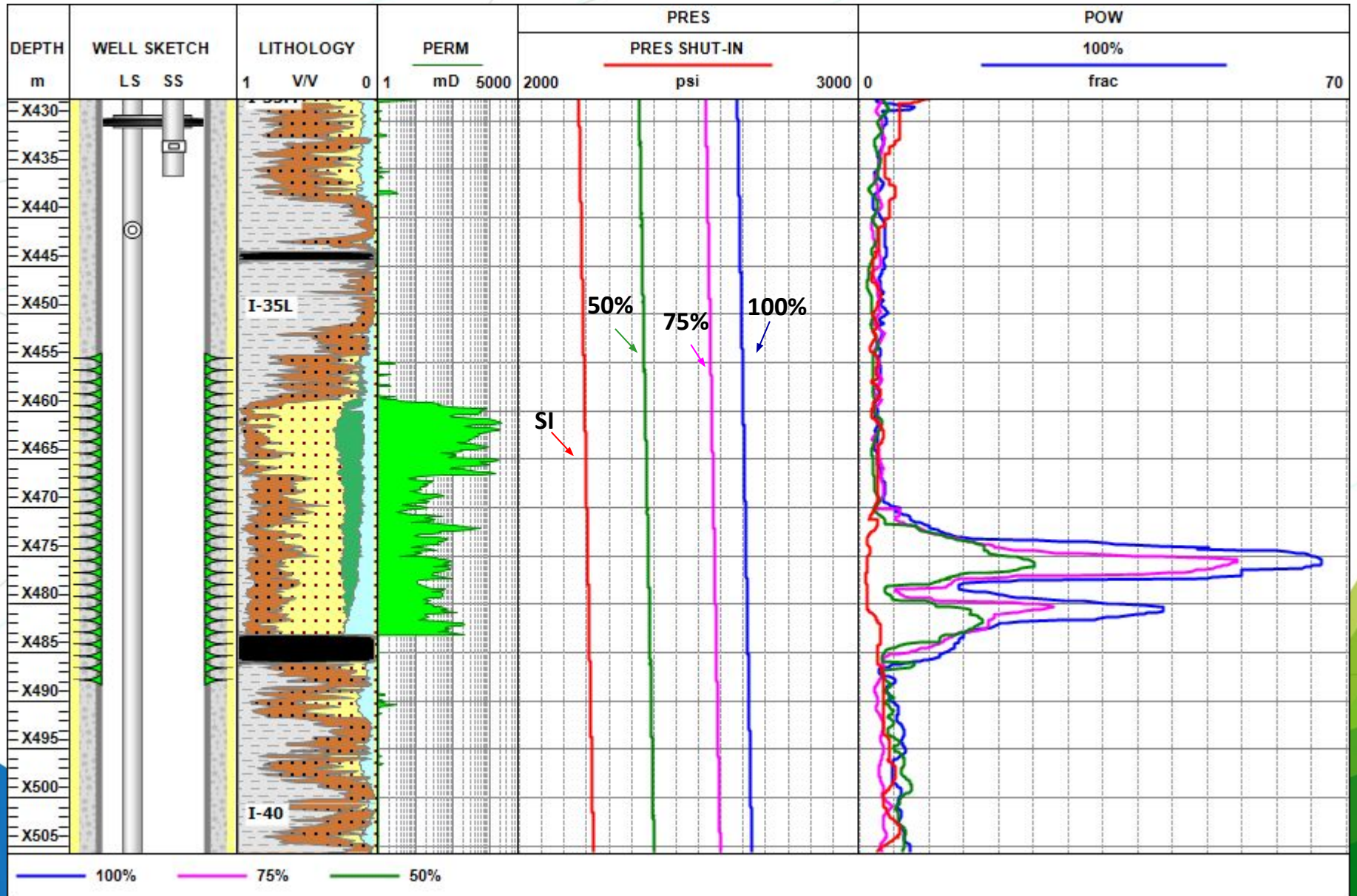


# Case Study

# Case 1. Smart completion (SS – Inj, LS – Shut-in)



# Case 1. Noise power



# Calculation procedure

Conditions	Target unit	Temperature °C	Pressure, psi	Noise power, psi	Normalized noise power, psi
Shut-in	I-35 L	56.1	2205	8.2	0
Flowing (100 %)	I-35 L	59.0	2677	19.4	11.2
Flowing (75%)	I-35 L	60.5	2582	18.4	10.2
Flowing (50%)	I-35 L	63.0	2450	15.7	7.56

