



Line Differential Protection 7SD52x / 7SD610

Presentation

Line differential relays 87L- SIPROTEC 4

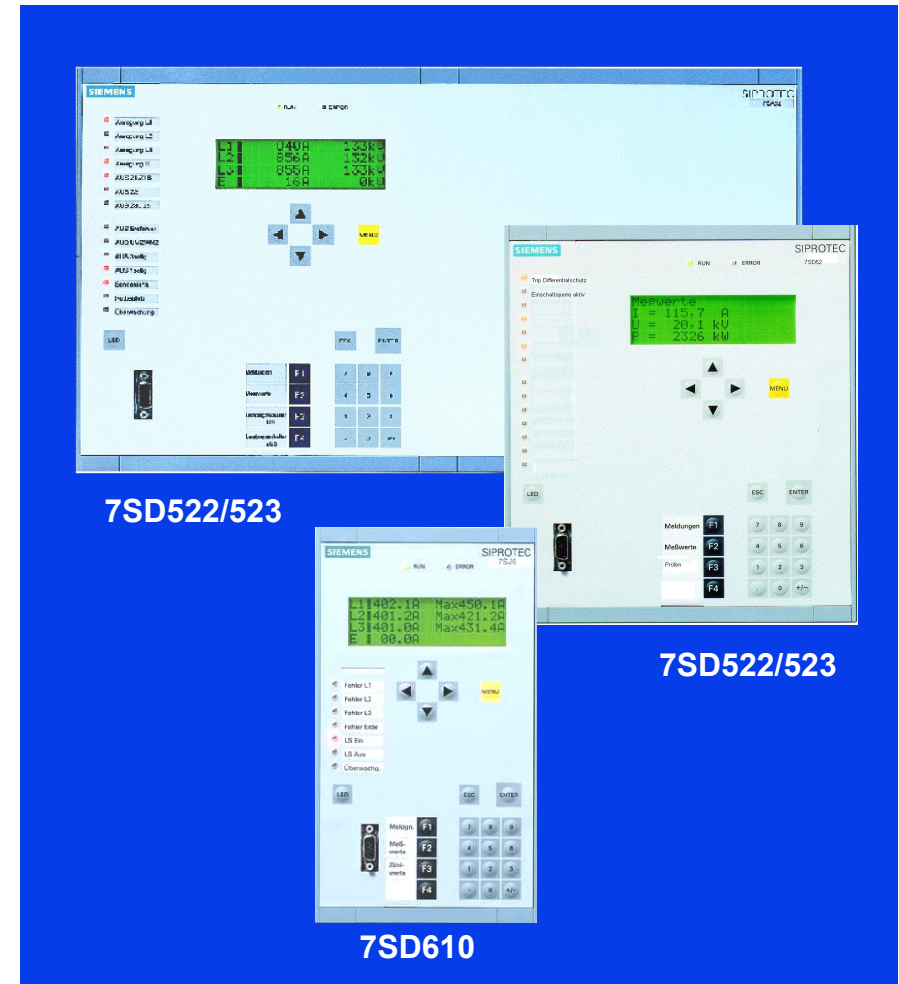


Universal Line Differential Relays 87L

- 7SD610
(2 ends)

- 7SD522
(2 ends , additional I/O)

- 7SD523
(2 up to 6 ends)



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- **The protection adapts its characteristic by itself. Adaptive measurement reduces the setting complexity and ensures maximum sensitivity.**
- **Multi terminal applications up to 6 line ends and redundant Relay to Relay communication.**
- **A transformer inside the feeder zone of protection is fully accommodated by the feeder differential protection and configured with a few simple settings.**
- **Current transformer mismatch 1:8 without matching transformers. Different CT classes possible.**
- **Flexible protection data communication uses a variety of communication media.**
- **Secure operation at unsymmetrical propagation times in Communication networks.**
- **High speed measurement supervision**
- **Simplified commissioning by application of WEB- technology**

• Device	• 7SD610 1/3 19''	• 7SD522 1/2 19''	• 7SD522 1/1 19''	• 7SD523 1/2 19''	• 7SD523 1/1 19''
• Current Inputs (I_{ph} / I_E)	• (3 / 1)*	• (3 / 1)*	• (3 / 1)*	• (3 / 1)*	• (3 / 1)*
• Voltage Inputs (U_{ph} / U_E)	• 3 / 1	• 3 / 1	• 3 / 1	• 3 / 1	• 3 / 1
• Binary Inputs	• 7	• 8	• 16 // 24	• 8	• 16 // 24
• Binary Outputs	• 5	• 15	• (23 // 31)**	• 15	• (23 // 31)**
• Life contact	• 1	• 1	• 1	• 1	• 1
• LC Display	• 4 Lines	• 4 Lines	• 4 Lines	• 4 Lines	• 4 Lines
• Protection Interfaces	• 1	• 1	• 1	• 2	• 2

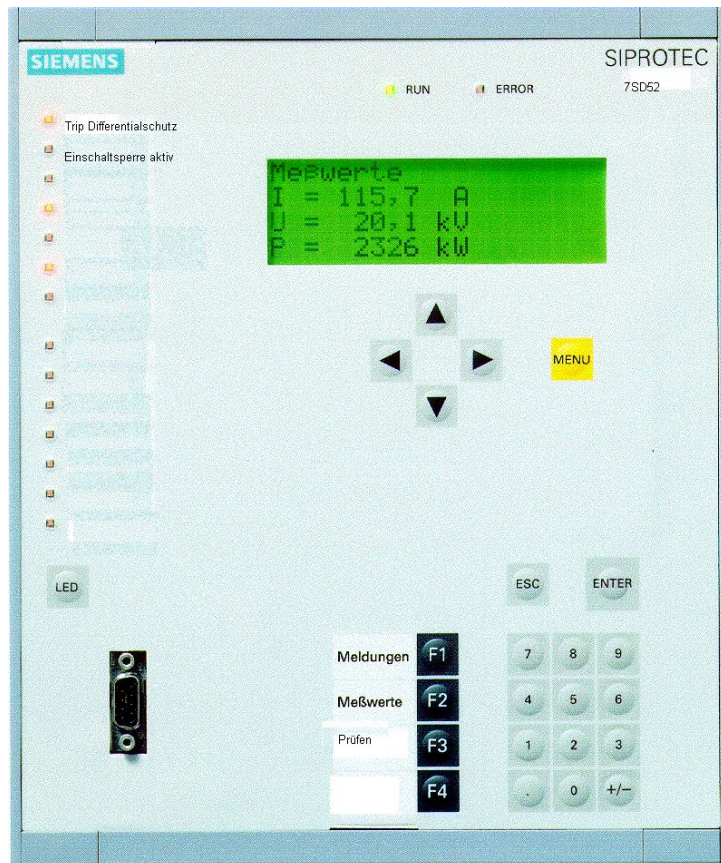
* 1A, 5A changeable (jumper position)

// depending on ordering data

** 5 high-speed relays

Protection and communication join together

Three benefits of 87L-SIPROTEC



Differential protection for the universal use with easy to handle settings

Two up to six line ends , for serial and parallel compensated lines, handles transformers and compensation coils within the protection zone, **tripping time approx. 12 ms with fast high set element**

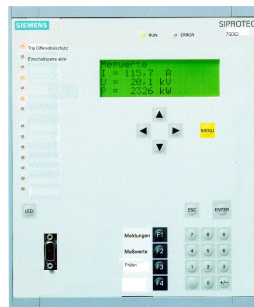
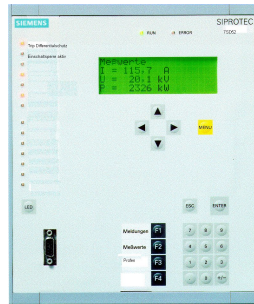
Adaptive differential measurement

Automatic consideration of CT errors and communication-errors

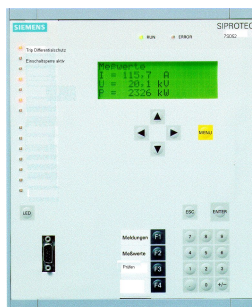
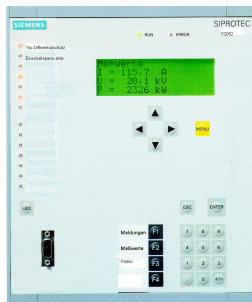
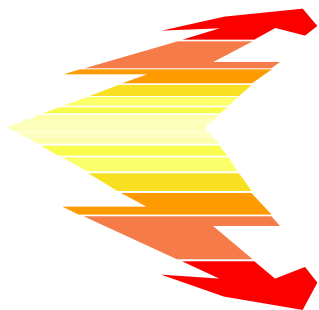
Increased set point during switching-on conditions

Direct and modular connection to fibre optic and digital communication networks

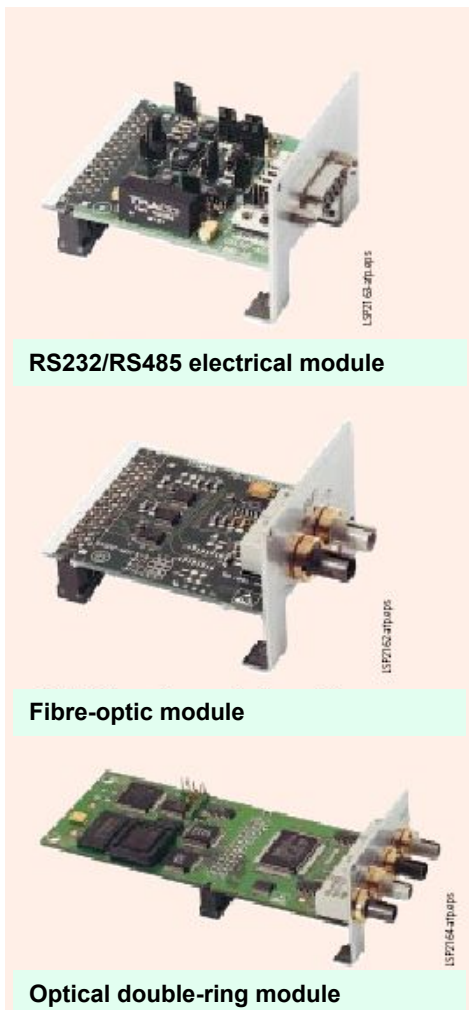
Main protection function 87: Features of the differential function



- Phase selective multi-end differential protection (2 - 6 ends).
- Fundamental vector comparison for the sensitive trip stage (Setting of $I_{Diff} > = 0.2- 0.3 I_N$). Suppress decaying DC-components and harmonics. Therefore allows a sensitive setting.
- Tripping time 12 ms with fast current comparison protection (Setting of $I_{Diff} >> > 1.2 I_{Load.max}$)
- Dynamic increase of differential set point $I_{Diff} >$ during switch-on of long lines / cables
- CT saturation detector (only 5 ms saturation free time due to external faults necessary)
- Phase selective intertrip
- Settable delay time for single phase faults (feature for inductive compensated networks)
- Transformer option: Inrush 2nd harmonic restraint with vector group adaptation. Undelayed trip for high fault currents
- Lockout function (Seal in of trip command)



- **Switch On to Fault protection (SOFT)**
(with breaker position from remote)
- **3 stage backup- or emergency O/C protection (IEC /ANSI) 50, 50N, 51, 51N**
Runs in parallel (backup) or in emergency mode, if 87L is blocked. (from external or due to communication-failure)
- **Three pole and single pole AR** (Single pole AR during 2pole fault without earth possible, Adaptive AR - Switch on from one side)
- **Breaker Failure protection 50BF**
- **Thermal Overload function** (Thermal replica with $I_{Operation}$)
- **User definable logic and control functions also with signals from remote (AND, OR, NOT, Timer, Flip-Flop)**
- **4 remote commands via binary input or logic inputs (destination relay is addressable), 24 remote signals (only 7SD522/523)**
- **Operational values: Currents I, Voltages V, Active/Reactive Power, Delay time, Differential-/Restraint current - Remote end I/V-values**
- **Exactly time synchronized fault records with voltages, currents, binary traces and differential and restraint current per phase**
- **Fast monitoring functions**
Fast broken current-wire supervision blocks 87L and avoids malfunction



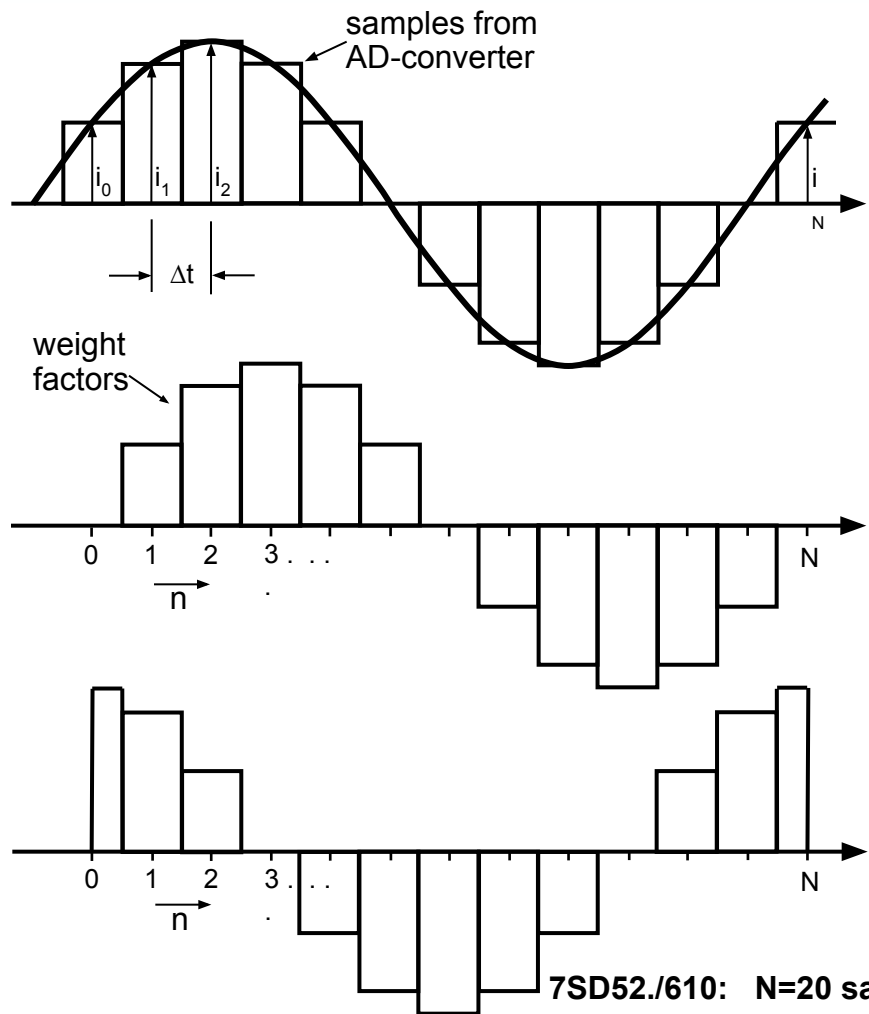
Flexibility due to plug in modules
Compatibility to international standards

- Front interface
 - DIGSI4
 - WEB Monitor
- Service interface (s)
 - DIGSI4 operation
 - modem connection
- System interface
 - IEC60870-5-103
 - Profibus DP
 - DNP3.0
- Time synchronising
 - IRIG-B (GPS)
 - DCF77

Vector comparison offers high sensitivity for high-resistive faults

- DC components and harmonics are suppressed by Advanced Fourier Filters
Suppress decaying DC-component 4 times better than a classical Fourier Filter.
- Different types of Ct's allowed, even with a sensitive setting.
- Relative slow, because of 1 cycle (20 ms, 50Hz) filtering window
Results in a tripping time from 30-50 ms for high resistive faults ($I_{Diff} < 1.2 .. 2 I_N$)

