

Siemens Power Academy TD



Line Differential Protection 7SD52x / 7SD610

Presentation

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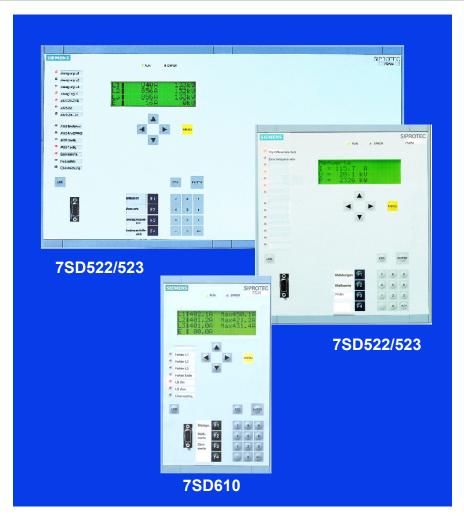
Using numerical protetction devices V4

Line differential relays 87L-SIPROTEC 4



Universal Line Differential Relays 87L

- 7SD610 (2 ends)
- 7SD522 (2 ends, additional I/O)
- 7SD523 (2 up to 6 ends)





- The protection adapts its characteristic by itself. Adaptive measurement reduces the setting complexity and ensures maximum sensitivity.
- Multi terminal applications up to 6 line ends and redundant Relay to Relay communication.
- A transformer inside the feeder zone of protection is fully accommodated by the feeder differential protection and configured with a few simple settings.
- Current transformer mismatch 1:8 without matching transformers.
 Different CT classes possible.
- Flexible protection data communication uses a variety of communication media.
- Secure operation at unsymmetrical propagation times in Communication networks.
- High speed measurement supervision
- Simplified commissioning by application of WEB- technology



• Device	• 7SD610 1/3 19"	• 7SD522	• 7SD522 1/1 19"	7SD523 ½ 19"	• 7SD523 1/1 19"
		1/2 19"			
Current Inputs (I _{ph} / I _E)	(3 / 1)*	• (3 / 1)*	• (3 / 1)*	(3 / 1)*	• (3 / 1)*
Voltage Inputs (U_{ph} / U_{E})	3/1	• 3 / 1	• 3 / 1	3/1	• 3 / 1
Binary Inputs	4 7	- 8	• 16 // 24	8	• 16 // 24
Binary Outputs	• 5	- 15	• (23 // 31)**	15	• (23 // 31)**
Life contact	1	1	• 1	1	•1
LC Display	4 Lines	• 4 Lines	• 4 Lines	4 Lines	4 Lines
Protection Interfaces	1	1	• 1	2	• 2

- 1A, 5A changeable (jumper position) depending on ordering data
- 5 high-speed relays

Protection and communication join together Three benefits of 87L-SIPROTEC





Differential protection for the universal use with easy to handle settings

Two up to six line ends, for serial and parallel compensated lines, handles transformers and compensation coils within the protection zone, tripping time approx. 12 ms with fast high set element

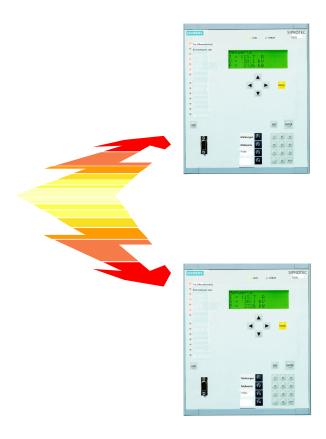
Adaptive differential measurement

Automatic consideration of CT errors and communication-errors
Increased set point during switching-on conditions

Direct and modular connection to fibre optic and digital communication networks

Main protection function 87: Features of the differential function





- Phase selective multi-end differential protection (2 6 ends).
- Fundamental vector comparison for the sensitive trip stage (Setting of $I_{Diff} > = 0.2 - 0.3 I_{N}$). Suppress decaying DC-components and harmonics. Therefore allows a sensitive setting.
- Tripping time 12 ms with fast current comparison protection (Setting of I_{Diff}>> > 1.2 I_{Load.max})
- Dynamic increase of differential set point I_{Diff} during switch-on of long lines / cables
- CT saturation detector (only 5 ms saturation free time due to external faults necessary)
- Phase selective intertrip
- Settable delay time for single phase faults (feature for inductive compensated networks)
- Transformer option: Inrush 2nd harmonic restraint with vector group adaptation. Undelayed trip for high fault currents
- Lockout function (Seal in of trip command)

Additional functions in the relay









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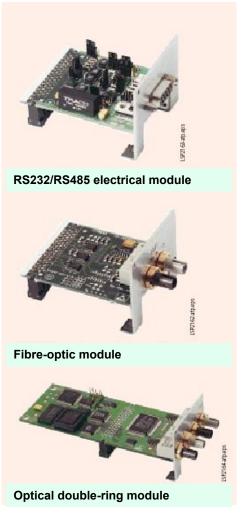
- Switch On to Fault protection (SOFT) (with breaker position from remote)
- 3 stage backup- or emergency O/C protection (IEC /ANSI) 50, 50N, 51, 51N Runs in parallel (backup) or in emergency mode,
- Three pole and single pole AR (Single pole AR during 2pole fault without earth possible, Adaptive AR - Switch on from one side)

if 87L is blocked. (from external or due to communication-failure)

- **Breaker Failure protection 50BF**
- Thermal Overload function (Thermal replica with I_{Operation})
- User definable logic and control functions also with signals from remote (AND, OR, NOT, Timer, Flip-Flop)
- 4 remote commands via binary input or logic inputs (destination) relay is addressable), 24 remote signals (only 7SD522/523)
- Operational values: Currents I, Voltages V, Active/Reactive Power, Delay time, Differential-/Restraint current - Remote end I/V-values
- Exactly time synchronized fault records with voltages, currents. binary traces and differential and restraint current per phase
- **Fast monitoring functions** Fast broken current-wire supervision □ blocks 87L and avoids malfunction

Communication features





Flexibility due to plug in modules Compatibility to international standards

- Front interface
 - DIGS14
 - **WEB Monitor**
- Service interface (s)
 - DIGSI4 operation
 - modem connection

- System interface
 - IEC60870-5-103
 - Profibus DP
 - DNP3.0
- Time synchronising
 - IRIG-B (GPS)
 - DCF77

I_{Diff}>: Vector comparison

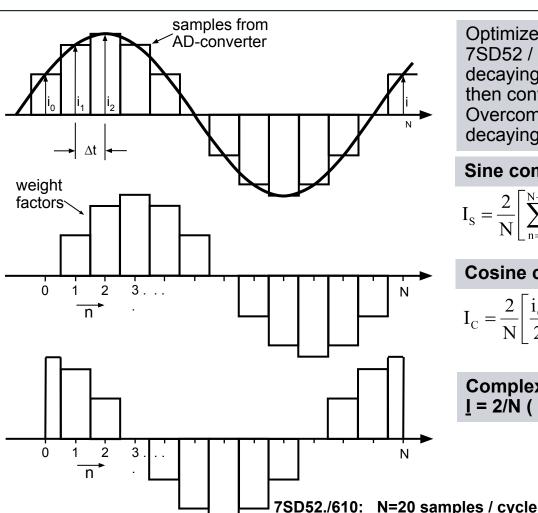


Vector comparison offers high sensitivity for high-resistive faults

- DC components and harmonics are suppressed by Advanced Fourier Filters
 Suppress decaying DC-component 4 times better then a classical Fourier Filter.
- •Different types of Ct's allowed, even with a sensitive setting.
- Relative slow, because of 1 cycle (20 ms,50Hz) filtering window Results in a tripping time from 30-50 ms for high resistive faults (I_{Diff} < 1.2 .. 2 I_{N})