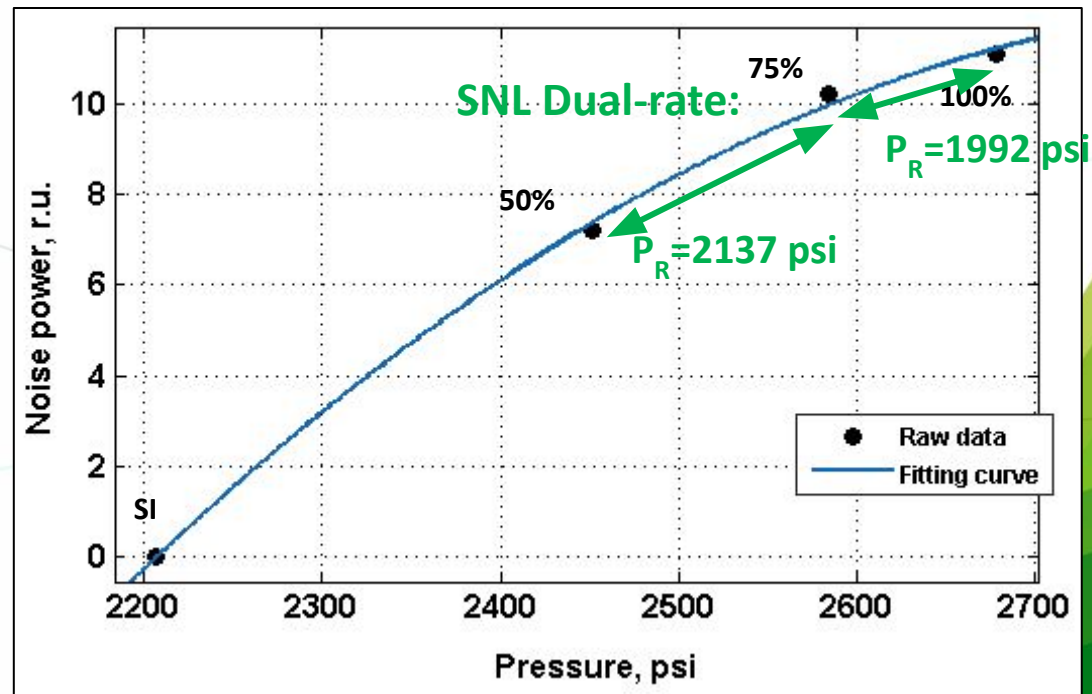
$$N_{pow} = a(P_{wf} - P_R)^2 + b(P_{wf} - P_R)$$

SNL Multi-rate:

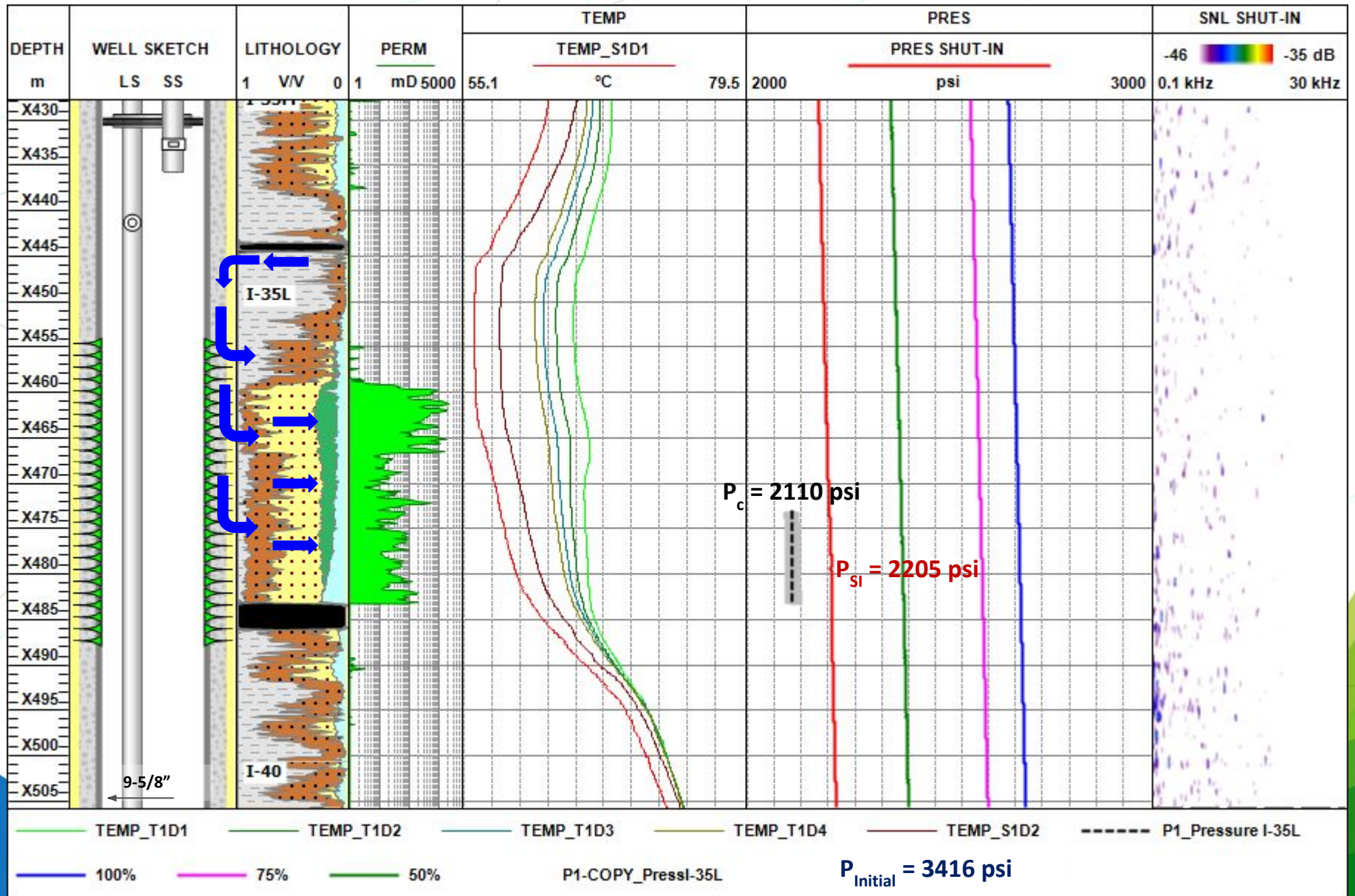
$$P_R = 2110 \text{ psi } (\pm 20);$$

$$a = 0.0015 (\pm 0.0001);$$

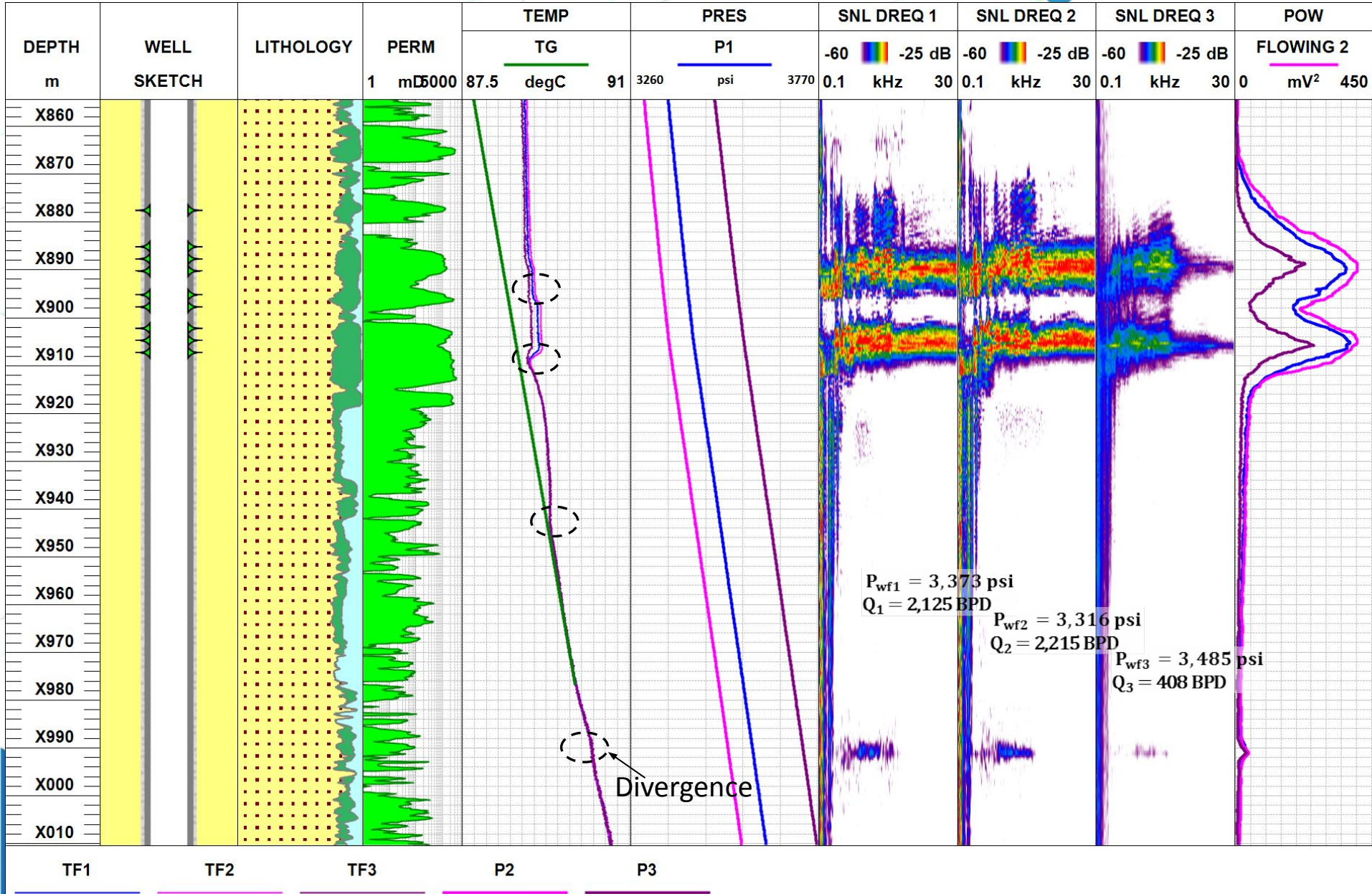