I_{Diff} : Vector comparison with Advanced Fourier filters (Basic principle)



Optimized filtering coefficients for 7SD52 / 7SD610 designed for suppressing decaying DC-components 4 times better than conventional Fourier-filters. Overcome stability problems with decaying DC-components

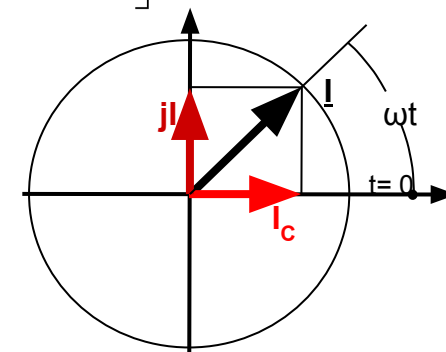
Sine component:

$$I_S = \frac{2}{N} \left[\sum_{n=1}^{N-1} \sin(\omega \cdot n \cdot \Delta t) \cdot i_n \right] \rightarrow 1 \dots N = 20$$

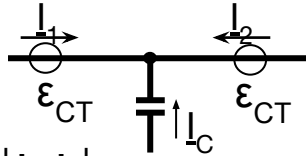
Cosine component:

$$I_C = \frac{2}{N} \left[\frac{i_0}{2} + \frac{i_N}{2} + \sum_{n=1}^{N-1} \cos(\omega \cdot n \cdot \Delta t) \cdot i_n \right] \rightarrow 1 \dots N = 20$$

Complex vector

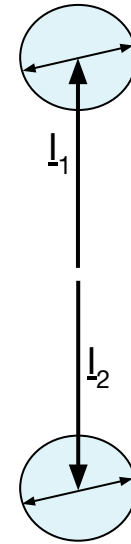
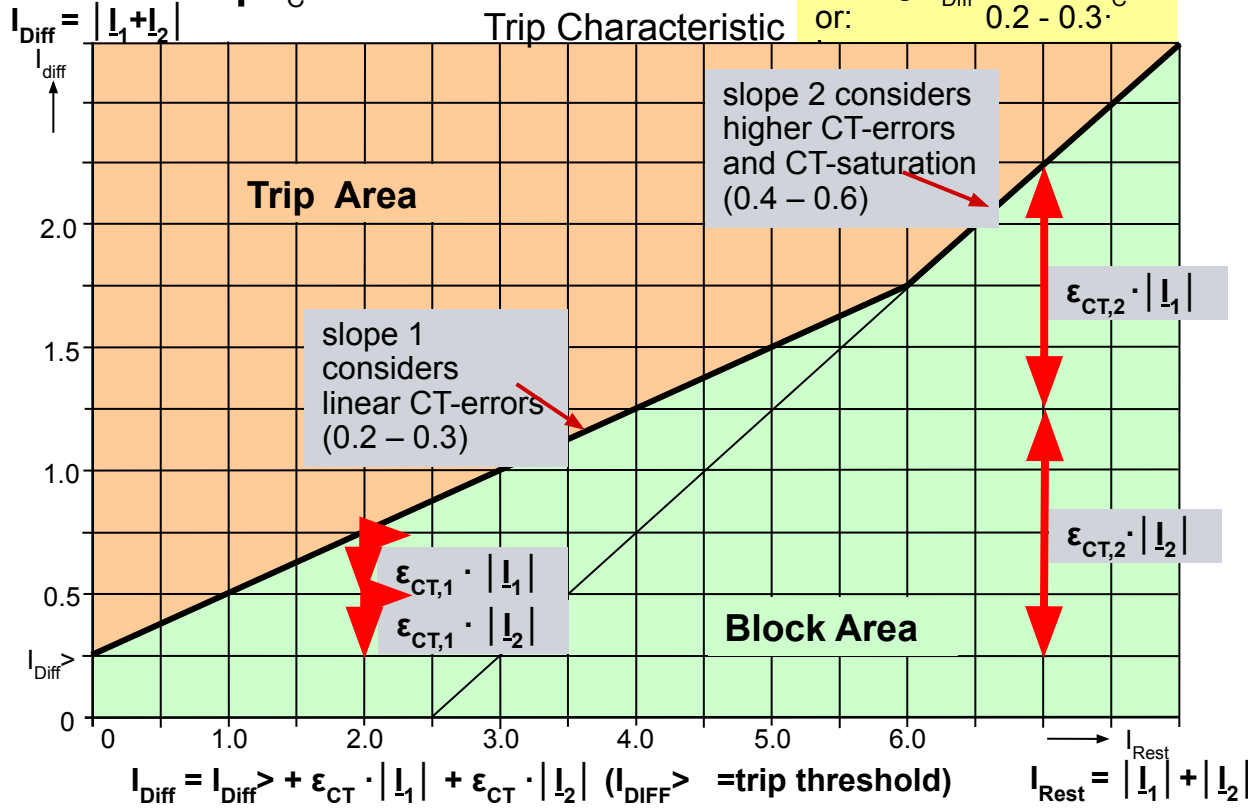
$$\underline{I} = \frac{2}{N} (I_C + j I_S)$$


$I_{Diff} >$: Theory of the classical differential tripping characteristic



Assumption: Equal CT type, currents are exactly synchronized (given through analogue measurement), equal CT-ratio

Setting: $I_{Diff} > = 2 - 3 \cdot I_C$
or: $0.2 - 0.3 \cdot I_C$



maximum measurement error (ϵ) due to CT - error

Example: CT class **10P10**, $S_n = 10VA$, $I_{sn} = 1A$

10% tolerance at K_{SSC} (**= 10 = k_{ALF_N}**) (in case of nominal burden is connected)

$$k_{ALF} = k_{ALF_N} \cdot \frac{P_{ct} + P_b}{P_{ct} + P'_b} = k_{ALF_N} \cdot \frac{R_{ct} + R_b}{R_{ct} + R'_b}$$

with: K_{SSC} : rated symmetrical short-circuit current factor (IEC 60044-6)

K_{ALF_N} : rated Accuracy Limit Factor

K_{ALF} : actual Accuracy Limit Factor

R_{ct} : secondary winding resistance

R_b : rated resistive burden

R'_b : actual resistive burden ($R_{LEADS} +$

Thumb rule:

$$R_{ct} \approx 0.1 \dots 0.2 \cdot R_{Relay}$$

R_b

Nominal burden :

$$R_b = \frac{S_n}{I_{sn}^2} = \frac{10VA}{1^2 A^2} = 10\Omega \rightarrow R_{ct} \approx 2\Omega$$

$$\frac{k_{ALF}}{k_{ALF_N}} = \frac{2\Omega + 10\Omega}{2\Omega + 1\Omega} = 4$$

- If less then rated burden is connected to the CT, the CT- error for load conditions (ϵ_{Load}) can be used for calculations with currents higher than the nominal current of the CT (I_{pn}) !
(In the example here: ϵ_{Load} could be taken for currents up to $4 \cdot I_{pn}$)

As the $I_{Diff} >$ step must be (very) sensitive for high resistive faults at maximum Load, for usual applications there is no need to set the parameter 0251 (k_{ALF}/K_{ALF_N}) higher than 1.5 !!

Resulting Relay Parameter (with exact calculation)

- $k_{ALF} / k_{ALF_N} = 1.5$ (calculation as above = 4 , $4 > 1.5$ □ Setting: 1.5)
[remains 1 if CT-data's are unknown]

- IEC 60044 -1:

tolerance in load area up to k_{ALF} / k_{ALF_N} : <2% for 5P (TPY), <3% for 10P (TPX) Ct's

Recommended setting in the relay: 3% for 5P, 5% for 10P

total error at accuracy limit $k_{ALF_N} = 5\%$ for class 5P and 10% for class 10 P

Recommended setting in the relay: 10% for 5P, 15% for 10P

I_{Diff} : Approximation of the CT- error

Basis for the adaptive restraint current calculation (max. expected differential current due to CT-errors) is the estimated error of each CT

from the CT-data's

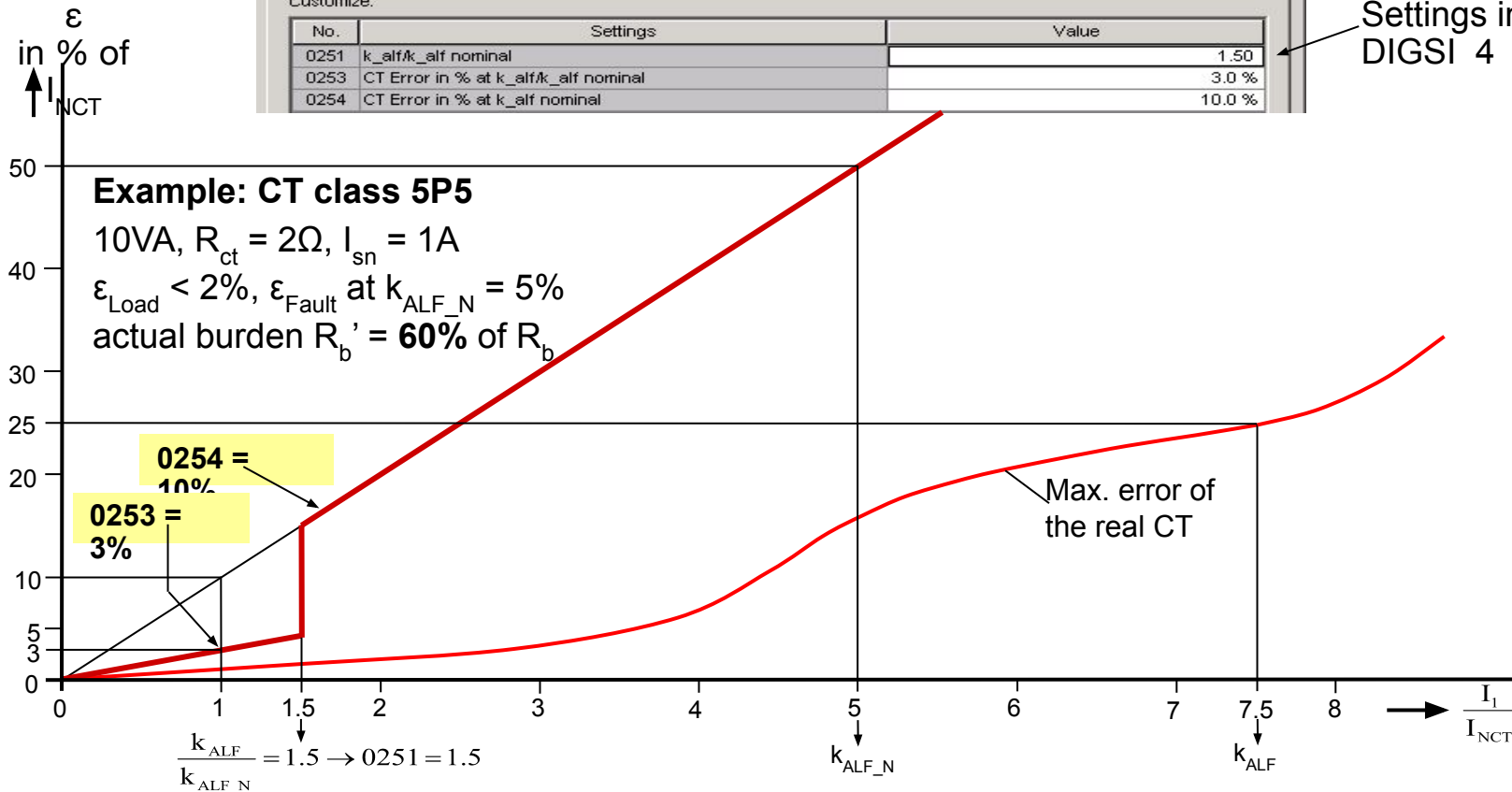
Power System Data 1

Transformers | Power System | Breaker | CT Datas

Customize:

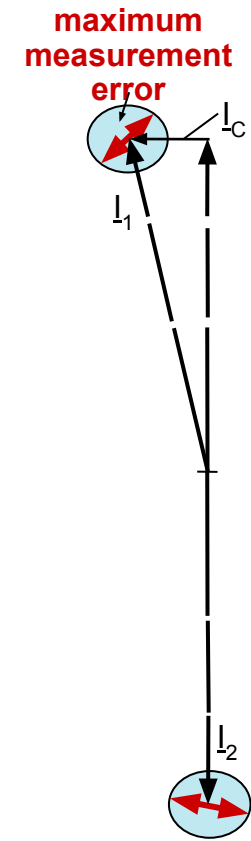
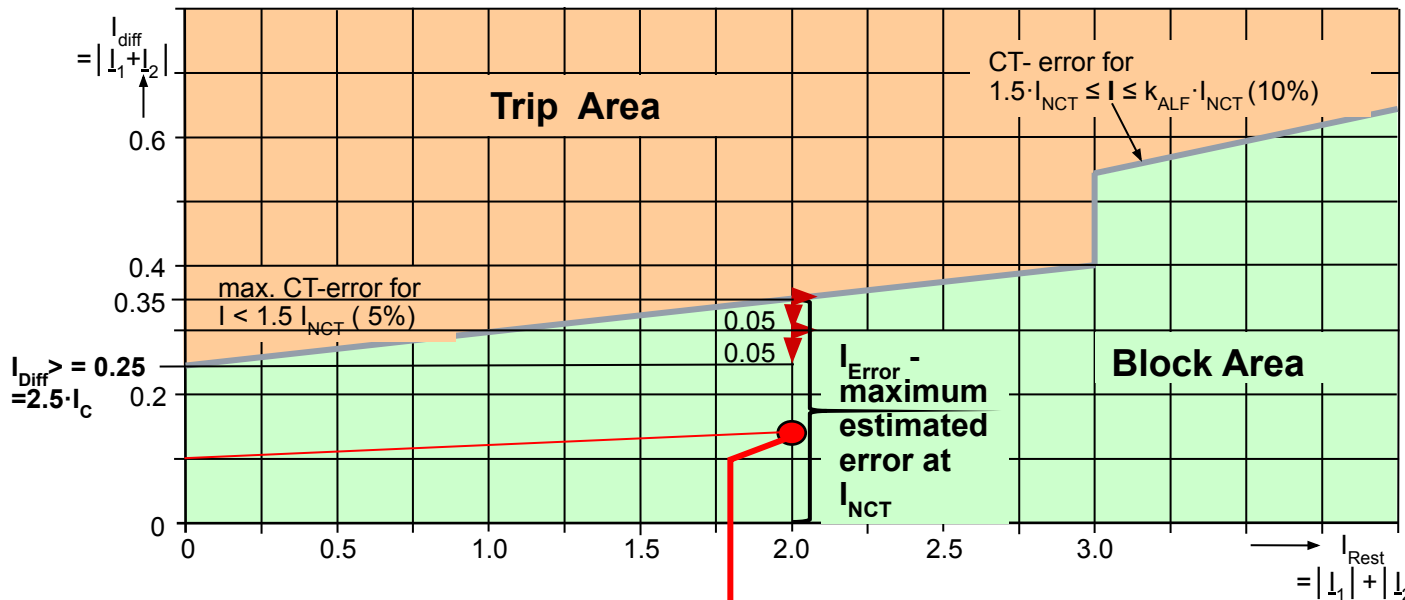
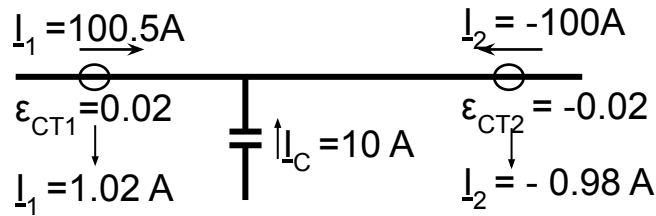
No.	Settings	Value
0251	k_{alf}/k_{alf} nominal	1.50
0253	CT Error in % at k_{alf}/k_{alf} nominal	3.0 %
0254	CT Error in % at k_{alf} nominal	10.0 %

