## LECTURE 4

IRob2305: Introduction to Robotics

## AGENDA

- Homogenous Transformation Matrix
- Link Connections
- Denavit-Hartneberg Parameters
- DH-Parameters


## WHAT DOWE KNOW FOR NOW?

- We can make a complete rotation matrix all the way from base to the end-effector frame by multiplying together each of the individual rotation matrices from one frame to the next frame:

$$
R_{2}^{0}=R_{1}^{0} R_{2}^{1}
$$

## CANWE DO ITWITH DISPLACEMENT VECTORS?

- $d_{3} \neq d_{1}^{0} d_{2}^{1} d_{3}^{2}$
- What if we want to know things like the position of our end effector in the base frame?
- How could we find d03?


## HOMOGENOUSTRANSFORMATION MATRIX

- $H_{n}^{m}=$ rotation + position of one frame $(\mathrm{n})$ relative to another frame ( m )


$$
\begin{gathered}
R_{2}^{1}=\left[\begin{array}{ccc}
\cos \theta_{2} & -\sin \theta_{2} & 0 \\
\sin \theta_{2} & \cos \theta_{2} & 0 \\
0 & 0 & 1
\end{array}\right] \quad d_{2}^{1}=\left[\begin{array}{c}
a_{4} \cos \theta_{2} \\
a_{4} \sin \theta_{2} \\
a_{3}
\end{array}\right] \\
\left.H_{2}^{1}=\left[\begin{array}{ccc}
\cos _{2} & -\sin \theta_{2} & 0 \\
\sin \theta_{2} & \cos \theta_{2} & 0 \\
0 & 0 & 1 \\
0 & 0 & 0
\end{array}\right] \begin{array}{cc}
a_{4} \cos \theta_{2} \\
a_{4} \cos \theta_{2} \\
a_{3} \\
\hline 0
\end{array}\right]
\end{gathered}
$$

$$
H_{2}^{0}=H_{1}^{0} H_{2}^{\prime}
$$

## DENAVIT-HARTENBERG METHOD

- Industry standard
- Faster
- Obscures the meaning behind the rotation matrix and displacement vector


## STEP I:ASSIGN FRAMES ACCORDING TO THE 4 DH RULES

## STEP 2: FILL OUT THE DH PARAMETER TABLE

## NOTES:

- Assigning coordinate systems:Assign $\mathrm{Z}_{\mathrm{i}}$ along the axis of joint i .
- For a revolute joint, the joint axis is along the axis of rotation.
- For a prismatic joint, the joint axis is along the axis of translation.
- Choose $X_{i}$ to point along the common perpendicular of $Z_{i}$ and $Z_{i+1}$ pointing towards the next joint.
- if $Z_{i}$ and $Z_{i+1}$ intersect, then choose $X_{i}$ to be normal to the plane of intersection.
- Choose $Y_{i}$ to round out a right hand coordinate system.
- The Y -axis is not used for Denavit Hartenberg so it is usually not drawn in the interest of less clutter.



## SYMBOL TERMINOLOGIES :

$\theta$ : A rotation about the $z$-axis.
$d$ : The distance on the $z$-axis.
$\boldsymbol{r}$ : The length of each common normal (Joint offset).
a : The angle between two successive $z$-axes (Joint twist)
$\square$ Only $\theta$ and $d$ are joint variables.

## The necessary motions to transform from one reference frame to the next.

(I) Rotate about the $z_{n}$-axis an able of $\theta_{n+1}$.
(II) Translate along $z_{n}$-axis a distance of $d_{n+1}$ to make $x_{n}$ and $x_{n+1}$ colinear.
(III) Translate along the $x_{n}$-axis a distance of $a_{n+1}$ to bring the origins of $x_{n+1}$ together.
(IV) Rotate $z_{n}$-axis about $x_{n+1}$ axis an angle of $\alpha_{n+1}$ to align $z_{n}$-axis with $z_{n+1}$-axis.