I_{Diff}>: Vector comparison with Advanced Fourier filters (Basic principle)





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Optimized filtering coefficients for 7SD52 / 7SD610 designed for suppressing decaying DC-components 4 times better then conventional Fourier-filters. Overcome stability problems with decaying DC-components

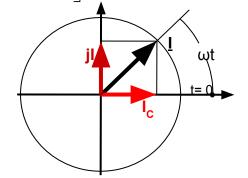
Sine component:

$$I_{S} = \frac{2}{N} \left[\sum_{n=1}^{N-1} \sin(\omega \cdot n \cdot \Delta t) \cdot i_{n} \right] \rightarrow 1...N = 20$$

Cosine component:

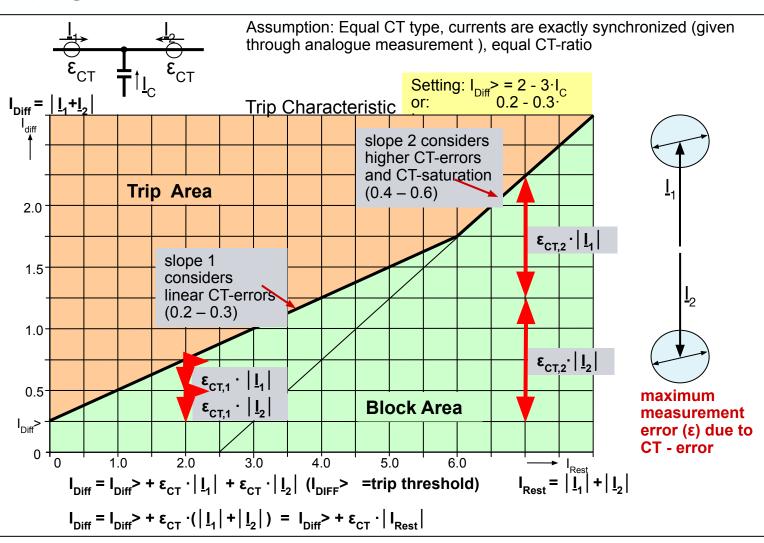
$$I_{C} = \frac{2}{N} \left[\frac{i_{0}}{2} + \frac{i_{N}}{2} + \sum_{n=1}^{N-1} \cos(\omega \cdot n \cdot \Delta t) \cdot i_{n} \right] \rightarrow 1...N = 20$$

Complex vector $\underline{I} = 2/N (|\underline{I}_c + \underline{j}|_s)$



I_{Diff}>: Theory of the <u>classical</u> differential tripping characteristic





(1 of 2)



Example: CT class 10P10, $S_n = 10VA$, $I_{sn} = 1A$ 10% tolerance at K_{SSC} (= 10 = $k_{ALF N}$) (in case of nominal burden is connected)

$$k_{ALF} = k_{ALF_N} \cdot \frac{P_{ct} + P_b}{P_{ct} + P_b'} = k_{ALF_N} \cdot \frac{R_{ct} + R_b}{R_{ct} + R_b'} \quad \text{with:} \quad \mathsf{K}_{\mathsf{SSC}} : \quad \text{rated symmetrical short-circular current factor} \\ \mathsf{K}_{\mathsf{ALF}_N} : \quad \mathsf{rated} \, \underline{\mathsf{Accuracy}} \, \underline{\mathsf{Limit}} \, \underline{\mathsf{Eactor}} \\ \mathsf{K}_{\mathsf{ALF}_N} : \quad \mathsf{rated} \, \underline{\mathsf{Accuracy}} \, \underline{\mathsf{Limit}} \, \underline{\mathsf{Eactor}} \\ \mathsf{K}_{\mathsf{alf}} : \quad \mathsf{secondary} \, \mathsf{winding} \, \mathsf{rete} \\ \mathsf{R}_{\mathsf{b}} : \quad \mathsf{rated} \, \mathsf{rete} \, \mathsf{ret$$

rated symmetrical short-circuit

current factor (IEC 60044-6)

actual Accuracy Limit Factor secondary winding resistance

actual resistive burden

rated resistive burden

Thumb rule:

 $R_{ct} \approx 0.1...0.2$

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Nominal burden:

 $R_b = \frac{S_n}{I^2} = \frac{10VA}{1^2 A^2} = 10\Omega \rightarrow R_{ct} \approx 2\Omega$

$$\frac{k_{ALF}}{k_{ALF}N} = \frac{2\Omega + 10\Omega}{2\Omega + 1\Omega} = 4$$

☐ If less then rated burden is connected to the CT,

the CT- error for load conditions (ϵ_{Load}) can be used for calculations with currents higher than the nominal current of the CT (I_{pn})!

(In the example here: ϵ_{Load} could be taken for currents up to $4 \cdot I_{pn}$

 $(R_{IFADS} +$



As the I_{Diff} > step must be (very) sensitive for high resistive faults at maximum Load, for usual applications there is no need to set the

Resulting Relay Parameter (with exact calculation)

parameter 0251 (k_{ALF}/K_{ALF N}) higher than 1.5 !!

• k_{ALF} / k_{ALF} = 1.5 (calculation as above = 4 , 4 > 1.5 \square Setting: 1.5) [remains 1 if CT-data's are unknown]

• IEC 60044 -1:

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tolerance in load area up to $\rm k_{ALF}$ / $\rm k_{ALF~N}$: <2% for 5P (TPY), <3% for 10P (TPX) Ct's Recommended setting in the relay: 3% for 5P, 5% for 10P

total error at accuracy limit $k_{ALF\ N}$ = 5% for class 5P and 10% for class 10 P Recommended setting in the relay: 10% for 5P, 15% for 10P

I_{Diff}>: Approximation of the CT- error



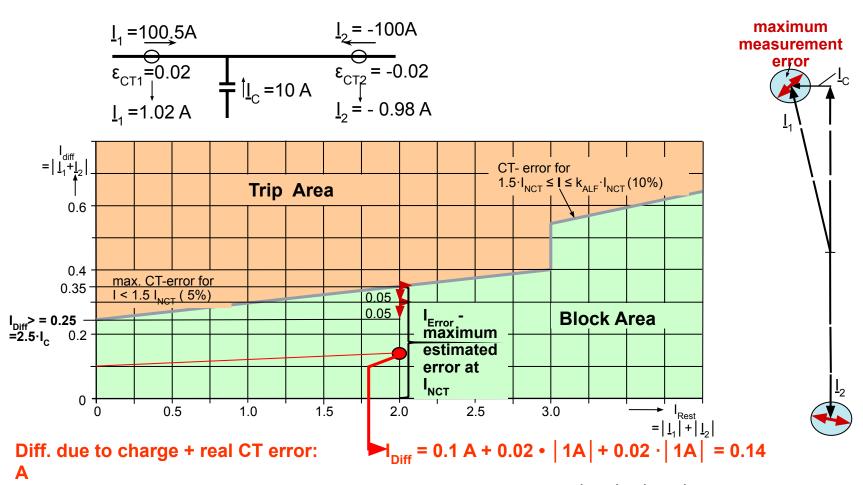
Basis for the adaptive restraint current calculation (max. expected differential current due to CT-errors) is the estimated error of each CT

from the CT-data's Power System Data 1 Transformers | Power System | Breaker | CT Datas Customize: Settings in Settings Value in % of DIGSI 4 k_alf/k_alf nominal 1.50 3.0 % 0253 CT Error in % at k_alf/k_alf nominal 10.0 % 0254 CT Error in % at k_alf nominal 50 **Example: CT class 5P5** 10VA, R_{ct} = 2Ω, I_{sn} = 1A 40 $\varepsilon_{\text{Load}}$ < 2%, $\varepsilon_{\text{Fault}}$ at $k_{\text{ALF N}}$ = 5% actual burden $R_b' = 60\%$ of R_b 30 25 0254 = 20 10% Max. error of 0253 =the real CT 3% 10 6 $=1.5 \rightarrow 0251 = 1.5$