Settings in DIGSI 4



$I_{Diff} >$: Example for a setting at nominal current

Assumption: CT-ratio is 100/1A, real error of Ct's is 2% (0.02) up to $1.5 I_{NCT}$



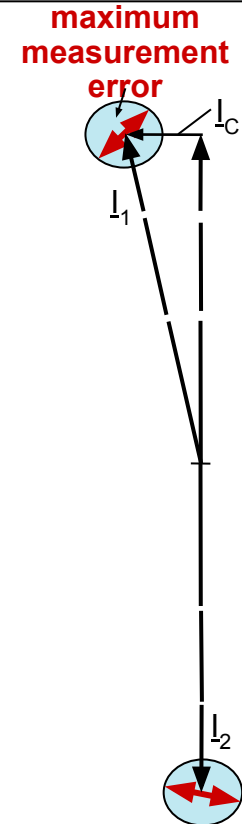
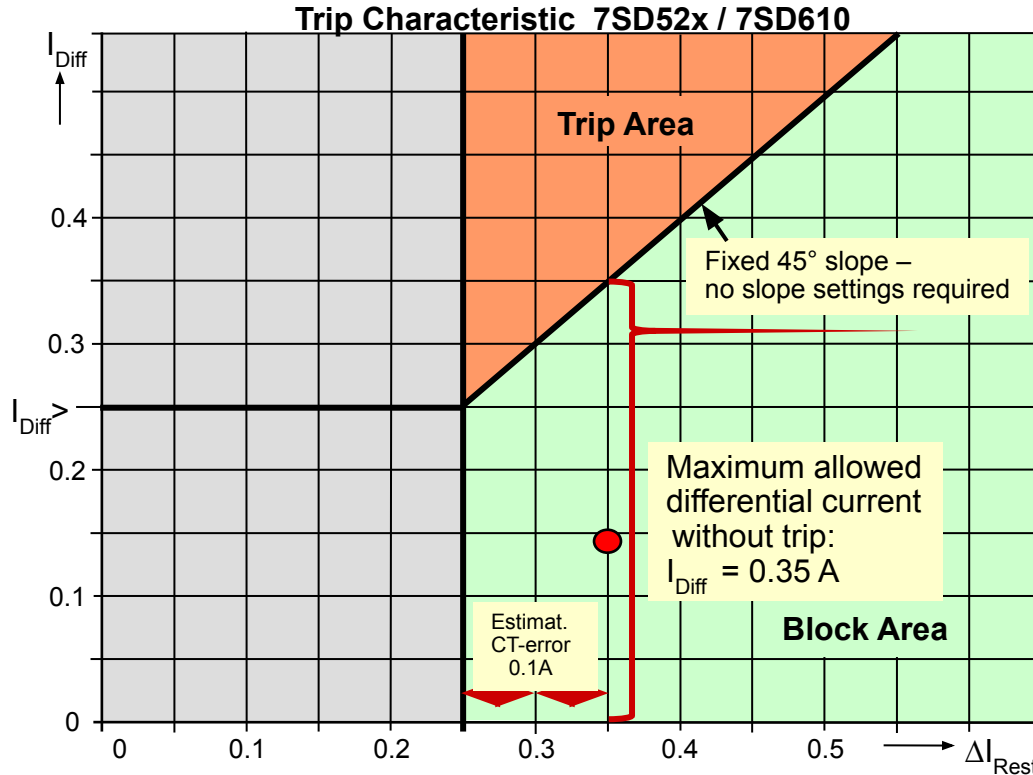
Diff. due to charge + real CT error:
A

$$I_{Diff} = 0.1 \text{ A} + 0.02 \cdot |1\text{A}| + 0.02 \cdot |1\text{A}| = 0.14$$

Max. estimated error = Restraint current : $I_{Error} = 0.25 \text{ A} + 0.05 \cdot (|1\text{A}| + |1\text{A}|) = 0.35 \text{ A}$

$I_{Diff} >$: Adaptive differential relaying Restraint current with consideration of the CT- errors

Same example as before! Assumption: Currents are exactly synchronized



Current summation:

Max. error

$$I_{Diff} = |I_1 + I_2|$$

$$I_{Error} = \Delta I_{Rest} (*) = I_{Diff} + \epsilon_{CT1} \cdot I_1 + \epsilon_{CT2} \cdot I_2 = I_{Diff} + \text{estimated CT-}$$

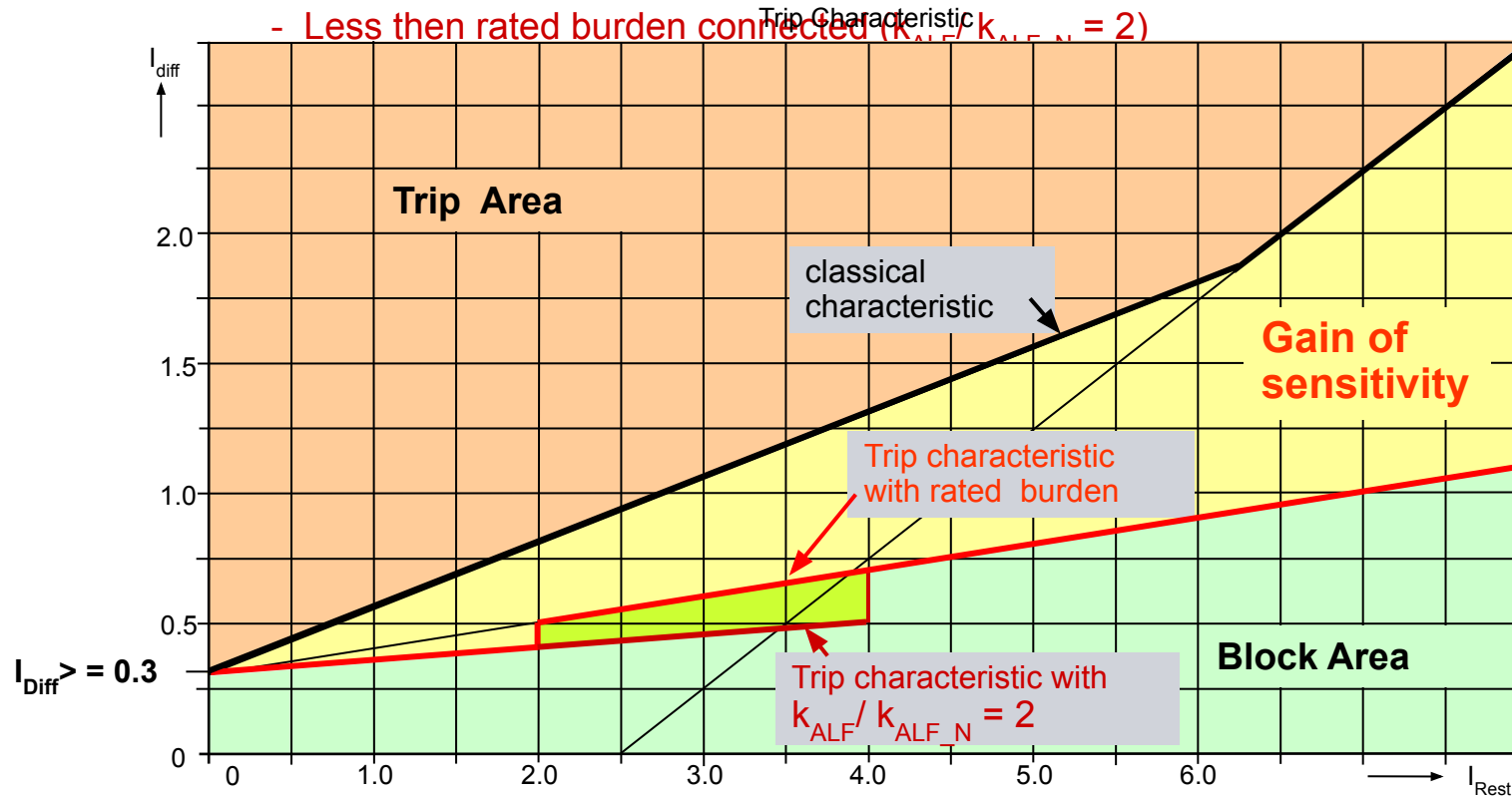
***) ΔI_{Rest} = adaptive restraint current**

Trip, if differential current I_{Diff} exceeds the restraint current (max. error)

$I_{Diff} >$: New differential method compared with a classical differential characteristic

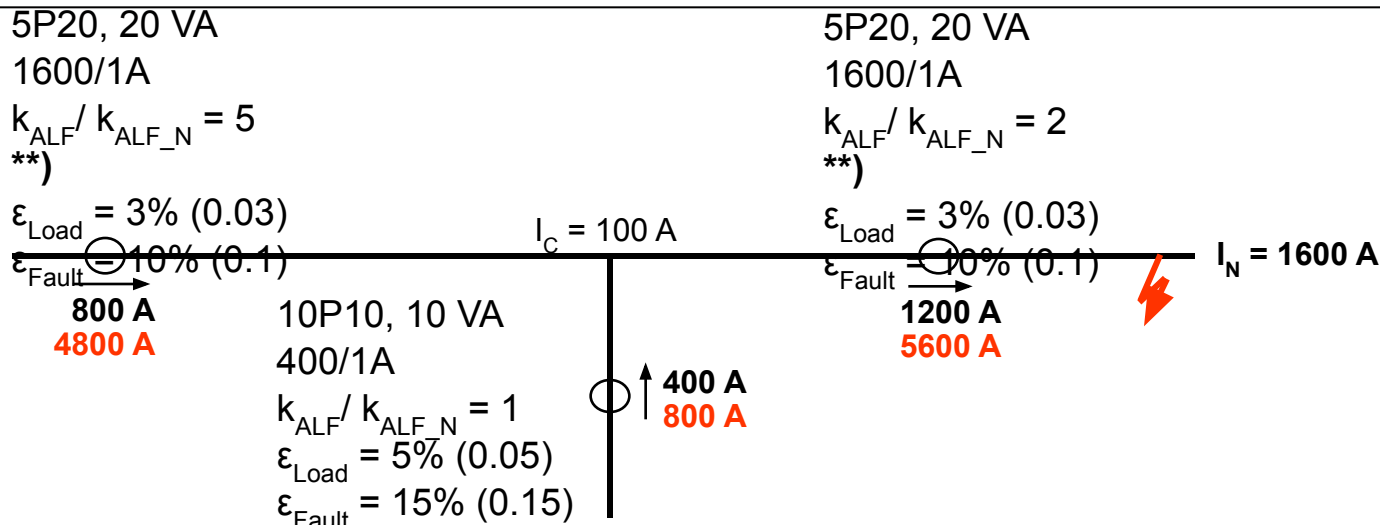
Assumption: Equal Ct's on both side, no effects from comms-system, standard settings

- Rated burden connected at the Ct's
- Less then rated burden connected ($k_{ALF}/k_{ALF_N} = 2$)



Classical: $I_{Diff} = 0.3 + 0.25 \cdot I_{Rest} = 0.3 + 0.25 \cdot 2 = 0.8$ (sensitivity under full load)
 New: $I_{Diff} = 0.3 + 0.05 \cdot I_{Rest} = 0.3 + 0.05 \cdot 2 = 0.4$ (double sensitivity under full load)

$I_{Diff} >$: Example 1: Adaptive (self-) restraining



**) Settings for this example.

In a real case both settings would be 1.5

$I_{Diff} > = \text{Differential-Setting} = 2.5 \cdot I_C = 250 \text{ A}$

$\Delta I_{Rest} = I_{Diff} > + \text{sum of estimated Ct- errors}$

I_{Diff} = Differential current due to vector summation of the individual currents

Case 1 (normal operation)

$\Delta I_{Rest} = 2.5 \cdot 100\text{A} + 0.03 \cdot 800\text{A} + 0.03 \cdot 1200\text{A} + 0.05 \cdot 400\text{A} = 330\text{A}$

$I_{Diff} = 100 \text{ A} (=I_C)$

$\Delta I_{Rest} / I_N = 0.206$

$I_{Diff} / I_N = 0.0625$

Case 2 (External Fault)

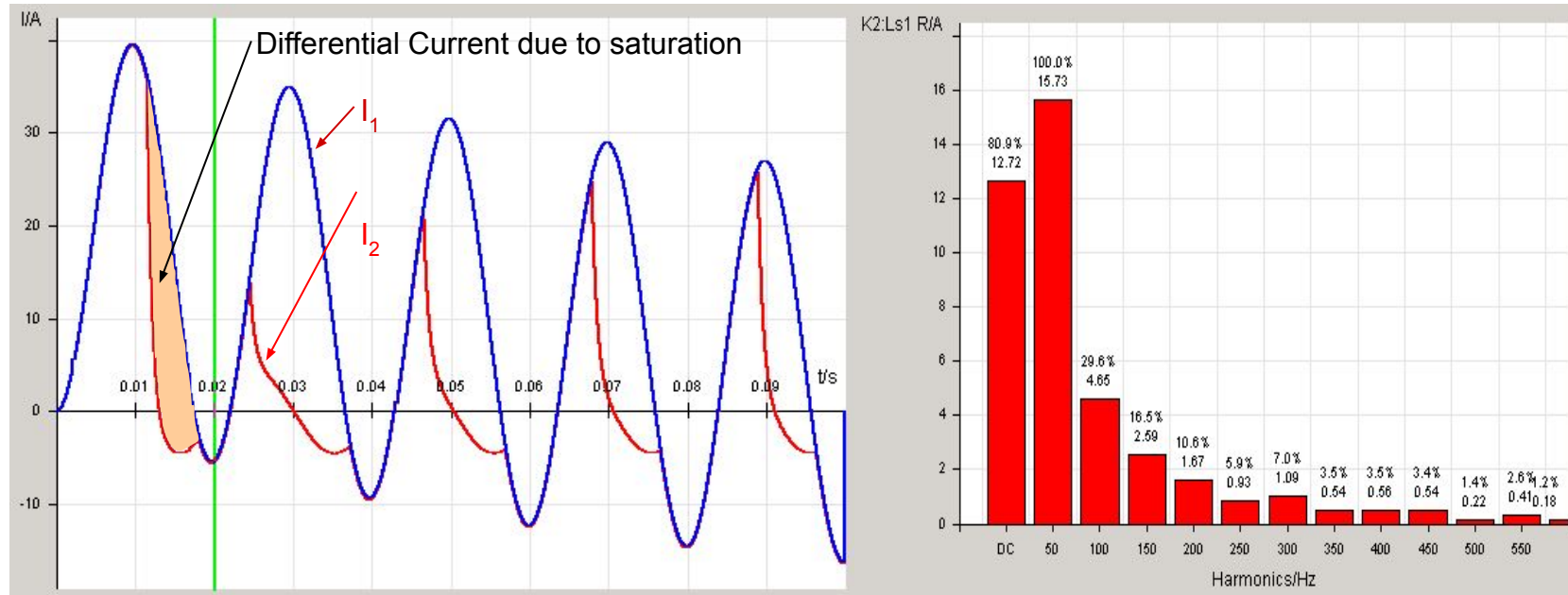
$\Delta I_{Rest} = 2.5 \cdot 100\text{A} + 0.03 \cdot 4800\text{A} + 0.1 \cdot 5600\text{A} + 0.15 \cdot 800\text{A} = 1074\text{A}$