$$b = -0.037 (\pm 0.002)$$



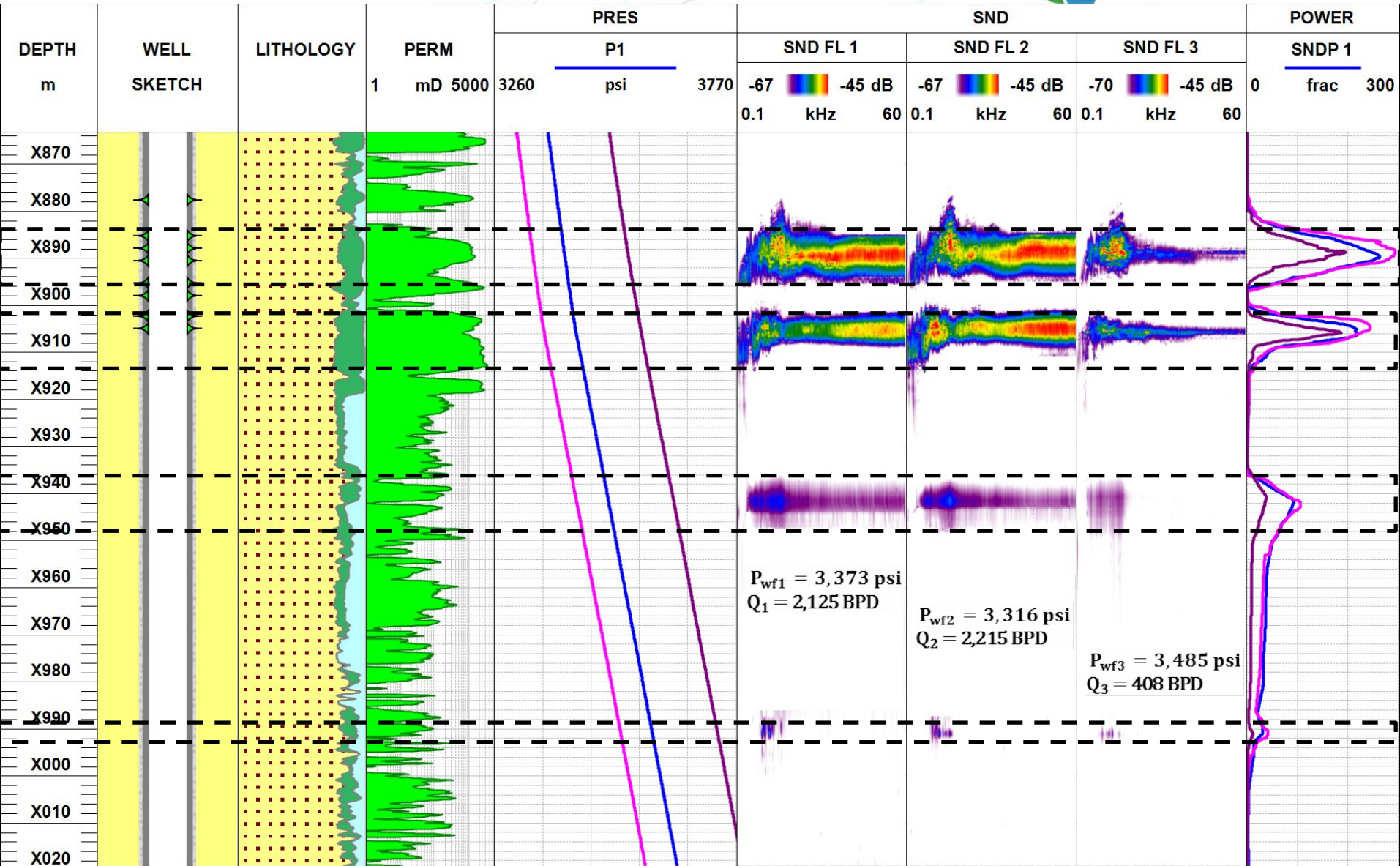
# Case 1. Shut-in



# Case 2. Oil Producer



# Case 2. Oil Producer



$P_{wf1} = 3,373 \text{ psi}$   