I_{Diff}>: Example for a setting at nominal current



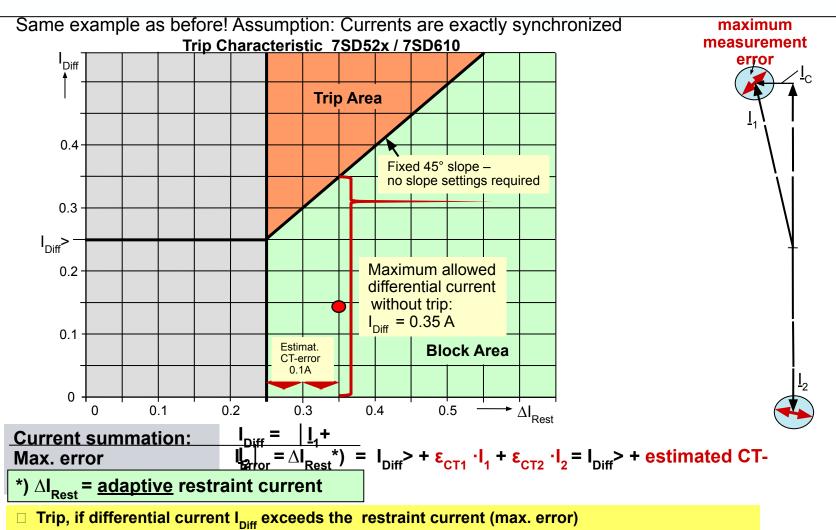
Assumption: CT-ratio is 100/1A, real error of Ct's is 2% (0.02) up to 1.5 I_{NCT}



Max. estimated error = Restraint current : I = 0.25 A + 0.05 • (1A + 1 A) = 0.35 A C 4 Page 15 Siemens Power Academy TD 07.1 Differential relay 7SD

I_{Diff}>: Adaptive differential relaying Restraint current with consideration of the CT- errors



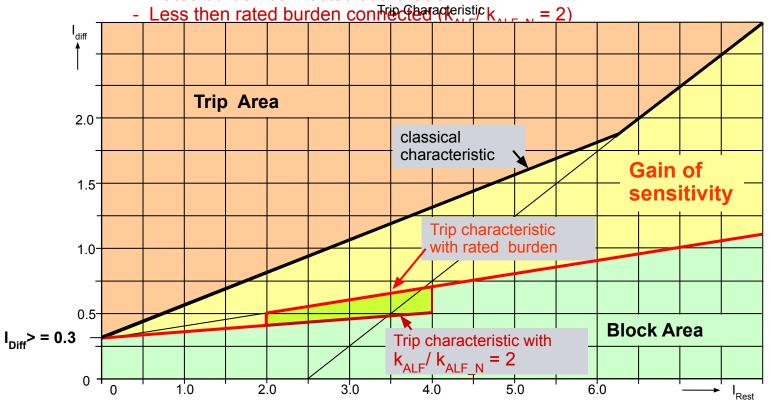


I_{Diff}>: New differential method compared with a classical differential characteristic



Assumption: Equal Ct's on both side, no effects from comms-system, standard settings

- Rated burden connected at the Ct's

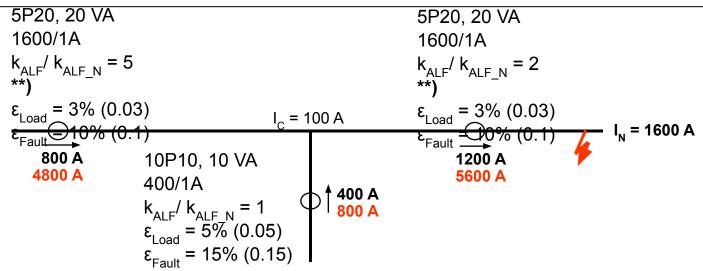


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Classical: $I_{Diff} = 0.3 + 0.25 \cdot I_{Rest} = 0.3 + 0.25 \cdot 2 = 0.8$ (sensitivity under full load) New: $I_{Diff} = 0.3 + 0.05 \cdot I_{Rest} = 0.3 + 0.05 \cdot 2 = 0.4$ (double sensitivity under full load)

I_{Diff}>: Example 1: Adaptive (self-) restraining





**) Settings for this example.

In a real case both settings would be 1.5

 I_{Diff} > = Differential-Setting = 2.5 · I_{C} = 250 A

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 $\Delta I_{Rest} = I_{Diff} > + sum of estimated Ct- errors$

 I_{Diff} = Differential current due to vector summation of the individual currents

Case 1 (normal operation)

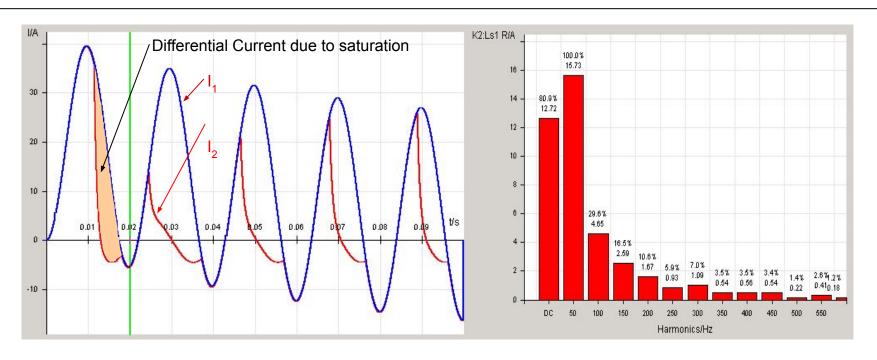
$$\Delta I_{Rest} = 2.5 \cdot 100A + 0.03 \cdot 800A + 0.03 \cdot 1200A + 0.05 \cdot 400A = 330A$$
 $\Delta I_{Rest} / I_{N} = 0.206$ $I_{Diff} = 100 A (=I_{C})$ $I_{Diff} / I_{N} = 0.0625$

Case 2 (External Fault)

 $\Delta I_{Rest} = 2.5 \cdot 100 A + 0.03 \cdot 4800 A + 0.1 \cdot 5600 A + 0.15 \cdot 800 A = 1074 A$ $\Delta I_{Rest} / I_{N} = 0.671 I_{Diff} = 40 A (due to lower voltage)$ $\Delta I_{N} = 0.025 I_{Diff} / I_{N} = 0.025 I_{$

I_{Diff}>: CT- saturation detector based on harmonic analysis **SIEMENS** of the current wave form - Signal analysis





- Wave form detector recognize saturation from

DC, f_2 , f_3 , f_4 , f_5 rated to the fundamental f_1 Factor = 1 - no saturation

Factor > 1 - saturation □Increase of CT- error with a factor f_{Sat}.