$I_{Diff} = 40 \text{ A (due to lower voltage)}$

$\Delta I_{Rest} / I_N = 0.671$

$I_{Diff} / I_N = 0.025$

I_{Diff} : CT- saturation detector based on harmonic analysis of the current wave form - Signal analysis



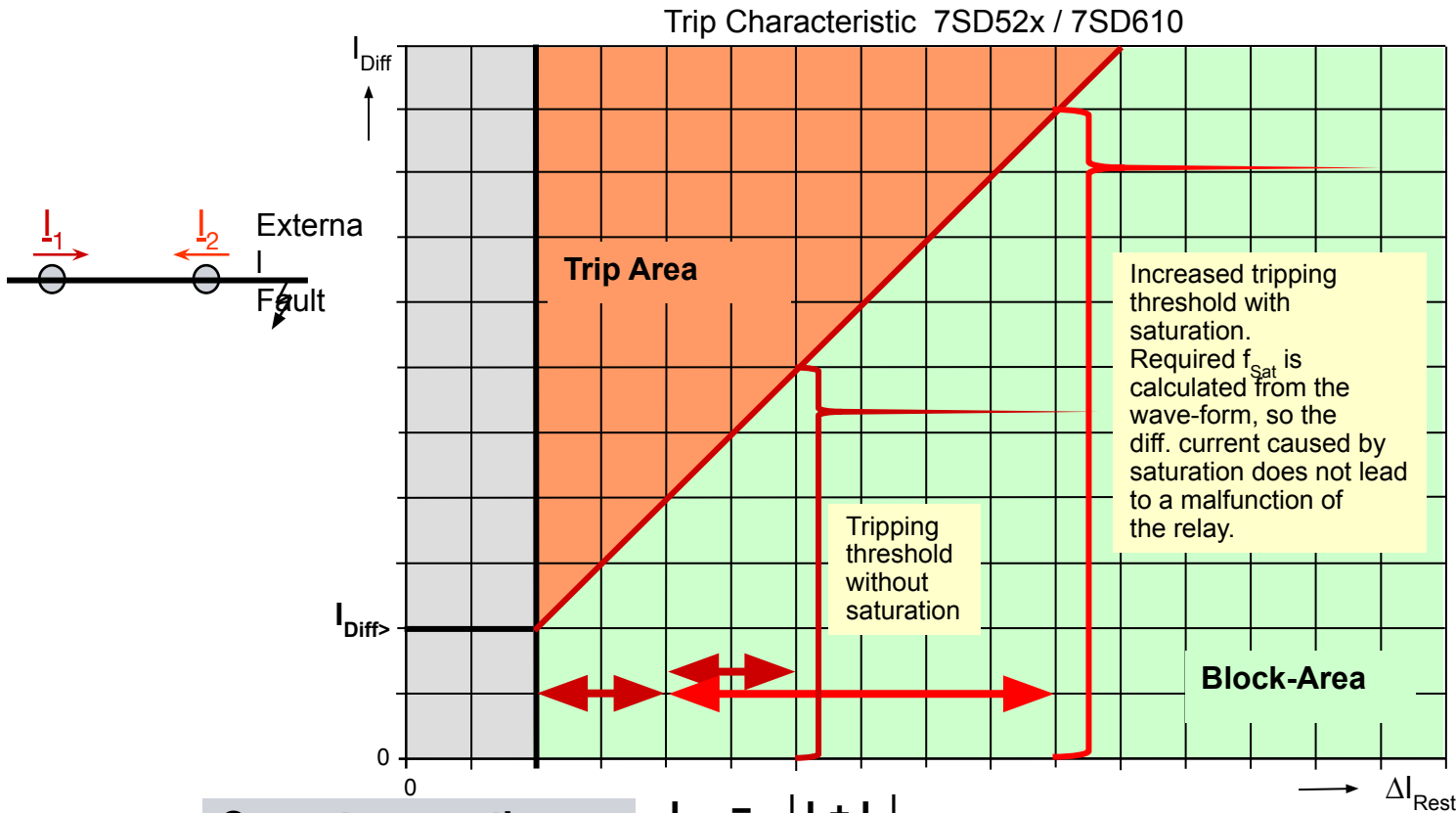
- Wave form detector recognize saturation from DC, f_2 , f_3 , f_4 , f_5 rated to the fundamental f_1
 Factor = 1 - no saturation

Factor > 1 - saturation Increase of CT- error with a factor f_{Sat} .
 Results in higher restraint current.

More differential current is required for tripping.

$I_{Diff} >$: Adaptive differential relaying

Consideration of nonlinear CT- errors due to saturation

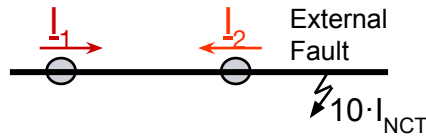


Current summation: $I_{Diff} = |I_1 + I_2|$

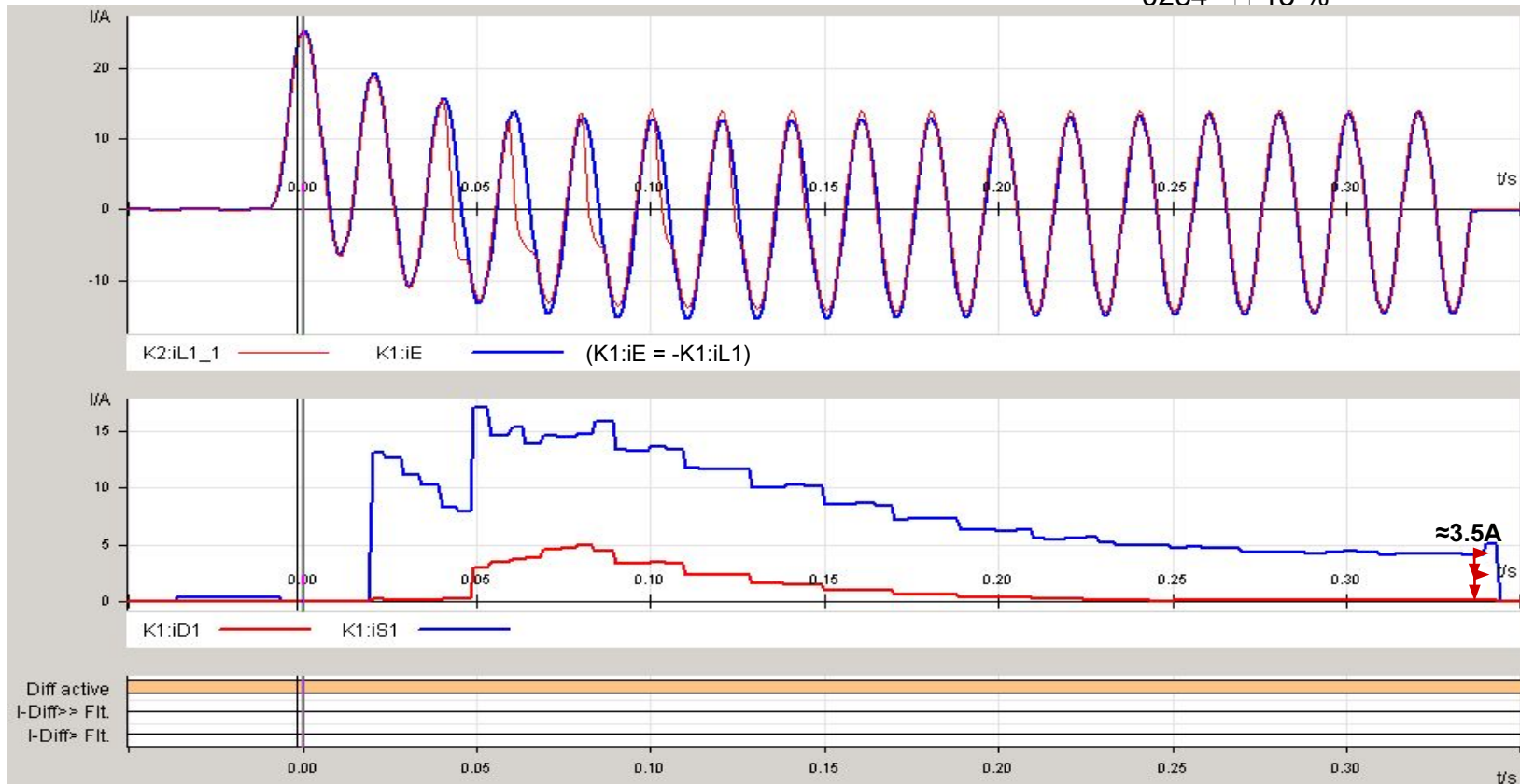
Max. error summation: $I_{Error} = \Delta I_{Rest} = I_{Diff} + \epsilon_{CT1} \cdot I_1 + f_{Sat} \cdot \epsilon_{CT2}$

Trip, if differential current exceeds the estimated error (= increased restraint)

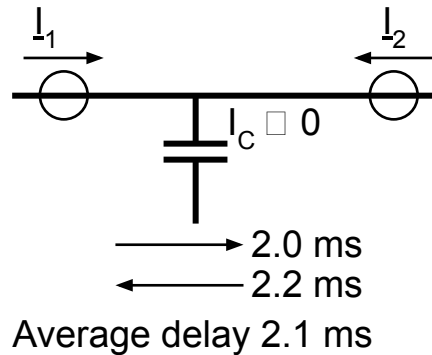
$I_{Diff} >$: Test: max. asymmetrical offset, Ct saturation



Settings: 1210/13 0.30
 A
 0251 1.0
 0253 5 %
 0254 15 %



I_{Diff} >: Adaptive consideration of a permanent time difference in transmit- and receive direction



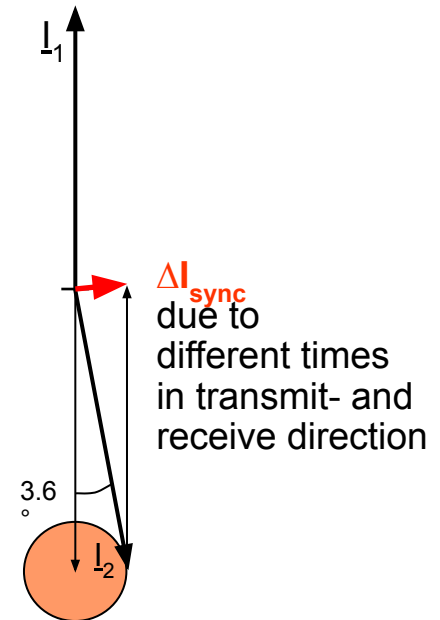
$$\Delta\Phi_{sync} \approx \frac{\Delta t \cdot 360^\circ}{20ms} \rightarrow (50Hz)$$

$$\text{here : } \Delta\Phi_{sync} \approx \frac{0.2ms \cdot 360^\circ}{20ms} = 3.6^\circ$$

$$= \frac{3.6^\circ \cdot 2\pi}{360^\circ} = 0.06283$$

$$\Delta I_{sync} \approx \Delta\Phi_{sync} \cdot |I_{sync}| \approx \Delta\Phi_{sync} \cdot |I_2|$$

(For more details:
refer to 7SD52 Synchronisation)



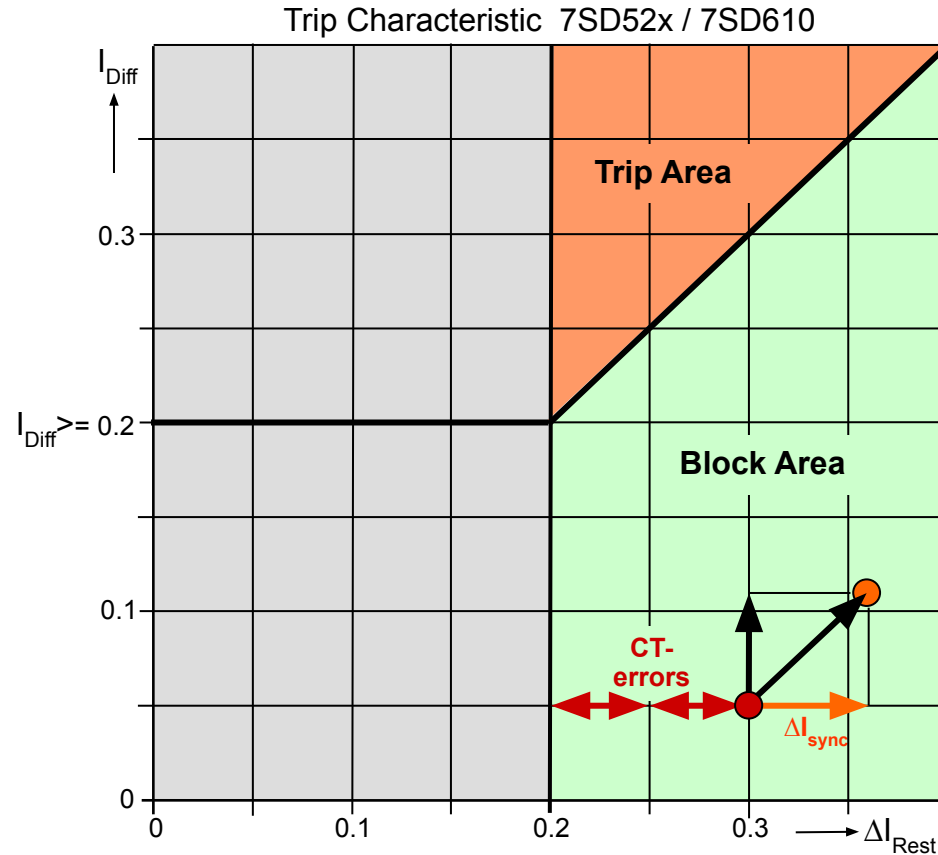
Protection Interface (Port D+E) - Settings Group A

General Interface 1 GPS

Customize:

No.	Settings	Value
1501	State of protection interface 1	ON
1502	Connection 1 over	Communication converter with 64 kBit/s
1505A	Prot 1: Maximal permissible delay time	30.0 ms
1506A	Prot 1: Diff. in send and receive time	0.200 ms