 $Q_1 = 2,125 \text{ BPD}$

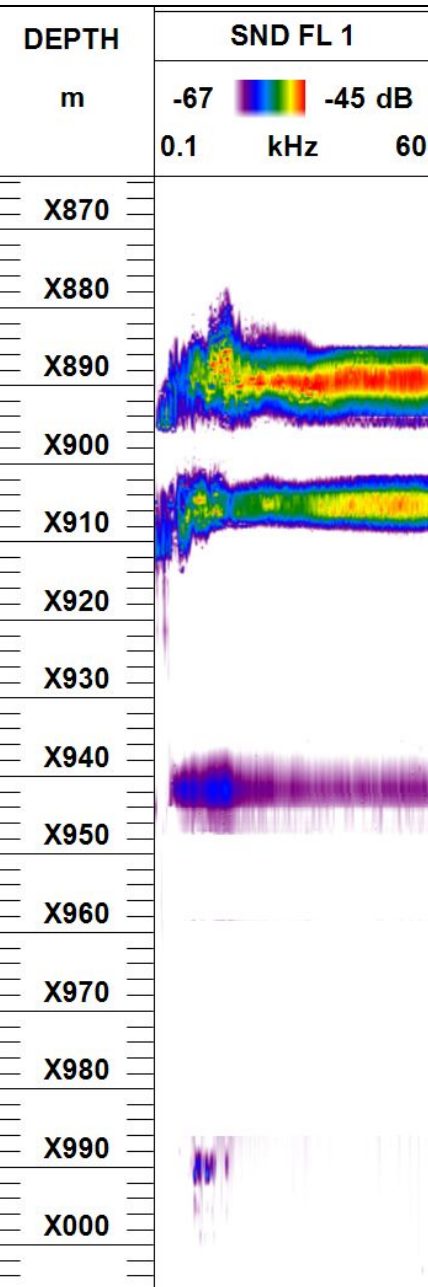
$P_{wf2} = 3,316 \text{ psi}$   
 $Q_2 = 2,215 \text{ BPD}$