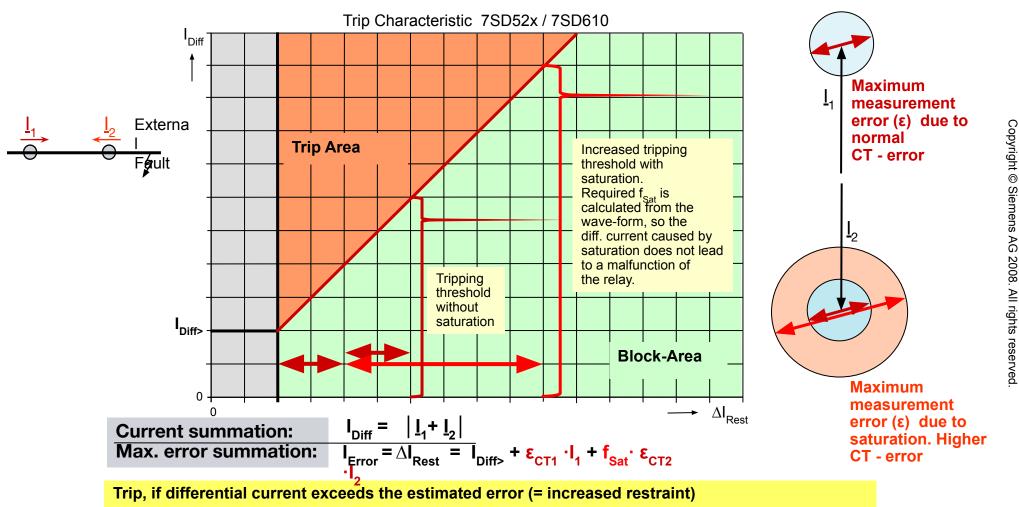
Results in higher restraint current.

More differential current is required for tripping.

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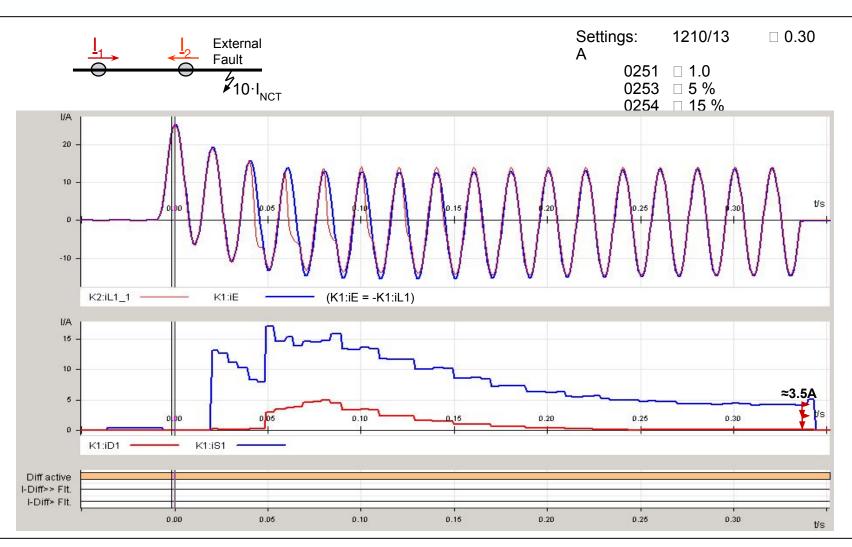
I_{Diff}>: Adaptive differential relaying

Consideration of nonlinear CT- errors due to saturation



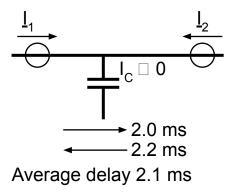
I_{Diff}>: Test: max. asymmetrical offset , Ct saturation





I_{Diff}>: Adaptive consideration of a <u>permanent</u> time difference in transmit- and receive direction

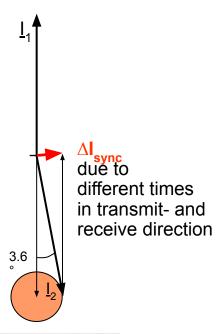




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$$\begin{split} & \Delta \Phi_{\text{sync}} \approx \frac{\Delta t \cdot 360^{\circ}}{20 \text{ms}} \rightarrow (50 \text{Hz}) \\ & \text{here} : \Delta \Phi_{\text{sync}} \approx \frac{0.2 \text{ms} \cdot 360^{\circ}}{20 \text{ms}} = 3.6^{\circ} \\ & = \frac{3.6^{\circ} \cdot 2\pi}{360^{\circ}} = 0.06283 \\ & \Delta I_{\text{sync}} \approx \Delta \Phi_{\text{sync}} \cdot \left| \underline{I}_{\text{sync}} \right| \approx \Delta \Phi_{\text{sync}} \cdot \left| \underline{I}_{2} \right| \end{split}$$

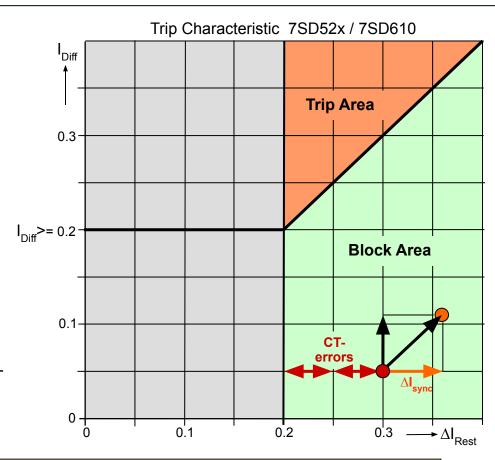
(For more details: refer to 7SD52 Synchronisation)





I_{Diff}>: Adaptive consideration of a <u>permanent</u> time difference. Total "Restraint Current"





Diff. current::

 $I_{\text{Diff}} = I_{\text{C}} + \Delta I_{\text{sync}}$ $\Delta I_{\text{Rest}} = I_{\text{Diff}} > + \text{CT-errors} +$ Rest. current:

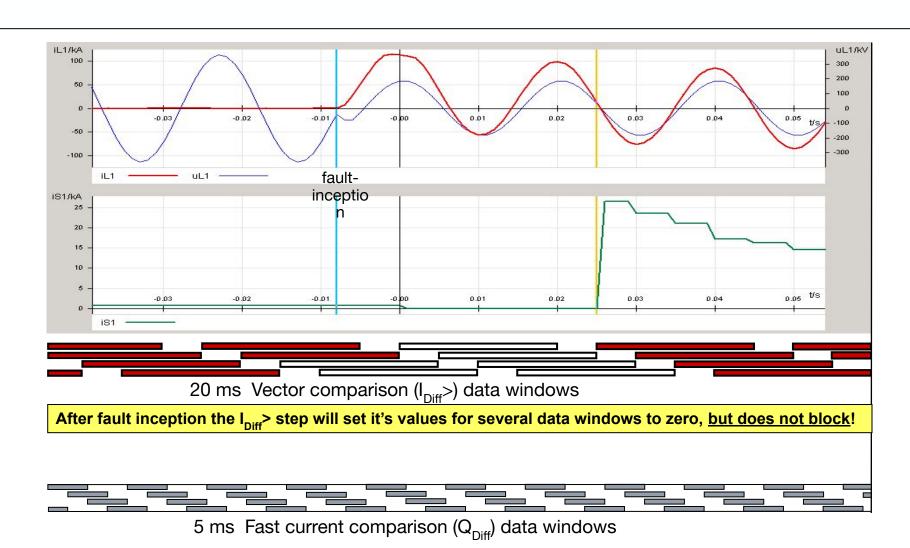
 $\Delta I_{\rm sync}$

Total "Restraint Current":

$$\Delta I_{\text{Rest}} = I_{\text{Diff}} > + f_{\text{Sat1}} \cdot \epsilon_{\text{CT1}} \cdot I_{1} + f_{\text{Sat2}} \cdot \epsilon_{\text{CT2}} \cdot I_{2} + \Delta I_{\text{sync}}$$