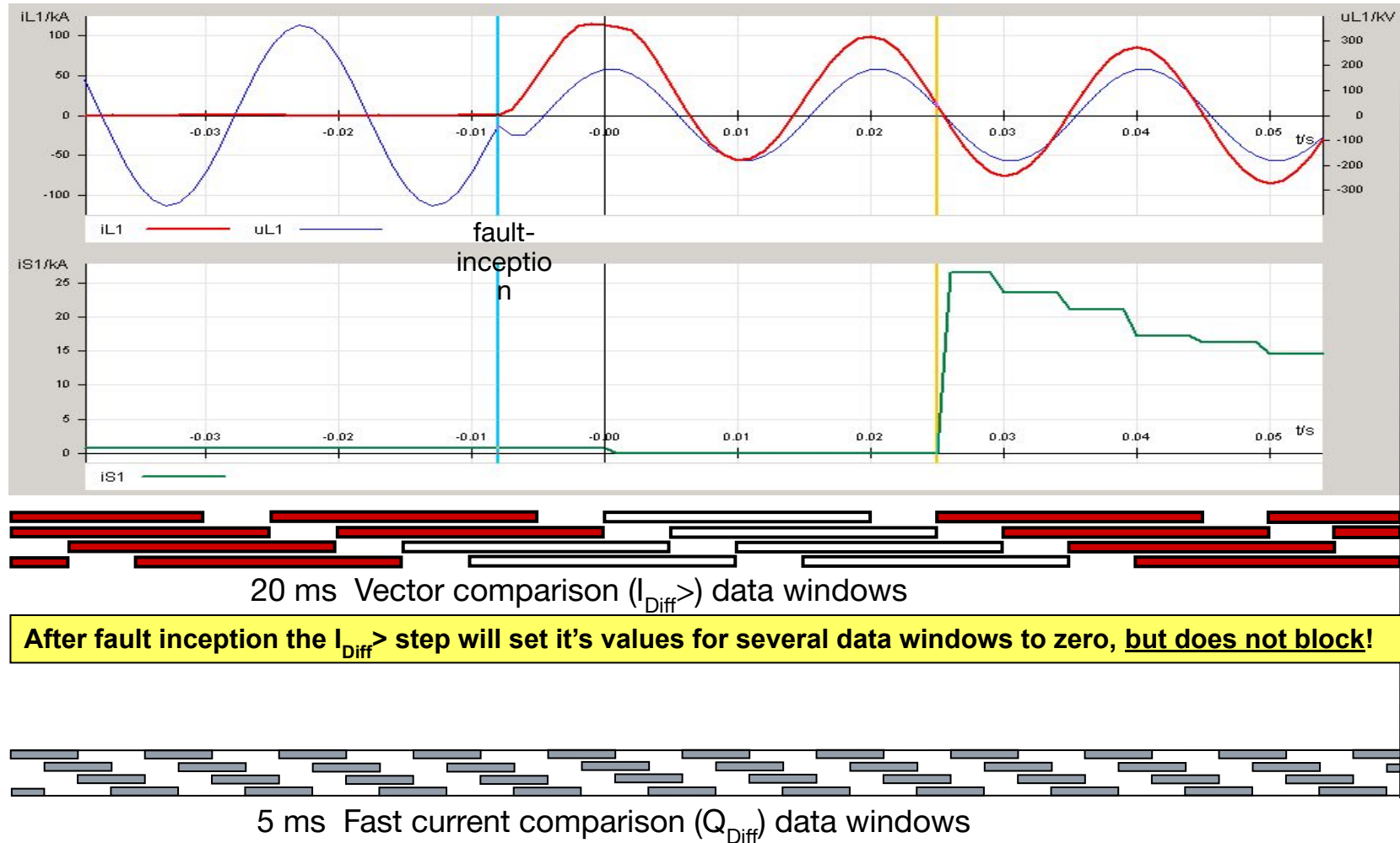
$I_{Diff} >$: Adaptive consideration of a permanent time difference. Total “Restraint Current”



Diff. current: $I_{Diff} = I_C + \Delta I_{sync}$
 Rest. current: $\Delta I_{Rest} = I_{Diff} > + \text{CT-errors} + \Delta I_{sync}$
Total “Restraint Current”:

$$\Delta I_{Rest} = I_{Diff} > + f_{Sat1} \cdot \epsilon_{CT1} \cdot I_1 + f_{Sat2} \cdot \epsilon_{CT2} \cdot I_2 + \Delta I_{sync}$$

$I_{Diff} >$: Sliding data windows after fault inception



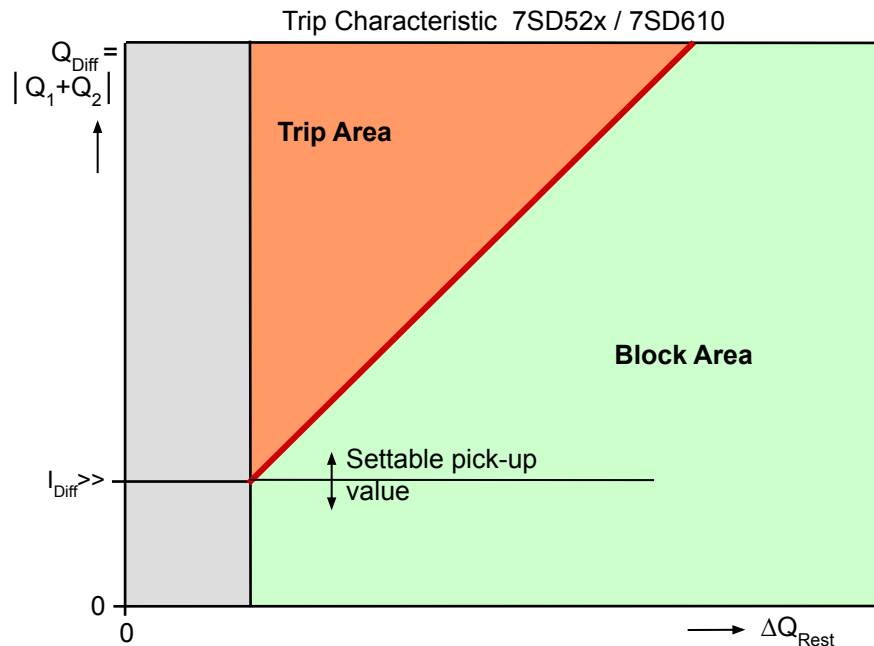
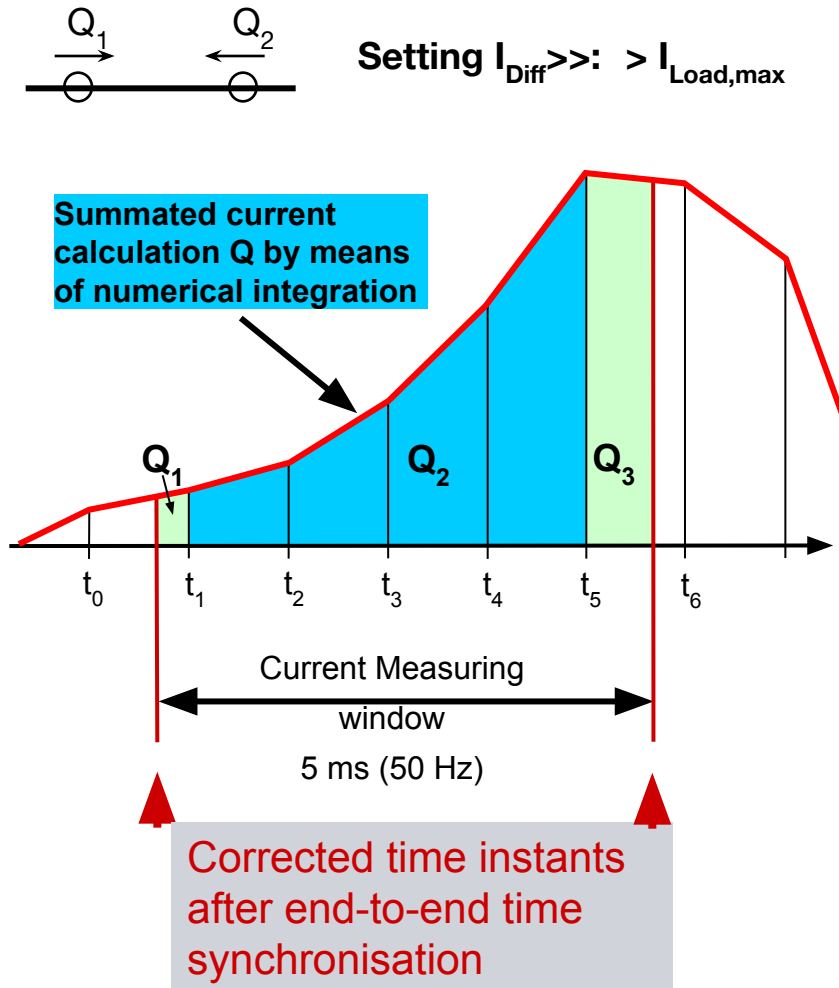
After fault inception the $I_{Diff} >$ step will set it's values for several data windows to zero, but does not block!

$I_{Diff} \gg (Q_{Diff})$: Fast current comparison

Fast Current comparison offers high speed tripping and a fast decision for internal or external fault condition

- Current comparison step doesn't suppress DC-components and harmonics. (simple integration)
Therefore recommended setting is $> I_{Load,max} (1.2 - 2 I_N)$.
- Current comparison decides in 5 ms for internal or external faults (5 ms window)
Internal: Immediate trip command (trip time typical 12 ms for 2 or 3 end topology) for differential currents $I_{Diff} > 1.2 - 2 I_N$
External: If $I_{Fault} > 2.5 \cdot I_{Diff} \gg$ setting: immediate **blocking** of the current comparison.
Reason: CT-saturation possible. Avoids any risk for stability due to differential current from current comparison.

$I_{Diff} \gg (Q_{Diff})$: Fast current comparison algorithm (Basic principle)

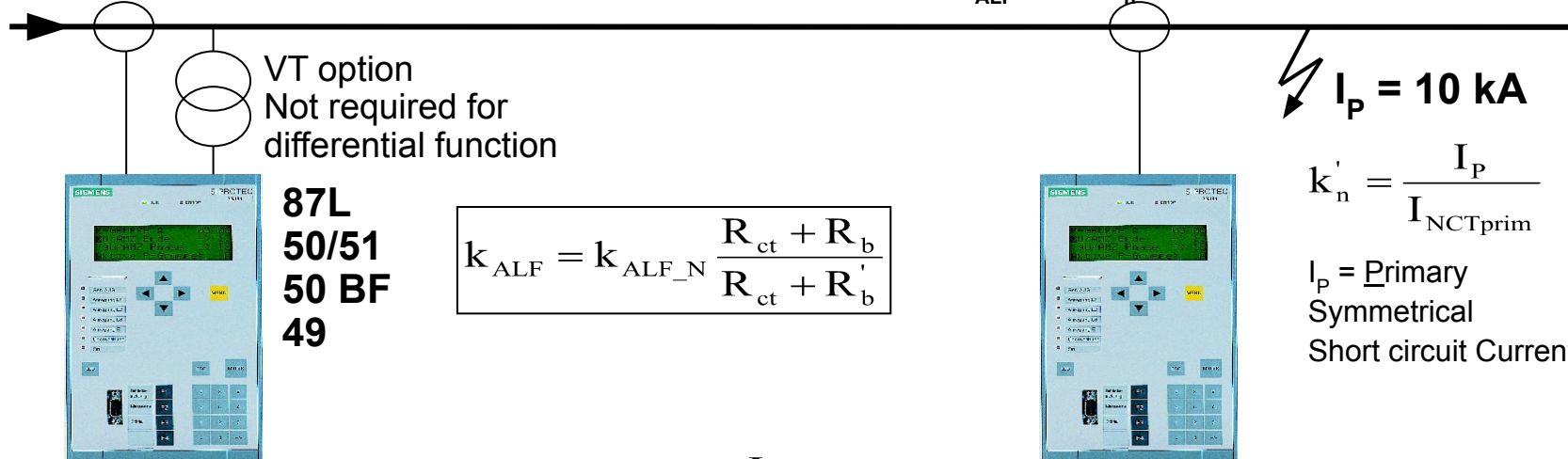


Calculated restraint values from CT-errors (always higher CT-error is taken).
Similar principal as vector comparison for restraint current calculation.

CT- requirements, mismatch of the primary CT currents

1200/1A, 10P10, 10VA
 $R_{ct} = 2.5\Omega, R'_b = 1.1\Omega$
 $(k_{ALF} = 34.7, k'_n = 8.33)$

150/5A, 5P20, 50VA
 $R_{ct} = 0.25\Omega, R'_b = 0.4\Omega$
 $(k_{ALF} = 69, k'_n = 66.6)$



- Mismatch of the primary CT currents:

$$\frac{I_{CTprim(max)}}{I_{CTprim(min)}} \leq 8$$

- 1A or 5A input selectable in the relay
- CT data's / errors are set in the relay and automatically considered in the restraint current calculation
- CT-requirements:
 - 1st condition: $k_{ALF} > k'_n$
 - 2nd condition: $k_{ALF} \geq 30$ **or** $\frac{1}{4}$ AC cycle saturation free time (5ms for 50Hz)

Application - Transformer and line/cable in the protection zone

Power System Data 2 - Settings Group A

Topology Data: Local Line End | Line Status | Trip 1-/3-pole

Customize:

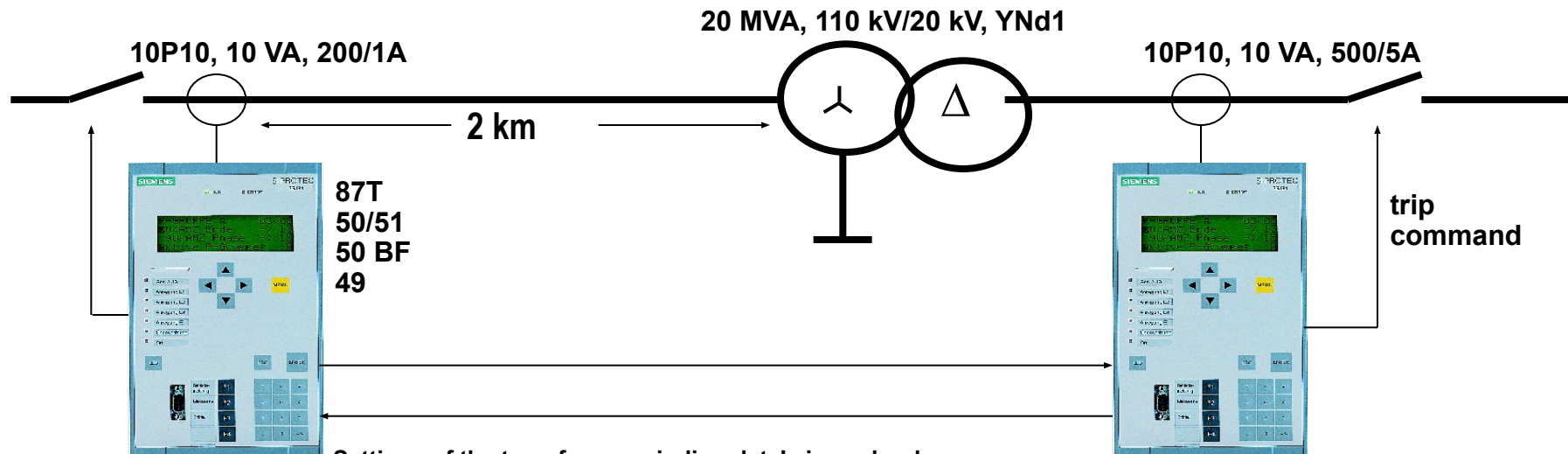
No.	Settings	
1106	Operational power of protection zone	20.0 MVA
1162	Vector group numeral for current	0
1163	Transformer starpoint is	Solid Earthed

Power System Data 2 - Settings Group A

Topology Data: Local Line End | Line Status | Trip 1-/3-pole

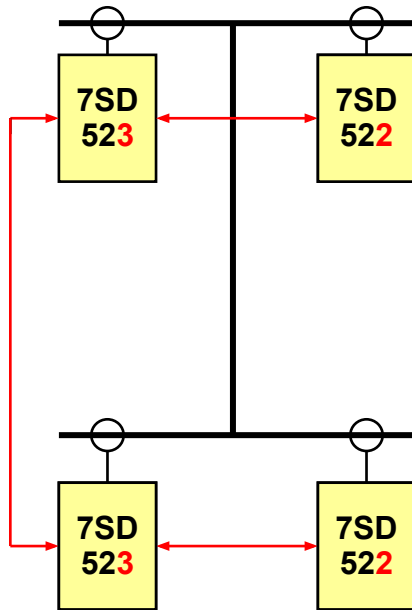
Customize:

No.	Settings	
1106	Operational power of protection zone	20.0 MVA
1162	Vector group numeral for current	1
1163	Transformer starpoint is	Not Earthed