Example


Example: Consider the SCARA robot arm and derive a geometric model of the robot using Denavit-Hartenberg convention


## The DH-table

| Link | $a_{i}$ | $\boldsymbol{\alpha}_{\boldsymbol{i}}$ | $\boldsymbol{d}_{\boldsymbol{i}}$ | $\boldsymbol{\theta}_{\boldsymbol{i}}$ |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 0 | 0 | $\boldsymbol{l}_{1}$ | 0 |
| 2 | $\boldsymbol{l}_{2}$ | 0 | 0 | $\boldsymbol{\theta}_{\mathbf{1}}$ |
| 3 | $\boldsymbol{l}_{3}$ | 0 | 0 | $\boldsymbol{\theta}_{\mathbf{2}}$ |
| 4 | 0 | 0 | $\boldsymbol{d}_{\mathbf{3}}$ | 0 |



- The homogeneous transformation matrices are

$$
\begin{array}{ll}
\mathbf{H}_{1}=\left[\begin{array}{llll}
1 & 0 & 0 & 0 \\
0 & 1 & 0 & 0 \\
0 & 0 & 1 & l_{1} \\
0 & 0 & 0 & 1
\end{array}\right] & \mathbf{H}_{2}=\left[\begin{array}{cccc}
c_{1} & -s_{1} & 0 & l_{2} c_{1} \\
s_{1} & c_{1} & 0 & l_{2} s_{1} \\
0 & 0 & 1 & 0 \\
0 & 0 & 0 & 1
\end{array}\right] \\
\mathbf{H}_{3}=\left[\begin{array}{cccc}
c_{2} & -s_{2} & 0 & l_{3} c_{2} \\
s_{2} & c_{2} & 0 & l_{3} s_{2} \\
0 & 0 & 1 & 0 \\
0 & 0 & 0 & 1
\end{array}\right] & \mathbf{H}_{4}=\left[\begin{array}{cccc}
1 & 0 & 0 & 0 \\
0 & 1 & 0 & 0 \\
0 & 0 & 1 & d_{3} \\
0 & 0 & 0 & 1
\end{array}\right]
\end{array}
$$

where,

$$
\begin{array}{ll}
c_{1}=\cos \theta_{1}, & s_{1}=\sin \theta_{1} \\
c_{2}=\cos \theta_{2}, & s_{2}=\sin \theta_{2}
\end{array}
$$

## - Thus,

$$
\begin{aligned}
{ }^{0} \mathbf{H}_{4} & =\mathbf{H}_{1} \cdot \mathbf{H}_{2} \cdot \mathbf{H}_{3} \cdot \mathbf{H}_{4} \\
& =\left[\begin{array}{ccccc}
1 & 0 & 0 & 0 \\
0 & 1 & 0 & 0 \\
0 & 0 & 1 & l_{1} \\
c_{1} & -s_{1} & 0 & l_{2} c_{1} \\
s_{1} & c_{1} & 0 & l_{2} s_{1} s_{1} \\
0 & 0 & 0 & 1 & 1
\end{array}\right]\left[\begin{array}{cccc}
c_{2} & -s_{2} & 0 & l_{3} c_{2} \\
s_{2} & c_{2} & 0 & l_{3} s_{2} s_{2} \\
0 & 0 & 0 & 1 \\
0 \\
0 & 0 & 0 & 1
\end{array}\right]\left[\begin{array}{cccc}
1 & 0 & 0 & 0 \\
0 & 1 & 0 & 0 \\
0 & 0 & 1 & d_{3} \\
0 & 0 & 0 & 1
\end{array}\right] \\
& =\left[\begin{array}{cccc}
c_{12} & -s_{12} & 0 & l_{3} c_{12}+l_{2} c_{1} \\
s_{12} & c_{12} & 0 & l_{3} s_{12}+l_{2} s_{1} \\
0 & 0 & 1 & l_{1}+d_{3} \\
0 & 0 & 0 & 1
\end{array}\right]
\end{aligned}
$$

where,

$$
c_{12}=\cos \left(\theta_{1}+\theta_{2}\right), \quad s_{12}=\sin \left(\theta_{1}+\theta_{2}\right)
$$

$$
\left[\begin{array}{cccc}
c_{\theta_{i}} & -s_{\theta_{i}} c_{\alpha_{i}} & s_{\theta_{i}} s_{\alpha_{i}} & a_{i} c_{\theta_{i}} \\
s_{\theta_{i}} & c_{\theta_{i}} c_{\alpha_{i}} & -c_{\theta_{\theta} s_{\alpha_{i}}} & a_{i} s_{\theta_{i}} \\
0 & s_{\alpha_{i}} & c_{\alpha_{i}} & d_{i} \\
0 & 0 & 0 & 1
\end{array}\right]
$$