I_{Diff}>: Sliding data windows after fault inception





I_{Diff}>> (Q_{Diff}) : Fast current comparison



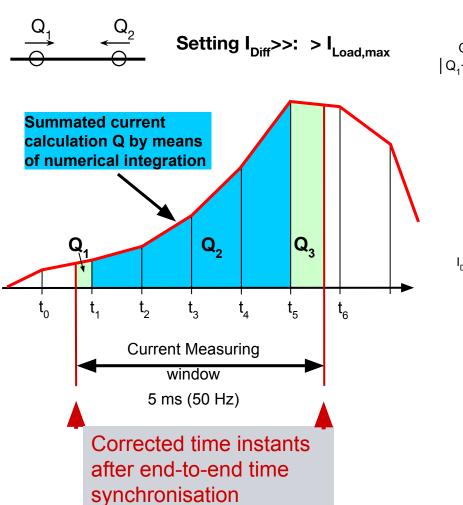
<u>Fast Current comparison</u> offers high speed tripping and a fast decision for internal or external fault condition

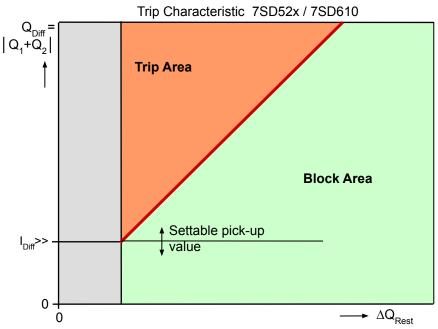
- Current comparison step doesn't suppress DC-components and harmonics.
 (simple integration)
 - Therefore recommended setting is $> I_{Load,max}$ (1.2 2 I_N).
- Current comparison decides in 5 ms for internal or external faults (5 ms window)
 <u>Internal</u>: Immediate trip command (trip time typical 12 ms for 2 or 3 end topology)
 for differential currents I_{Diff} > 1.2 2 I_N
 - External: If I_{Fault} > 2.5·I_{Diff} >> setting: immediate **blocking** of the current comparison.

Reason: CT-saturation possible. Avoids any risk for stability due to differential current from current comparison.

I_{Diff}>> (Q_{Diff}) : Fast current comparison algorithm (Basic principle)



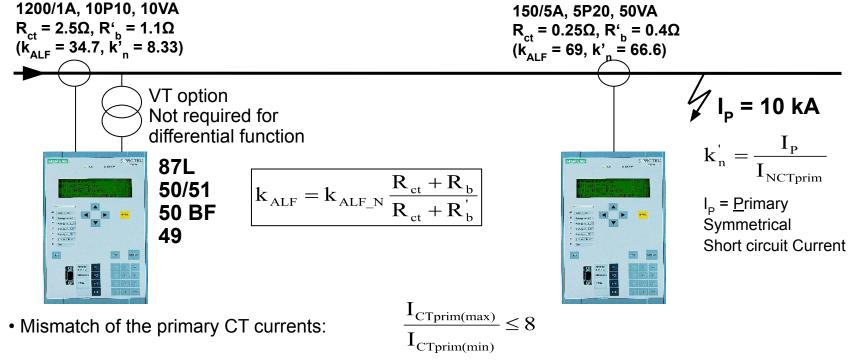




Calculated restraint values from CT-errors (always higher CT-error is taken). Similar principal as vector comparison for restraint current calculation.

CT- requirements, mismatch of the primary CT currents





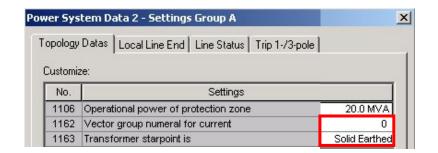
- 1A or 5A input selectable in the relay
- CT data's / errors are set in the relay and automatically considered in the restraint current calculation
- CT-requirements:

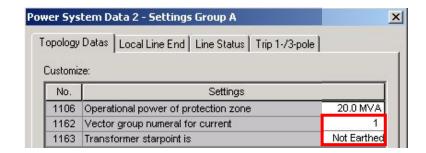
1st condition: $k_{ALF} > k'_{n}$

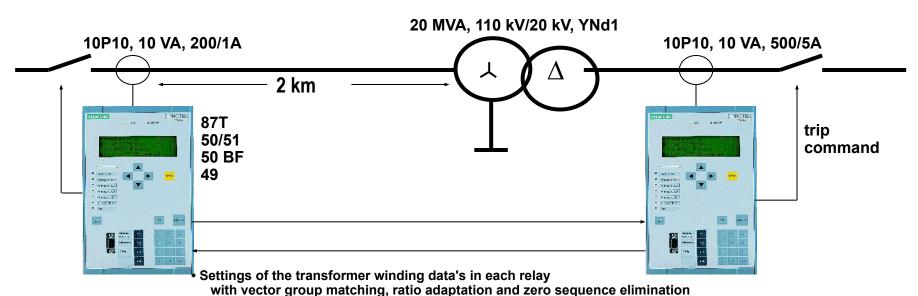
2nd condition: $k_{ALF} \ge 30$ or $\frac{1}{4}$ AC cycle saturation free time (5ms for 50Hz)

Application - Transformer and line/cable in the protection zone





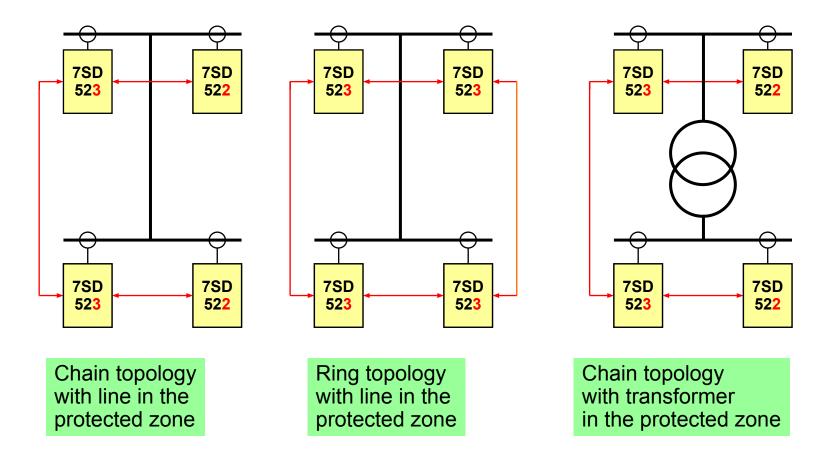




- Differential set point is rated to the nominal current of the transformer
- Inrush restraint with second harmonic included (time limit for Cross block)
- High set element for immediate trip (12 ms) through heavy internal fault currents