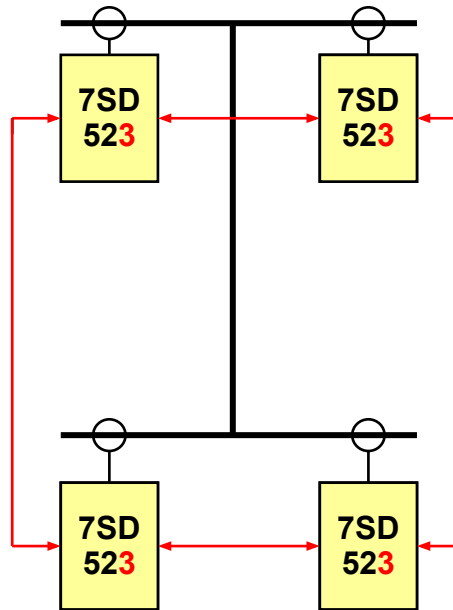


- Settings of the transformer winding data's in each relay with vector group matching, ratio adaptation and zero sequence elimination
- Differential set point is rated to the nominal current of the transformer
- Inrush restraint with second harmonic included (time limit for Cross block)
- High set element for immediate trip (12 ms) through heavy internal fault currents

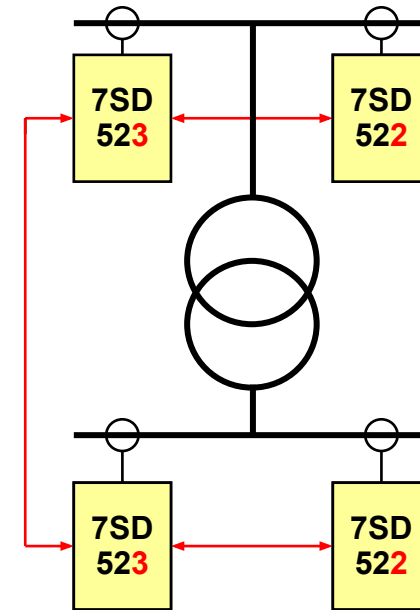
Examples for different Topologies



Chain topology with line in the protected zone



Ring topology with line in the protected zone



Chain topology with transformer in the protected zone

Relay to Relay Communication Designed for the use of Digital Communication Networks and FO ¹⁾

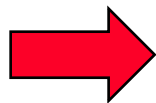
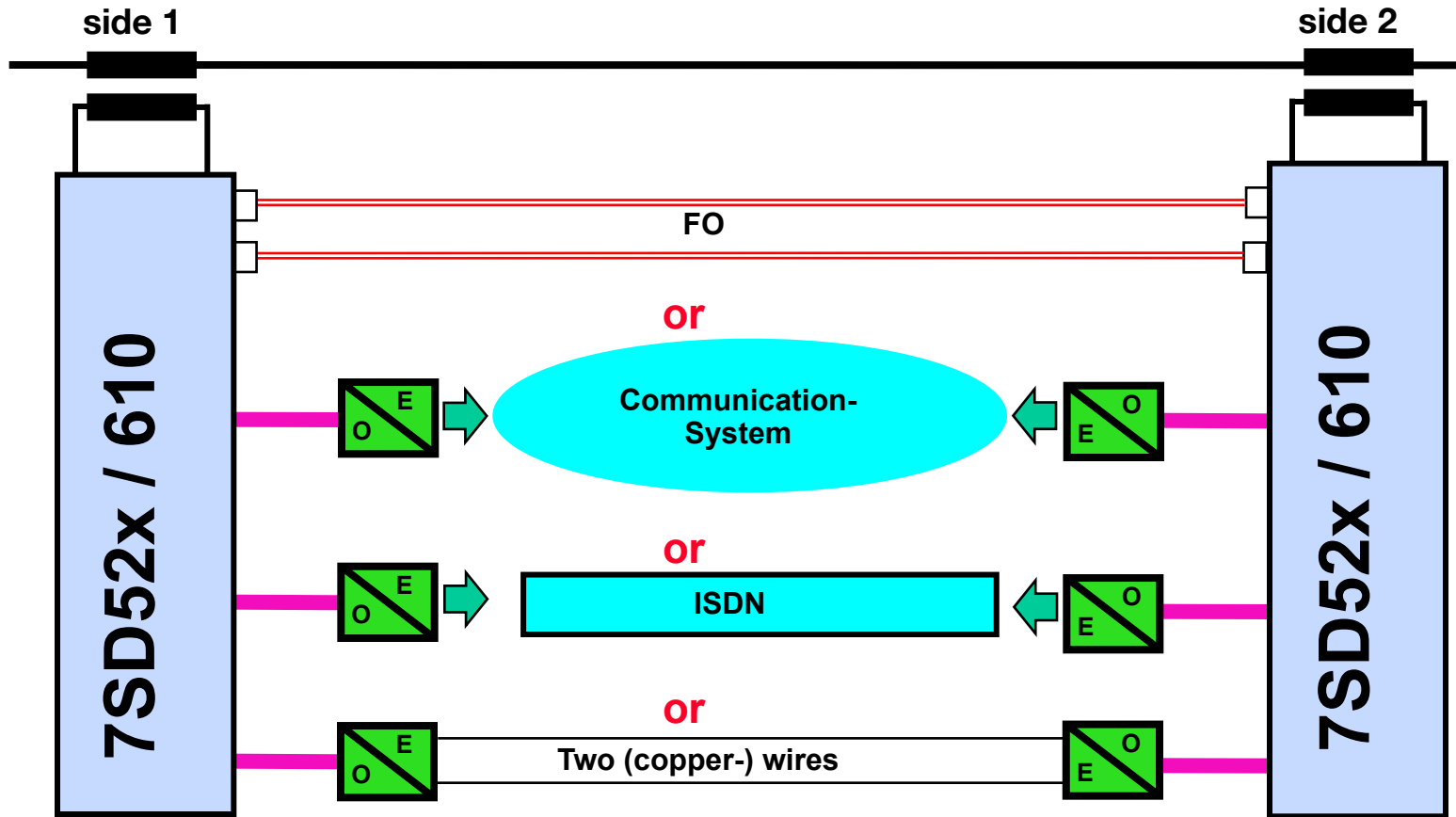
Main features of the relay to relay communication

- **Synchronous data exchange with HDLC- protocols**
Very save through 32 bit CRC-checksum
- **Permanent supervision of the data transmission**
Indication of disturbances and loss of connection
- **Measurement and compensation of the telegram delay time**
Max. 30 ms per connection, automatic adaptation in that range
Immediate detection of delay time changes through switching effects
- **Monitors availability of the data connection**
- **Easy settings according the data link (FO or comms-system)**
(N·64 kBit/s, N settable from 1 - 8 for comms-system, N=8 for FO)
- **Communication device addresses**
Protection devices are clearly assigned to a defined protection section. Each relay knows the addresses of remote.
- **Detection of reflected telegrams in a loop back in a comms- network** - Immediate blocking of 87L function
- **Option: Microsecond exact time synchronisation via GPS 1s pulse input**
Independent measurement of transmit and receive delay time
Hardware prepared for this feature



¹⁾ Fibre optic cables

Relay to Relay Communication (Overview)



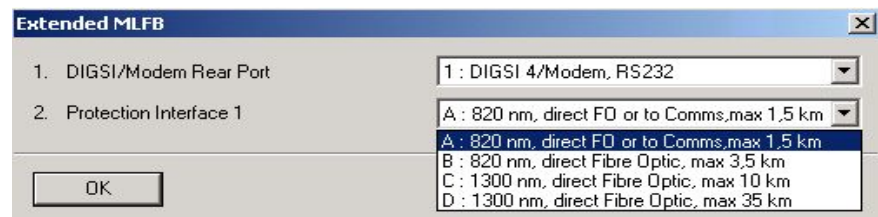
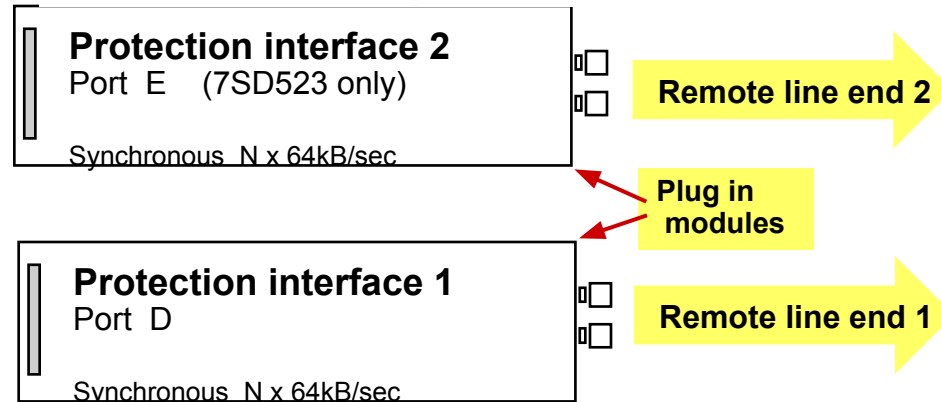
Communication according existing possibilities, the relay remains the same !

Relay to Relay Communication

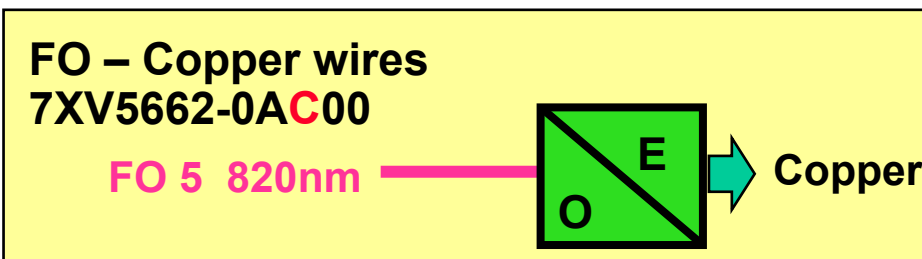
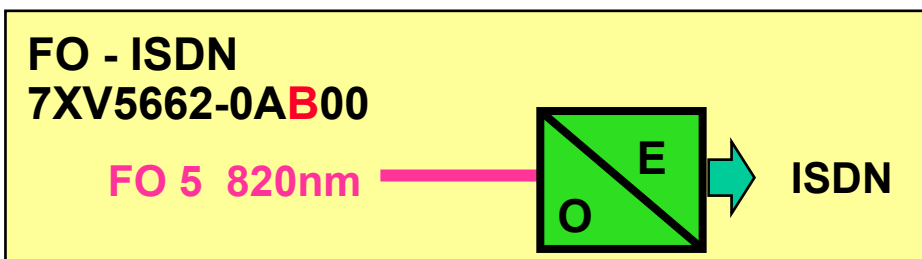
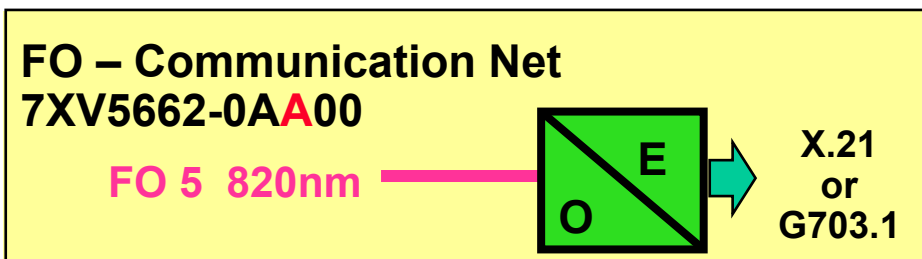
- Communication modules, Protection Interface (PI)

Options for the Protection Interface

FO 5		ST-connector	1.5 km 820 nm Multimode
internal			
FO 6		ST-connector	3.5 km 820 nm Multimode
internal			
FO 17		ST-connector	24 km 1300 nm Monomode
internal			
FO 18		FC-connector	60 km 1300 nm Monomode
internal			
FO 19		FC-connector	100 km 1300 nm Monomode
internal			



Relay to Relay Communication - Communication converter

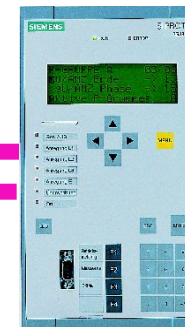
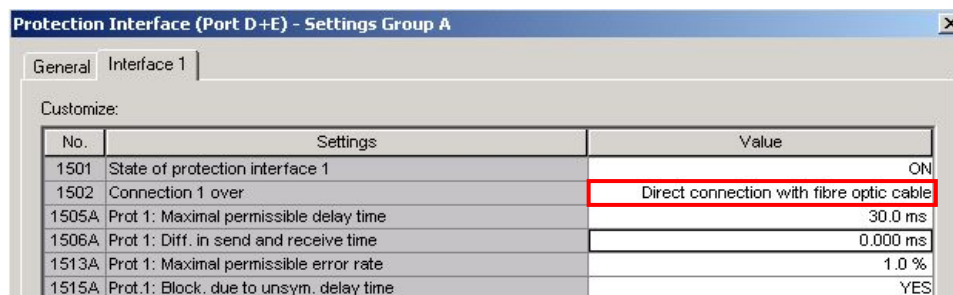


Relay to Relay Communication

- Application: Fibre optic connection

Direct connection with fibre optic (FO) cables

- Offers high speed tripping (12 ms), baud rate is 512 kBit/s
- Flexible plug in modules for different fibre cables or distances



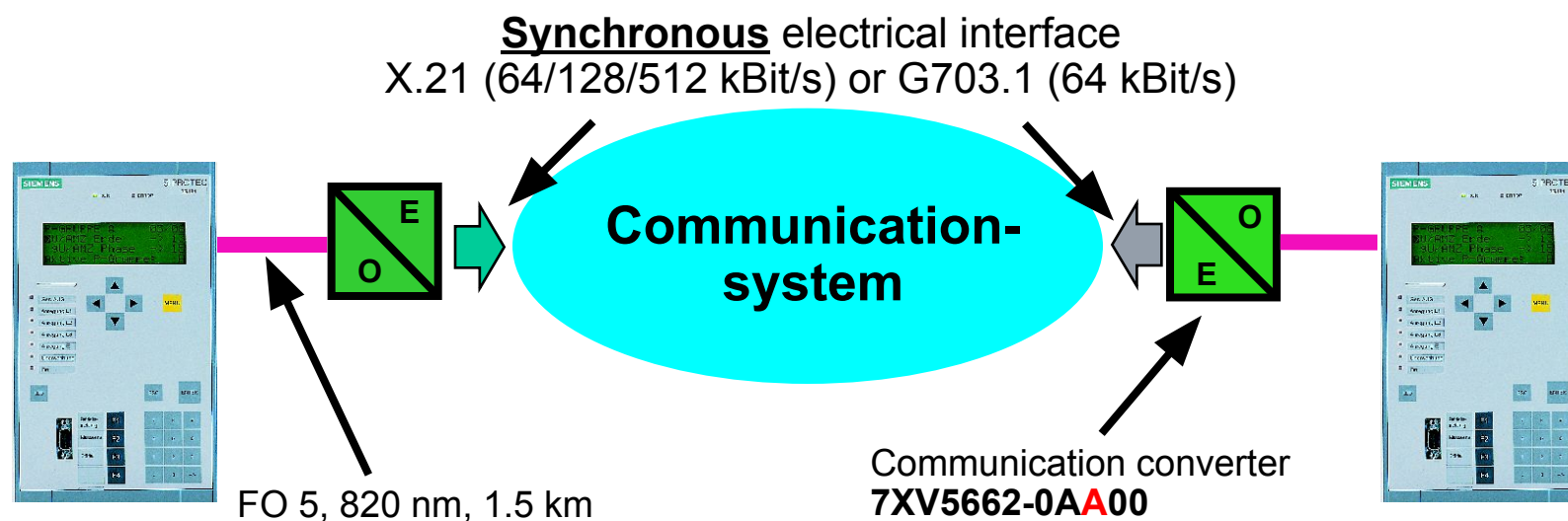
Module in device	Type of connector	Type of fibre	Optical wavelength	Perm. path attenuation	Distance, typical
FO5 ¹⁾	ST	Multimode 62.5/125 µm	820 nm	8 dB	1.5 km 0.95 miles
FO6 ²⁾	ST	Multimode 62.5/125 µm	820 nm	16 dB	3.5 km 2.2 miles
FO7 ²⁾	ST	Monomode 9/125 µm	1300 nm	7 dB	10 km 6.25 miles
FO8 ²⁾	FC	Monomode 9/125 µm	1300 nm	18 dB	35 km 22 miles