$P_{wf3} = 3,485 \text{ psi}$   
 $Q_3 = 408 \text{ BPD}$

P2

P3

# Calculation procedure



Depth X475 ft:

$$N_{pow} = -0.001*(P_R - P_{wf})^2 + 0.072*(P_R - P_{wf})$$

$$P_R = 3598 \text{ psi}$$

Depth X532 ft:

$$N_{pow} = -0.001*(P_R - P_{wf})^2 + 0.073*(P_R - P_{wf})$$

$$P_R = 3617 \text{ psi}$$

Depth X948 ft:

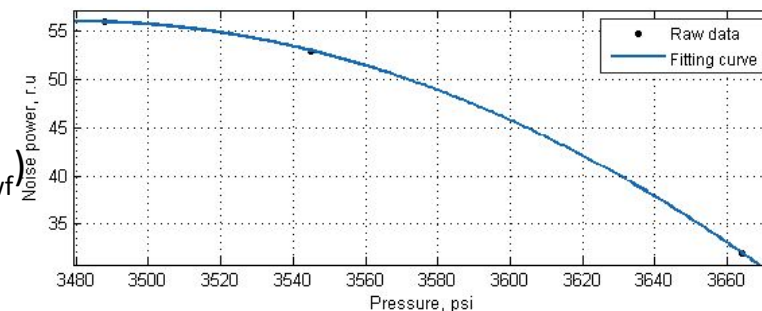
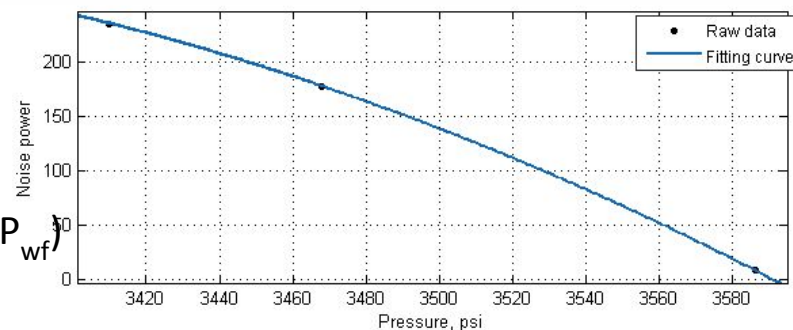
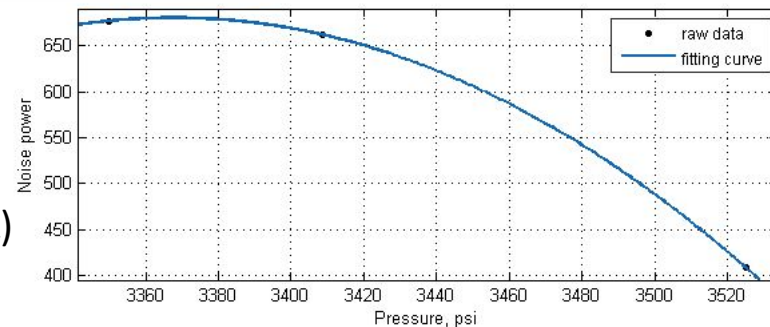
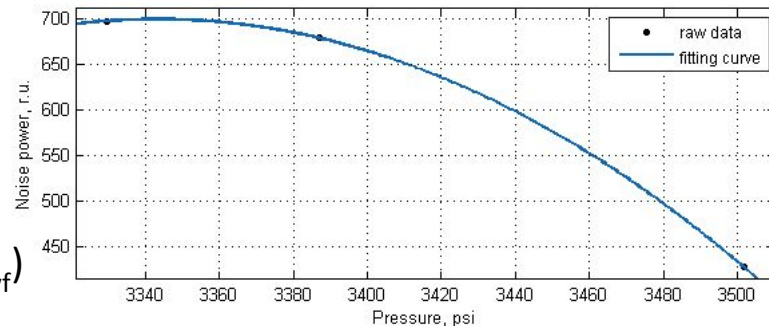
$$N_{pow} = -0.002*(P_R - P_{wf})^2 - 0.0016*(P_R - P_{wf})$$

$$P_R = 3660 \text{ psi}$$

Depth X812 ft:

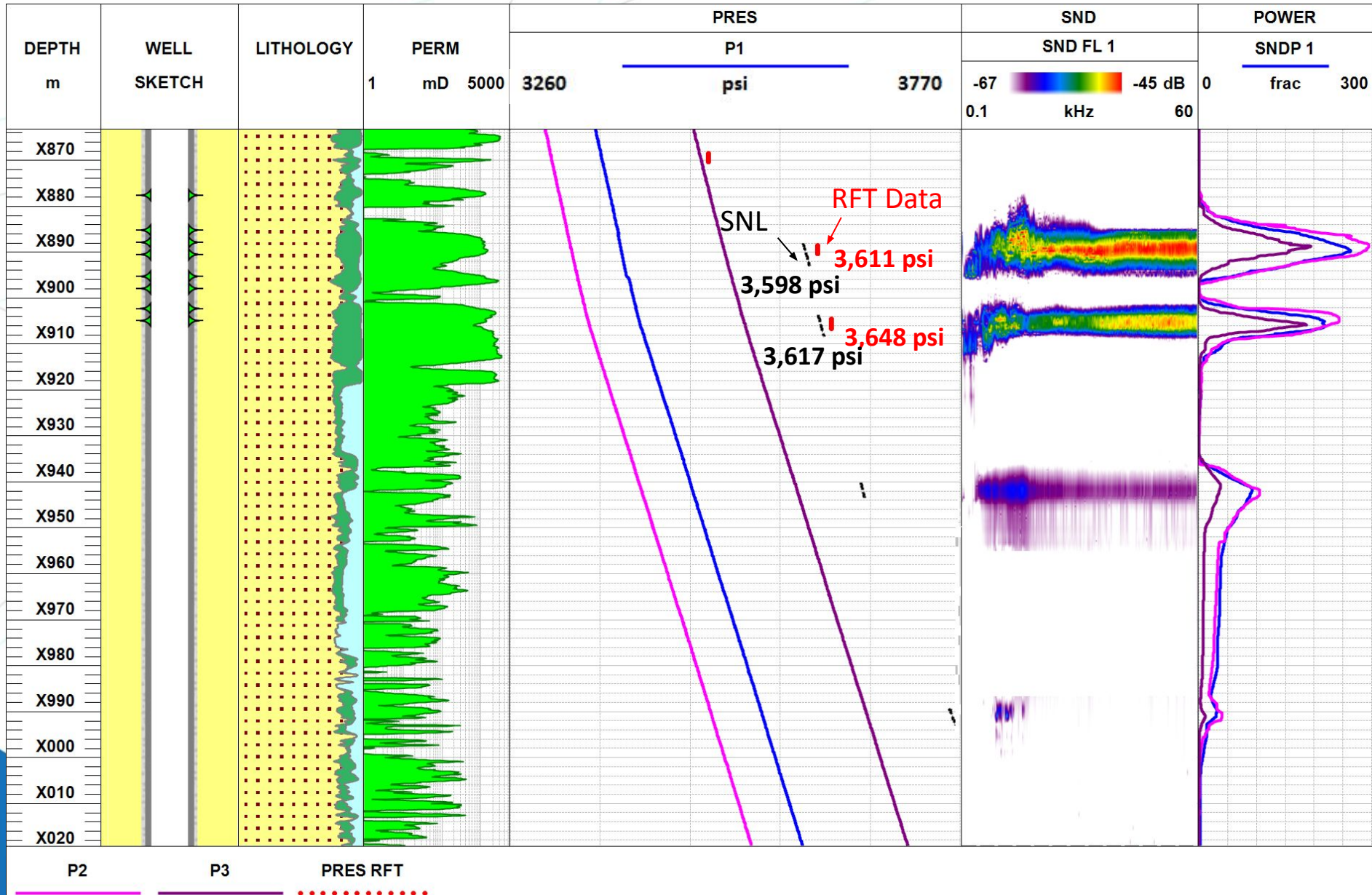
$$N_{pow} = -0.0007*(P_R - P_{wf})^2 + 0.004*(P_R - P_{wf})$$

$$P_R = 3761 \text{ psi}$$





# SNL Multi-rate & RFT



# Conclusion



1. Multi-rate SNL is more accurate than Dual-rate SNL;
2. Shut-in survey is not mandatory;
3. Multi-rate SNL is applicable for multi-phase fluid;

**Thank you!**