Examples for different Topologies





Relay to Relay Communication Designed for the use of Digital Communication Networks and FO 1)





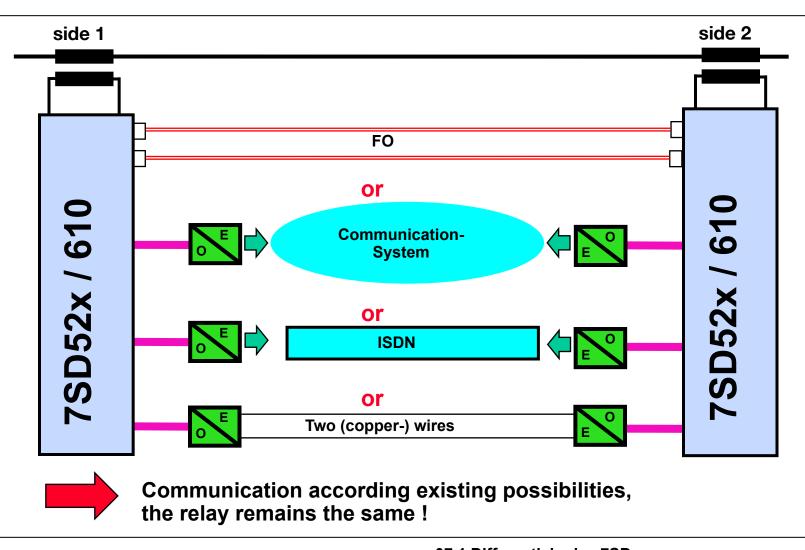
Main features of the relay to relay communication

- Synchronous data exchange with HDLC- protocols Very save through 32 bit CRC-checksum
- Permanent supervision of the data transmission Indication of disturbances and loss of connection
- Measurement and compensation of the telegram delay time Max. 30 ms per connection, automatic adaptation in that range Immediate detection of delay time changes through switching effects
- Monitors availability of the data connection
- Easy settings according the data link (FO or comms-system) (N·64 kBit/s, N settable from 1 - 8 for comms-system, N=8 for FO)
- Communication device addresses Protection devices are clearly assigned to a defined protection section. Each relay knows the addresses of remote.
- Detection of reflected telegrams in a loop back in a comms- network - Immediate blocking of 87L function
- **Option:** Microsecond exact time synchronisation via GPS 1s pulse input

Independent measurement of transmit and receive delay time Hardware prepared for this feature

Relay to Relay Communication (Overview)

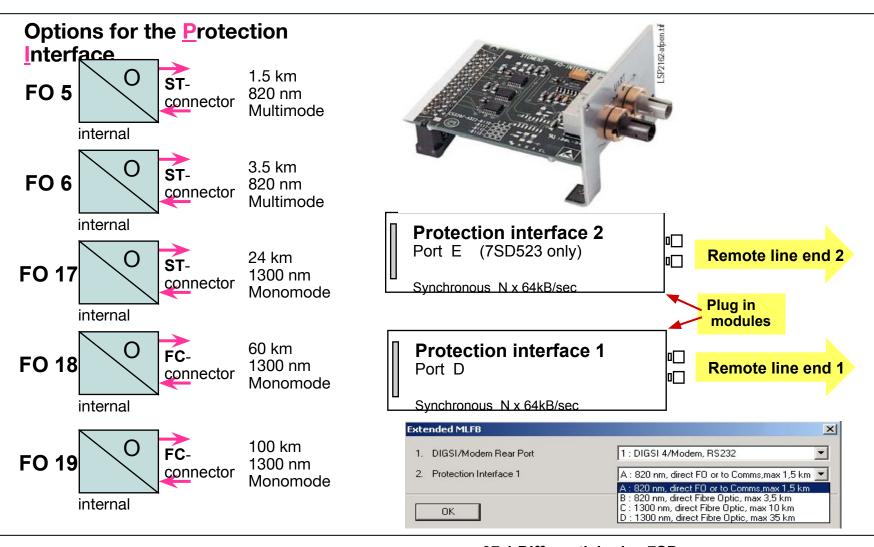




Relay to Relay Communication



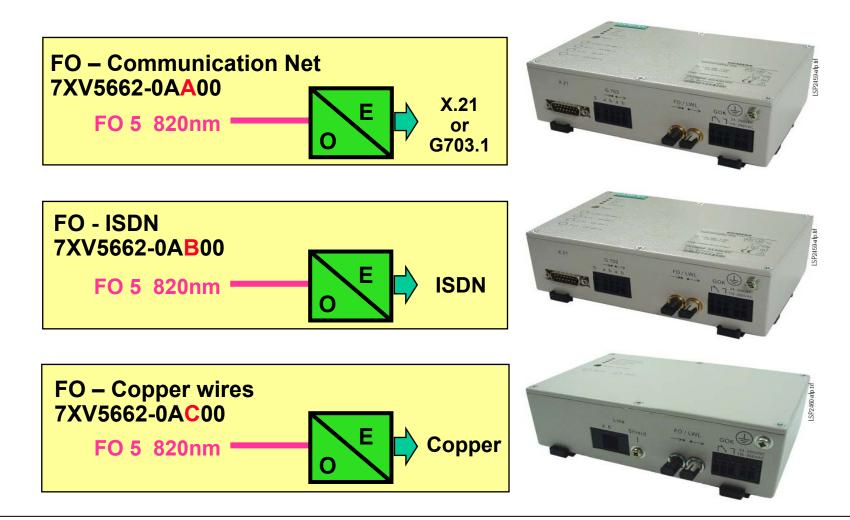
- Communication modules, Protection Interface (PI)



Relay to Relay Communication

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- Communication converter

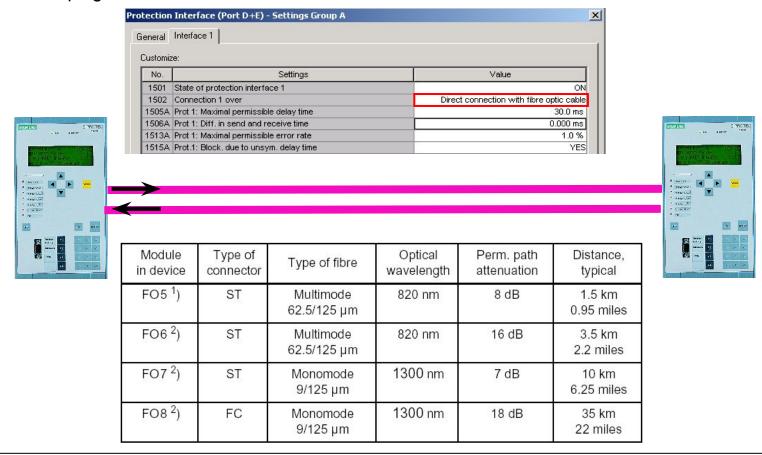






<u>Direct connection with fibre optic (FO) cables</u>

- Offers high speed tripping (12 ms), baud rate is 512 kBit/s
- Flexible plug in modules for different fibre cables or distances