Relay to Relay Communication

- Application: Digital communication network

Connection via a communication system with multiplexers

- Automatic delay time measurement (adaptive correction from 0 ms - 30 ms)
- Immediate detection of split-path condition in the transmit or receive path
- Communication addresses clearly identify the relays



Protection Interface (Port D+E) - Settings Group A

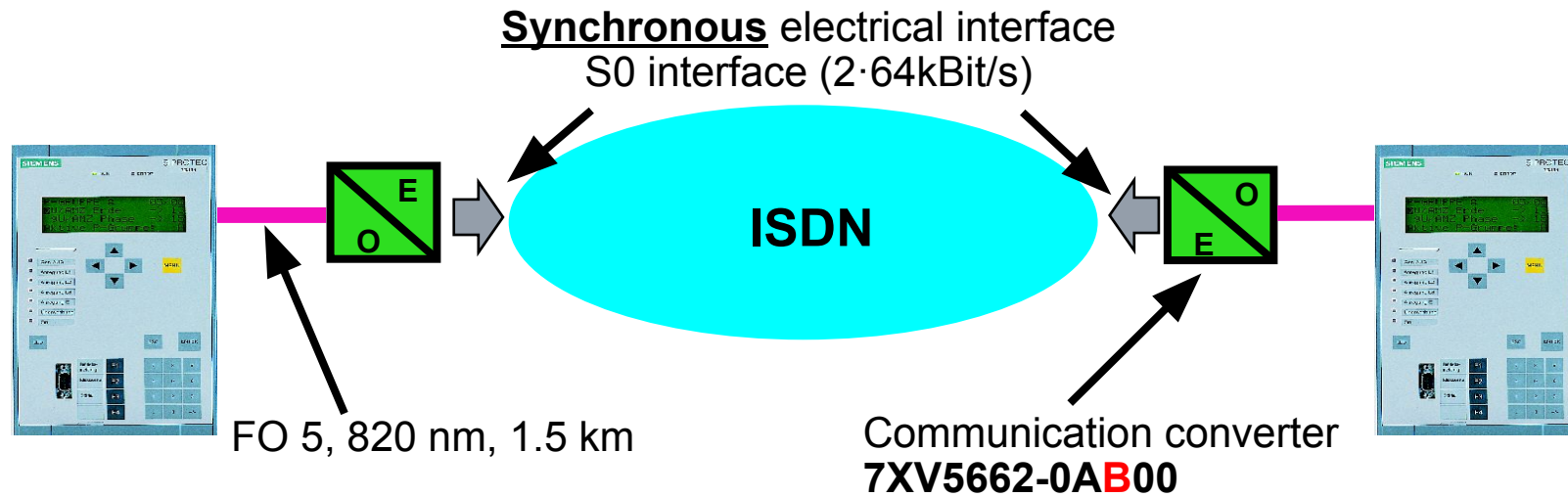
No.	Settings	Value
1501	State of protection interface 1	ON
1502	Connection 1 over	Communication converter with 64 kBit/s
1505A	Prot 1: Maximal permissible delay time	30.0 ms
1506A	Prot 1: Diff. in send and receive time	0.100 ms
1513A	Prot 1: Maximal permissible error rate	1.0 %
1515A	Prot.1: Block. due to unsym. delay time	YES

Relay to Relay Communication

- Application: ISDN network

Connection via an ISDN Network

- Automatic delay time measurement (adaptive correction from 0 ms - 30 ms)
- Immediate detection of split-path condition in the transmit or receive path
- Communication addresses clearly identify the relays



Protection Interface (Port D+E) - Settings Group A

General Interface 1

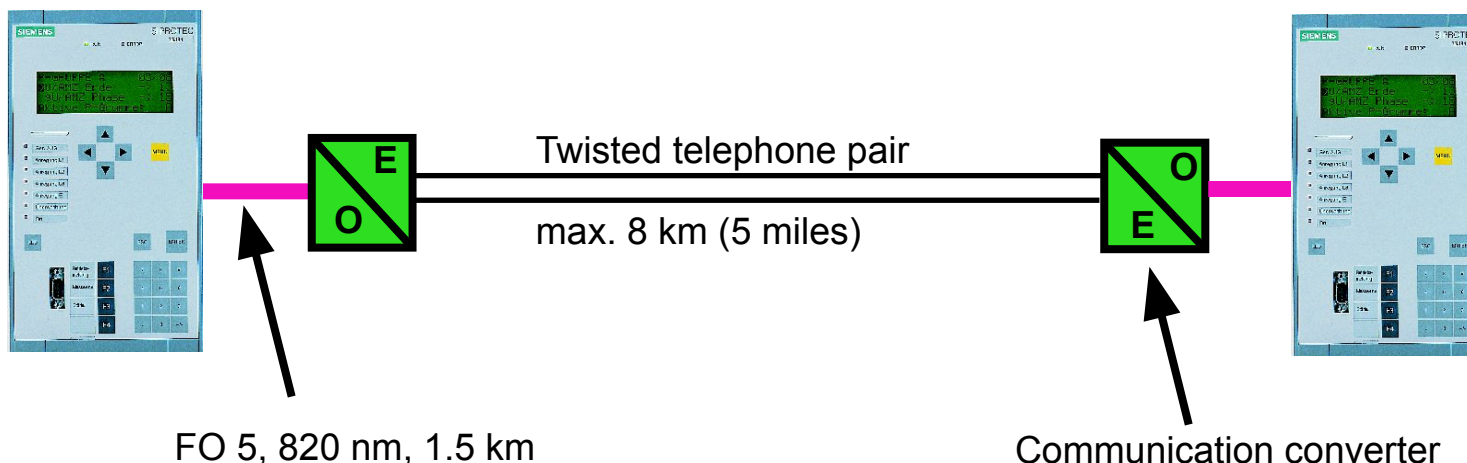
Customize:

No.	Settings	Value
1501	State of protection interface 1	ON
1502	Connection 1 over	Communication converter with 64 kBit/s
1505A	Prot 1: Maximal permissible delay time	30.0 ms
1506A	Prot 1: Diff. in send and receive time	0.100 ms
1513A	Prot 1: Maximal permissible error rate	1.0 %
1515A	Prot.1: Block. due to unsym. delay time	YES

Relay to Relay Communication

- Application: Leased telephone line or Pilot wire (1 of 2)

Leased telephone line (standby or dial-up)
- 2 wire telephone cable (max. 8 km)



Protection Interface (Port D+E) - Settings Group A

General Interface 1

Customize:

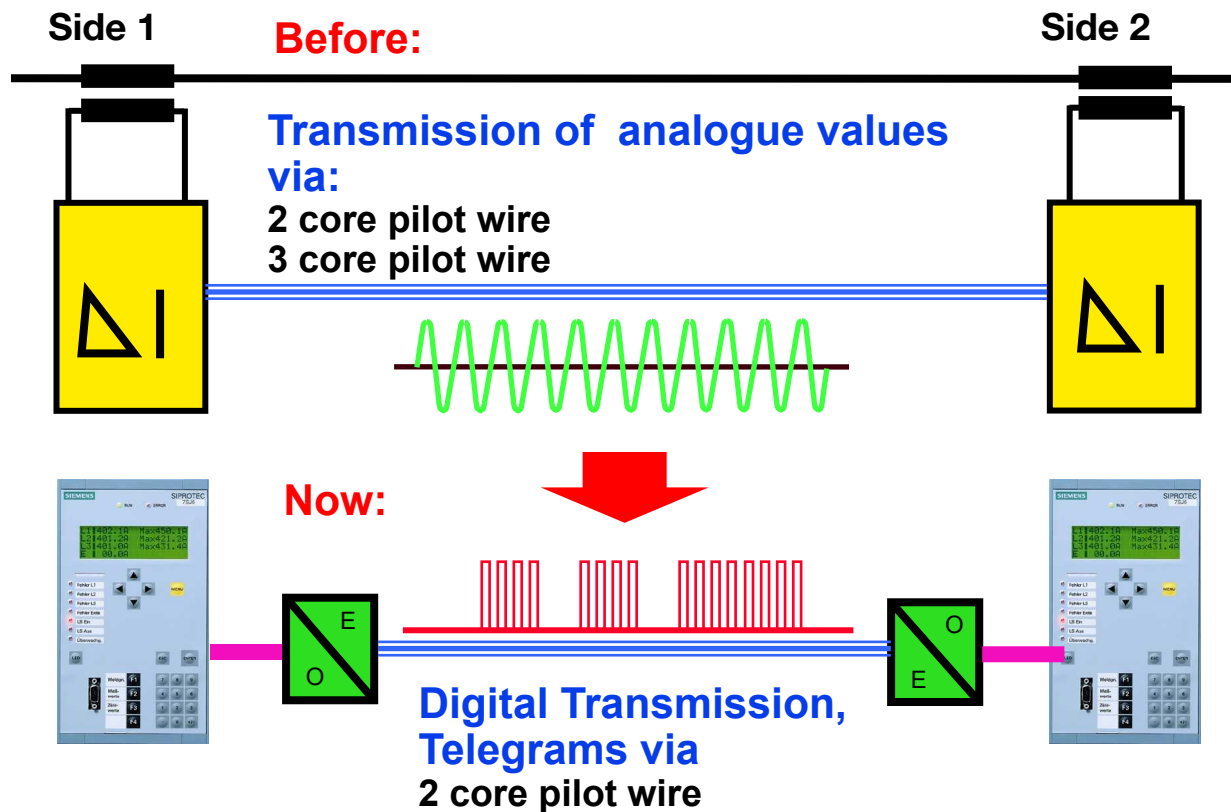
No.	Settings	Value
1501	State of protection interface 1	ON
1502	Connection 1 over	Communication converter with 128 kBit/s
1505A	Prot 1: Maximal permissible delay time	30.0 ms
1506A	Prot 1: Diff. in send and receive time	0.100 ms
1513A	Prot 1: Maximal permissible error rate	1.0 %
1515A	Prot.1: Block. due to unsym. delay time	YES

Relay to Relay Communication

- Application: Leased telephone line or Pilot wire (2 of 2)

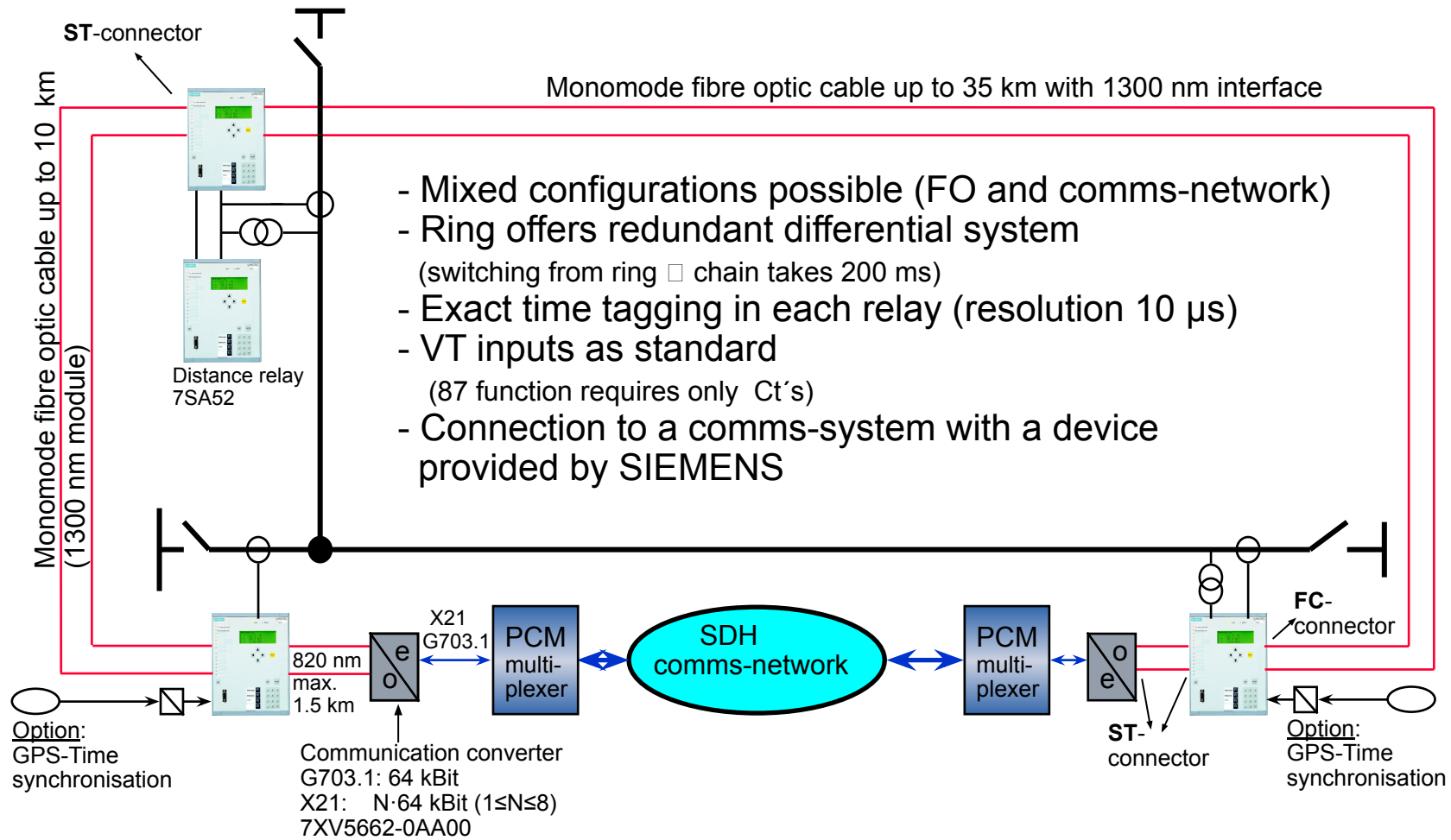
Serial communication

New technology on existing (copper-) connection



Relay to Relay Communication

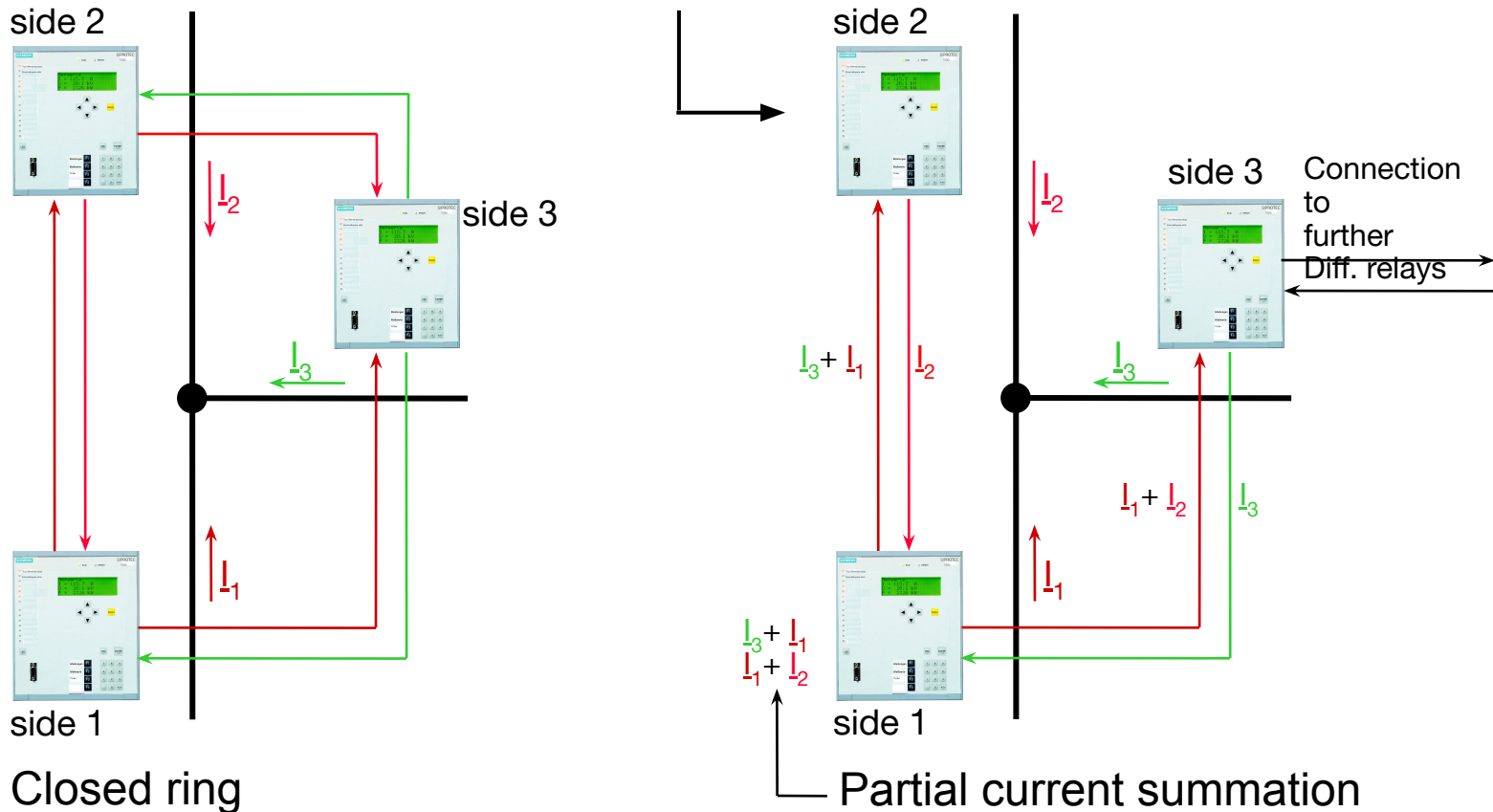
- Application for a three terminal configuration with 7SD523



Relay to Relay Communication

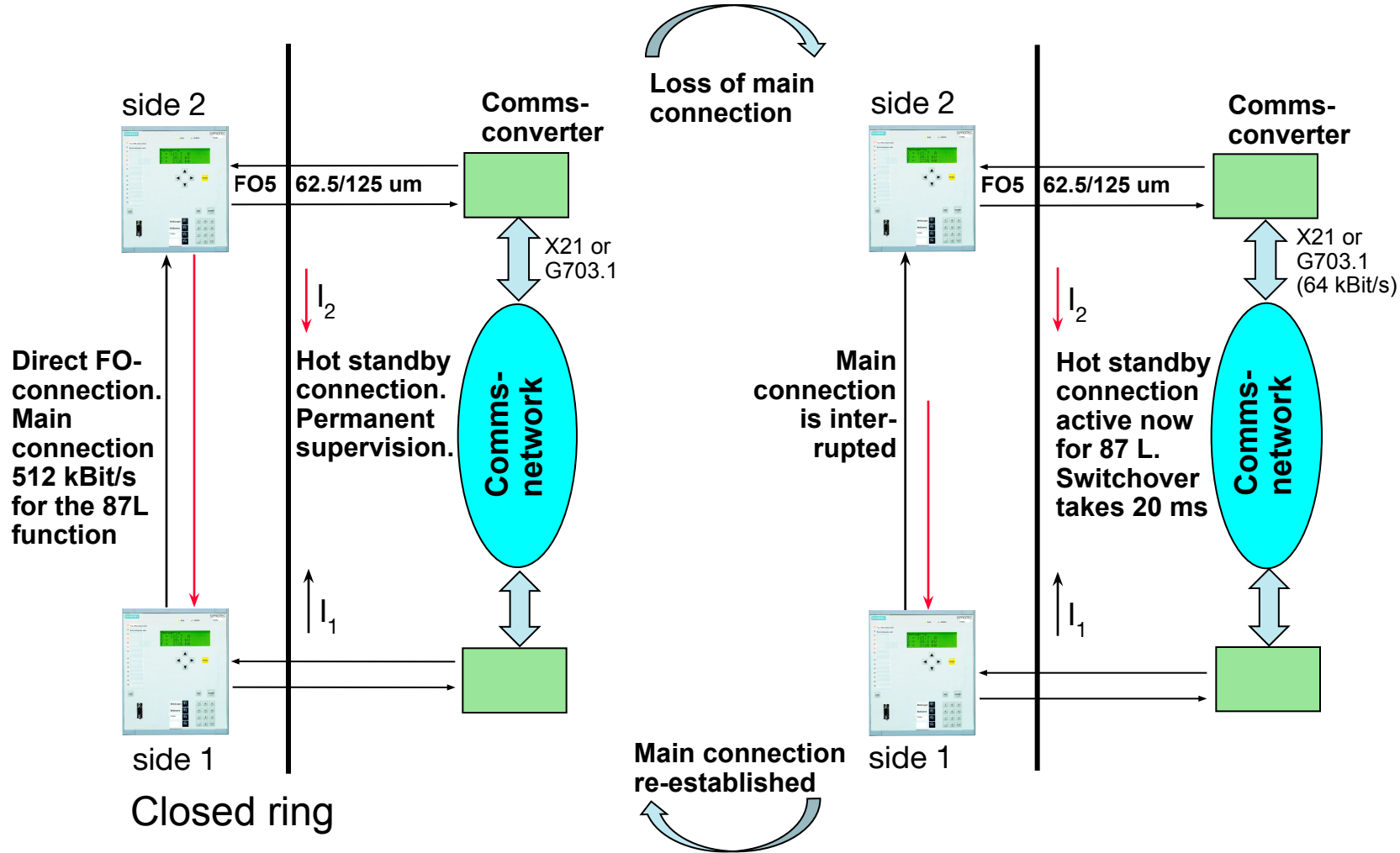
- Ring- and Chain topology, loss of one data connection tolerated

Automatic changeover from closed ring- to chain topology, if case of one connection is lost or not available



Relay to Relay Communication

- Hot- Standby connection in a two terminal configuration



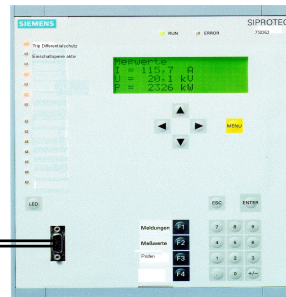
WEB-Technology



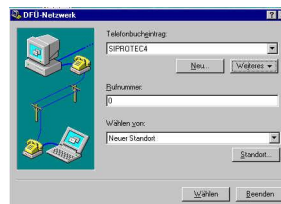
Help system in
INTRANET / INTERNET
<http://www.siprotec.com>



Access to the relay with a WEB Monitor



The homepage of the relay
is:<http://141.142.255.150>
IP-address is set with DIGSI 4
on front- or rear service port



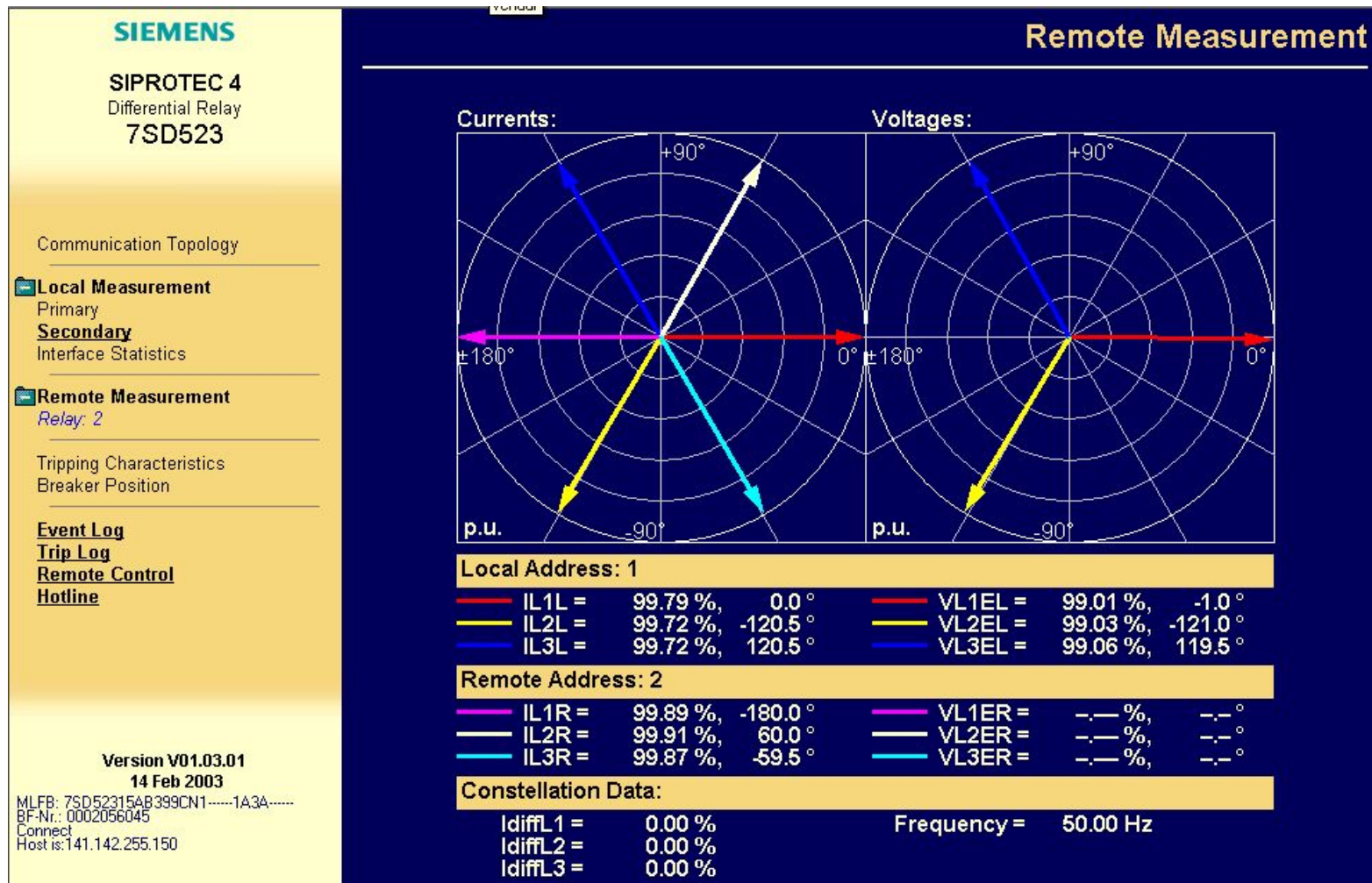
1. Serial connection
Direct or via modem with a
standard DIAL-UP Network

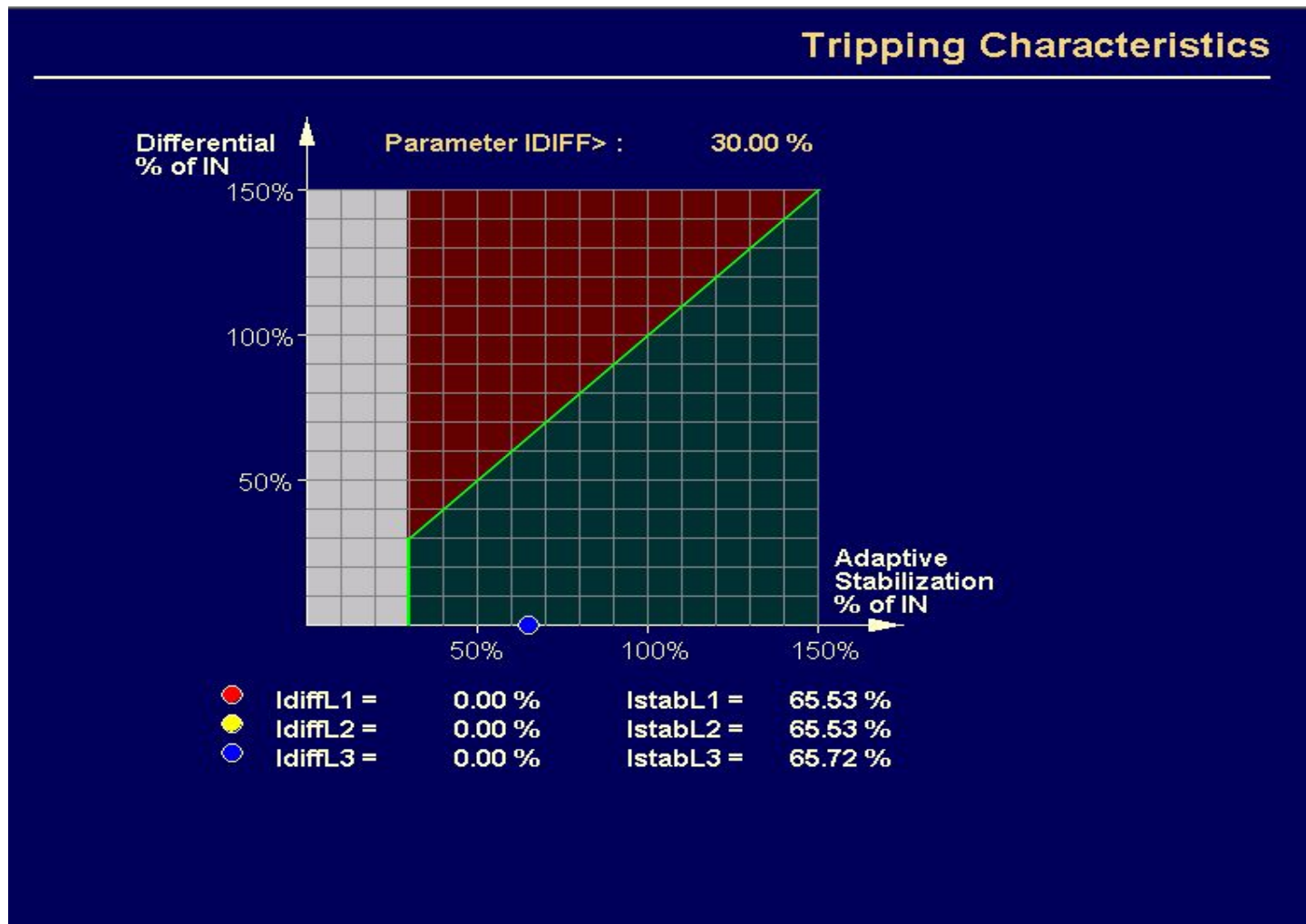
2. HTML page view in a WEB Monitor
with the IP-address of the relay
<http://141.142.255.150>



**WEB server in the relays
firmware**

Server sends it's HTML-pages
and JAVA-code to the WEB Monitor
after a DIAL-UP connection





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