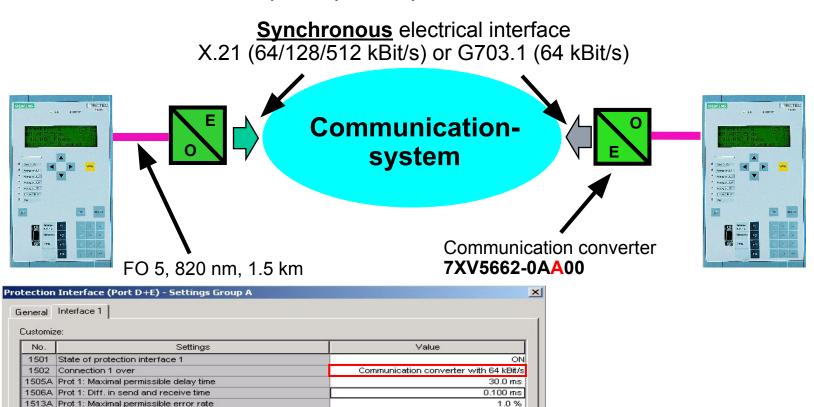




- Application: Digital communication network

Connection via a communication system with multiplexers

- Automatic delay time measurement (adaptive correction from 0 ms 30 ms)
- Immediate detection of split-path condition in the transmit or receive path
- Communication addresses clearly identify the relays



1515A Prot.1: Block, due to unsym, delay time

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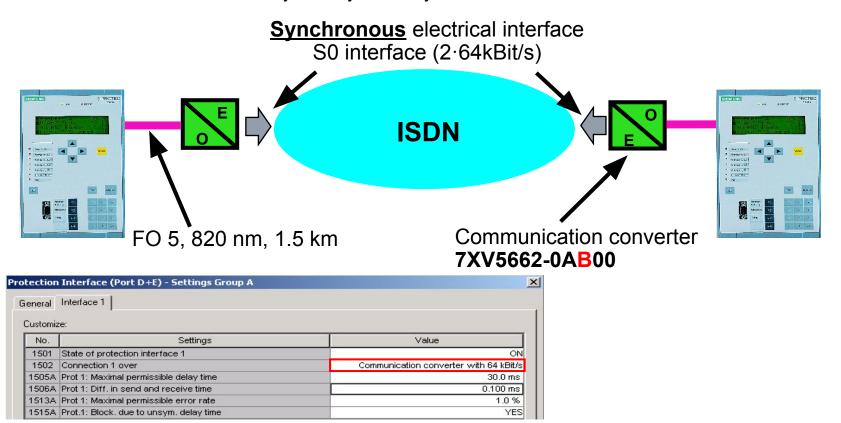
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- Application: ISDN network

Connection via an ISDN Network

- Automatic delay time measurement (adaptive correction from 0 ms 30 ms)
- Immediate detection of split-path condition in the transmit or receive path
- Communication addresses clearly identify the relays

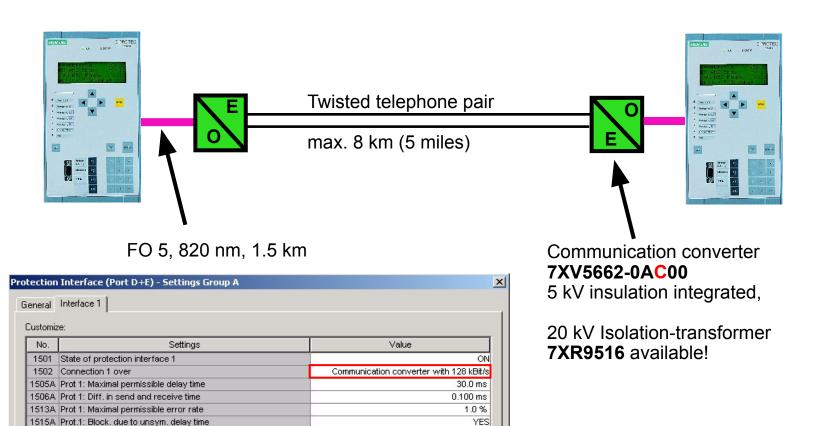




- Application: Leased telephone line or Pilot wire (1 of 2)

Leased telephone line (standby or dial-up)

- 2 wire telephone cable (max. 8 km)

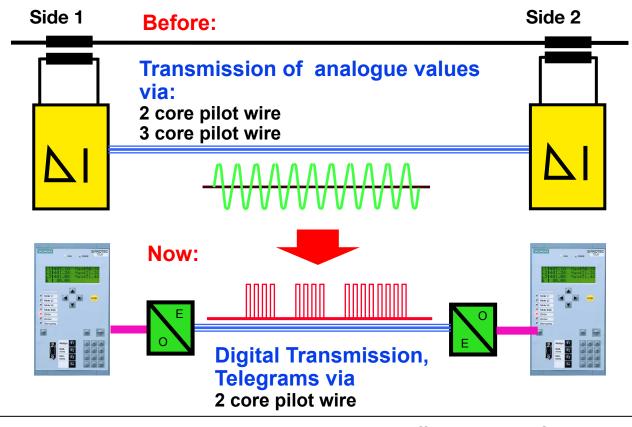




- Application: Leased telephone line or Pilot wire (2 of 2)

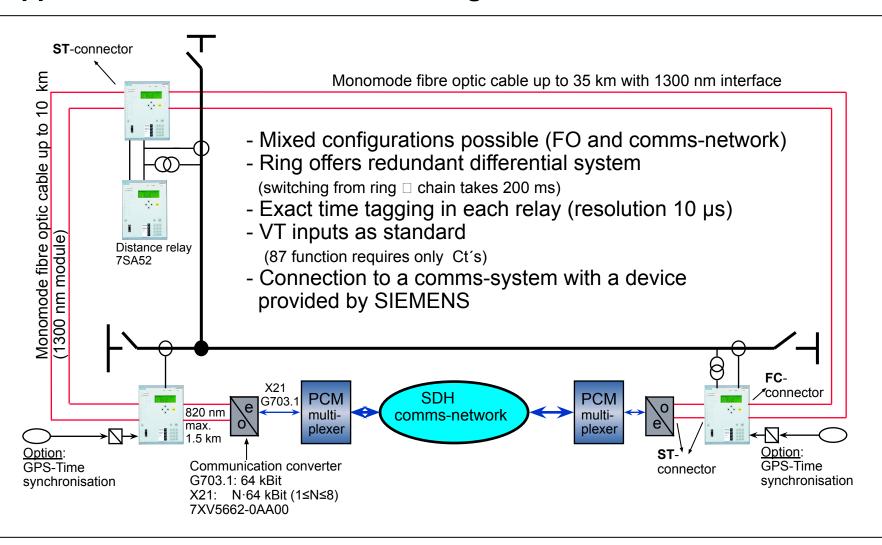
Serial communication

New technology on existing (copper-) connection





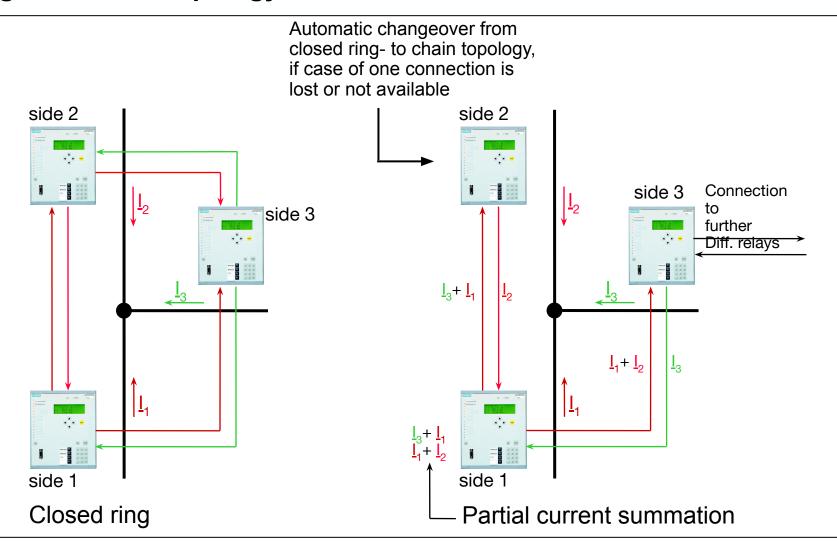
- Application for a three terminal configuration with 7SD523



Relay to Relay Communication



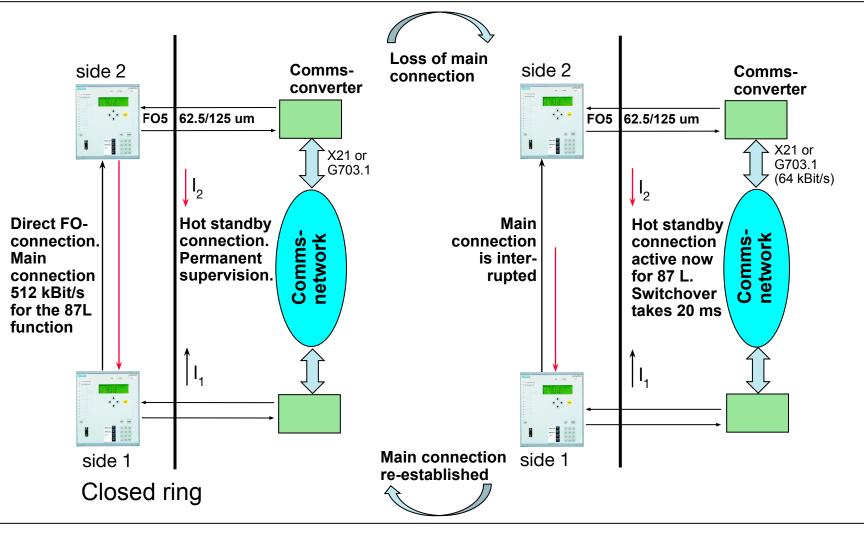
- Ring- and Chain topology, loss of one data connection tolerated



Relay to Relay Communication

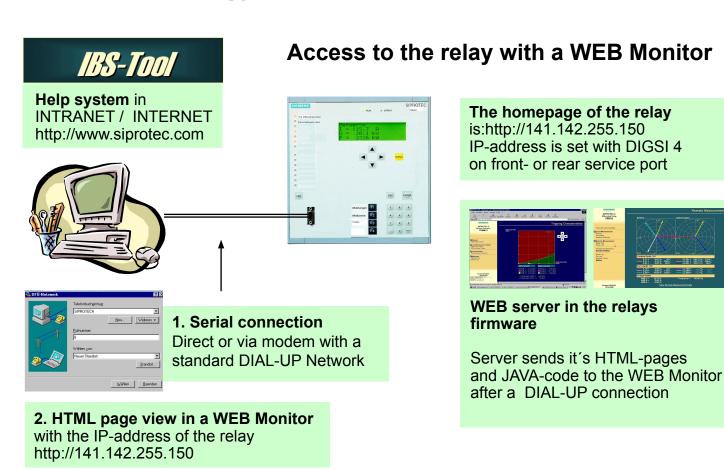
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- Hot- Standby connection in a two terminal configuration

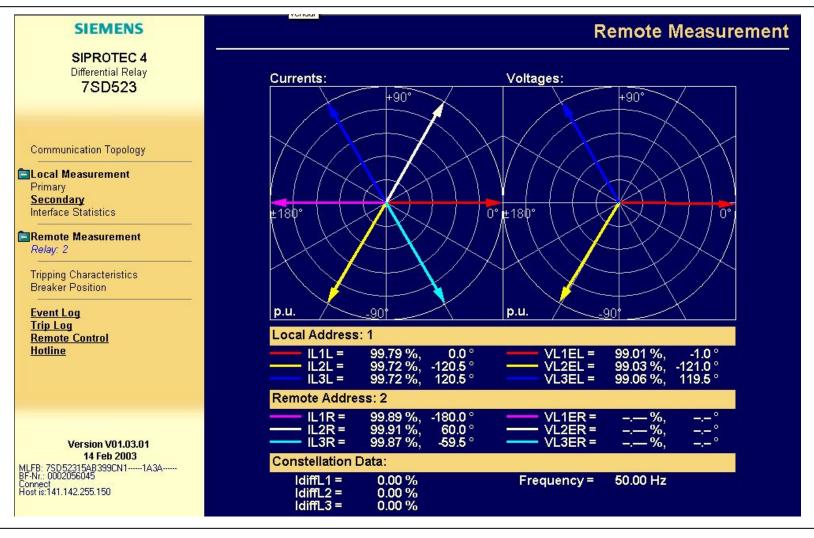




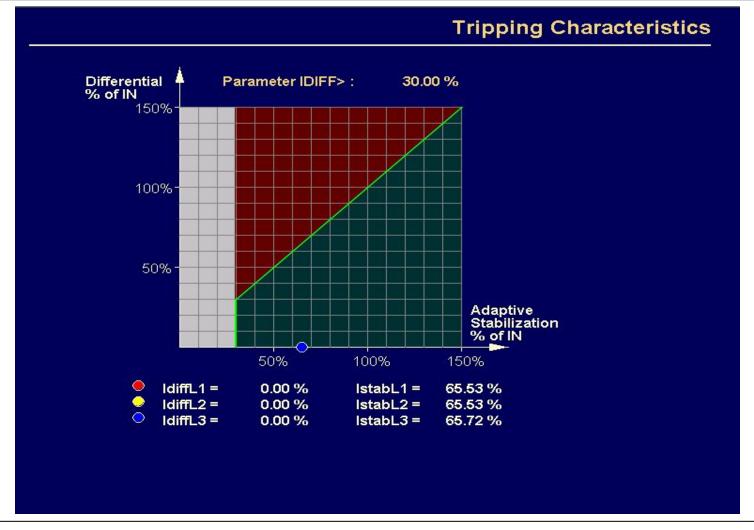
WEB-Technology



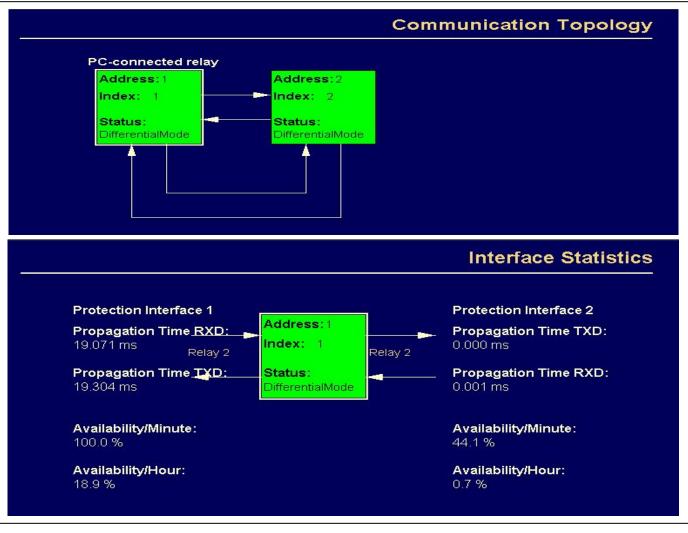












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